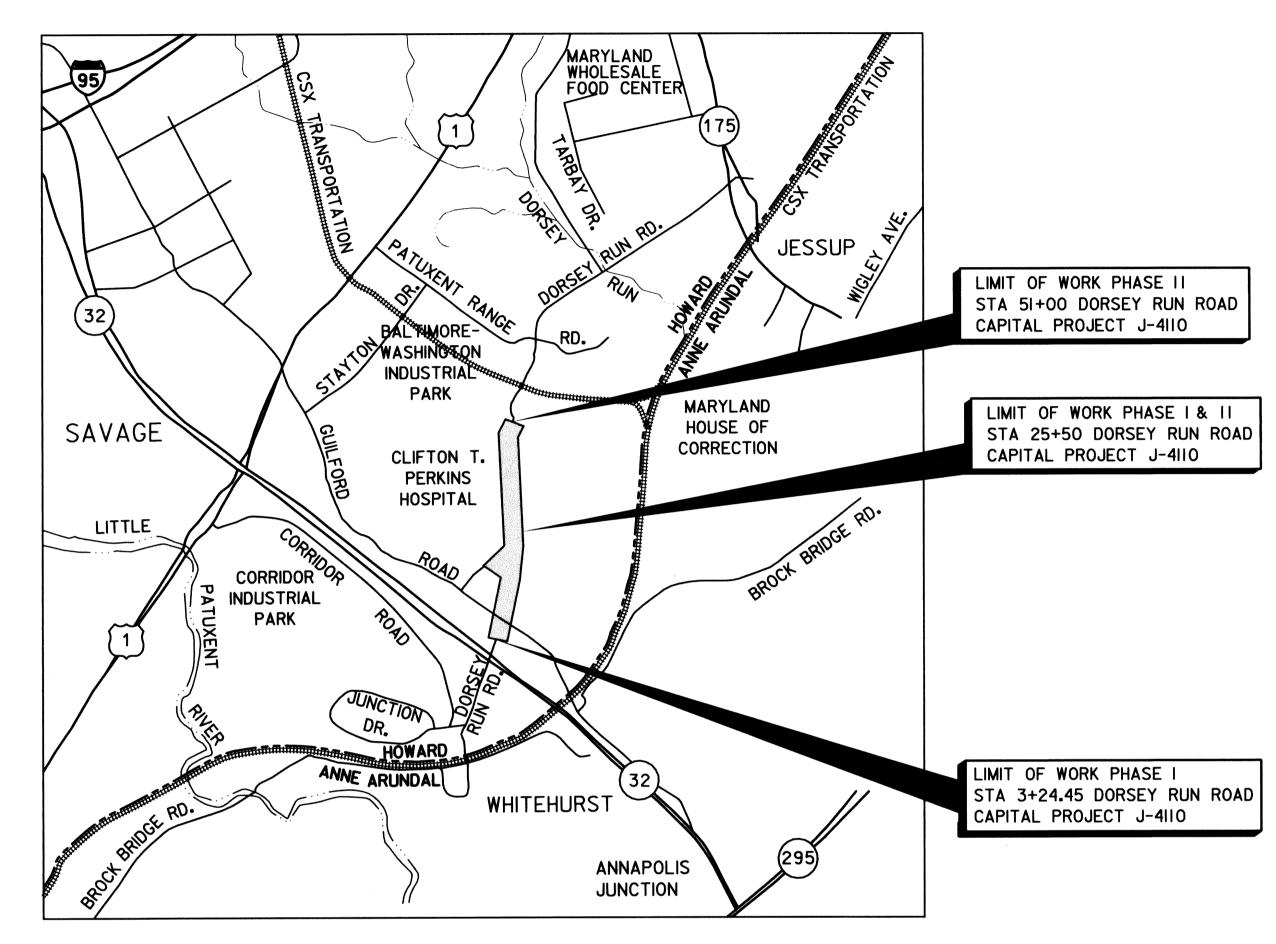
# HOWARD COUNTY, MARYLAND DEPARTMENT OF PUBLIC WORKS

		INDEX OF SHEETS
	SHEET NO.	DESCRIPTION
	1	TITLE SHEET
	2-3	TYPICAL SECTIONS
	4	DETAIL SHEET
	5	GEOMETRY SHEET
	6-7	ROADWAY PLANS
$\Lambda$	8-10B	CURB RETURN ELEVATION DETAILS
	11-12	EROSION & SEDIMENT CONTROL PLANS
	13	EROSION & SEDIMENT DETAILS
	14-16	ROAD PROFILES
	17-18	STORM DRAIN PROFILES & DETAILS
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	21	DRAINAGE AREA MAP
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	28-29	LIGHTING PLANS
	30	WATER PLAN & PROFILE
$\Lambda$	30A	PAVEMENT ELEVATIONS



#### GENERAL NOTES

- 1. ALL WORK SHALL BE PERFORMED IN ACCORDANCE WITH THE MARYLAND STATE HIGHWAY ADMINISTRATION'S STANDARD SPECIFICATIONS FOR CONSTRUCTION AND MATERIALS, OCTOBER 1993 AND THE STANDARD DETAILS OF THE MD. S.H.A. AND HOWARD COUNTY.
- 2. APPROXIMATE LOCATION OF EXISTING UTILITIES ARE SHOWN. THE CONTRACTOR SHALL TAKE ALL NECESSARY PRECAUTIONS TO PROTECT THE EXISTING UTILITIES AND MAINTAIN UNINTERRUPTED SERVICE. ANY DAMAGE INCURRED DUE TO CONTRACTOR'S OPERATION SHALL BE REPAIRED IMMEDIATELY AT THE CONTRACTOR'S EXPENSE.
- 3. THE CONTRACTOR SHALL TEST PIT EXISTING UTILITIES, WHERE DIRECTED BY THE ENGINEER, A MINIMUM OF TWO WEEKS IN ADVANCE OF CONSTRUCTION OPERATIONS.
- 4. CONTRACTOR TO NOTIFY THE FOLLOWING UTILITIES AT LEAST THREE DAYS BEFORE STARTING WORK SHOWN ON THESE DRAWINGS.

MISS UTILITY
BELL TELEPHONE SYSTEM
LONG DISTANCE CABLE DIVISION
BALTIMORE GAS AND ELECTRIC
HOWARD COUNTY BUREAU OF UTILITIES
HOWARD COUNTY CONSTRUCTION INSPECTION
SURVEY DIVISION

1-800-257-7777
393-3649
393-3553 OR 3554
539-8000 EXT. 691
313-2366
313-2366
313-2417/2418

- 5. INSTALLATION OF TRAFFIC CONTROL DEVICES, MARKING AND SIGNING SHALL BE IN ACCORDANCE WITH THE MANUAL OF UNIFORM TRAFFIC CONTROL DEVICES 1991 EDITION.
- 6. PIPE SHALL NOT BE INSTALLED BY THE CONTRACTOR UNTIL THE LENGTH CALLED FOR AT EACH STATION HAS BEEN APPROVED BY THE ENGINEER IN THE FIELD.
- 7. HORIZONTAL DATUM: NAD 27. VERTICAL DATUM: NGVD 88. MEAN SEA LEVEL DATUM 1929.
- 8. ALL FILL AREAS WITHIN ROADWAYS AND UNDER STRUCTURES TO BE COMPACTED TO A MINIMUM 95% OF MAXIMUM OBTAINABLE DENSITY DETERMINED BY MARSHALL PROCTOR.
- 9. ALL PIPE ELEVATIONS SHOWN ARE INVERT \_\_\_\_\_ ELEVATIONS.
- 10. PROFILE STATIONS SHALL BE ADJUSTED AS NECESSARY TO CONFORM TO PLAN DIMENSIONS.
- 11.ELDERLY AND HANDICAP FACILITIES THE DESIGN OF THIS PROJECT HAS INCORPORATED FACILITIES FOR THE ELDERLY AND HANDICAPPED IN COMPLIANCE WITH STATE AND FEDERAL LEGISLATION.
- 12. FOR ALL WETLAND ISSUES PLEASE SEE MDE TRACKING NO. 02-NT-0354/200265672.

LOCATION MAP SCALE: 1"=2000'

## DORSEY RUN ROAD (SOUTH LINK)

### ROAD REALIGNMENT

CAPITAL PROJECT J-4110 PHASE 1
ROADWAY CLASSIFICATION : MAJOR COLLECTOR
DESIGN SPEED = 40 MPH

DEPARTMENT OF PUBLIC WORKS

HOWARD COUNTY, MARYLAND

Photo

OTRECTOR OF PUBLIC WORKS

DATE

CHIEF, BUREAU OF HIGHWAYS

DATE

Phono: (410)

Phoenix - Nolan Joint Venture

1420-A Joh Avenue
Suiće A
Baltimere, Maryland 21227



	DES: J.R.H.	E.M.P.	Δ	Added IOB and Pavement Elevations	10-7-02	
	DRN: D.R.B.					
	DIM. D.M.D.					
	CHK:					
_	DATE:	- D.V	NO	DEVICTOR	DATE	600/
		BY	NO.	REVISION	DATE	600′

TITLE SHEET

BLOCK NO.

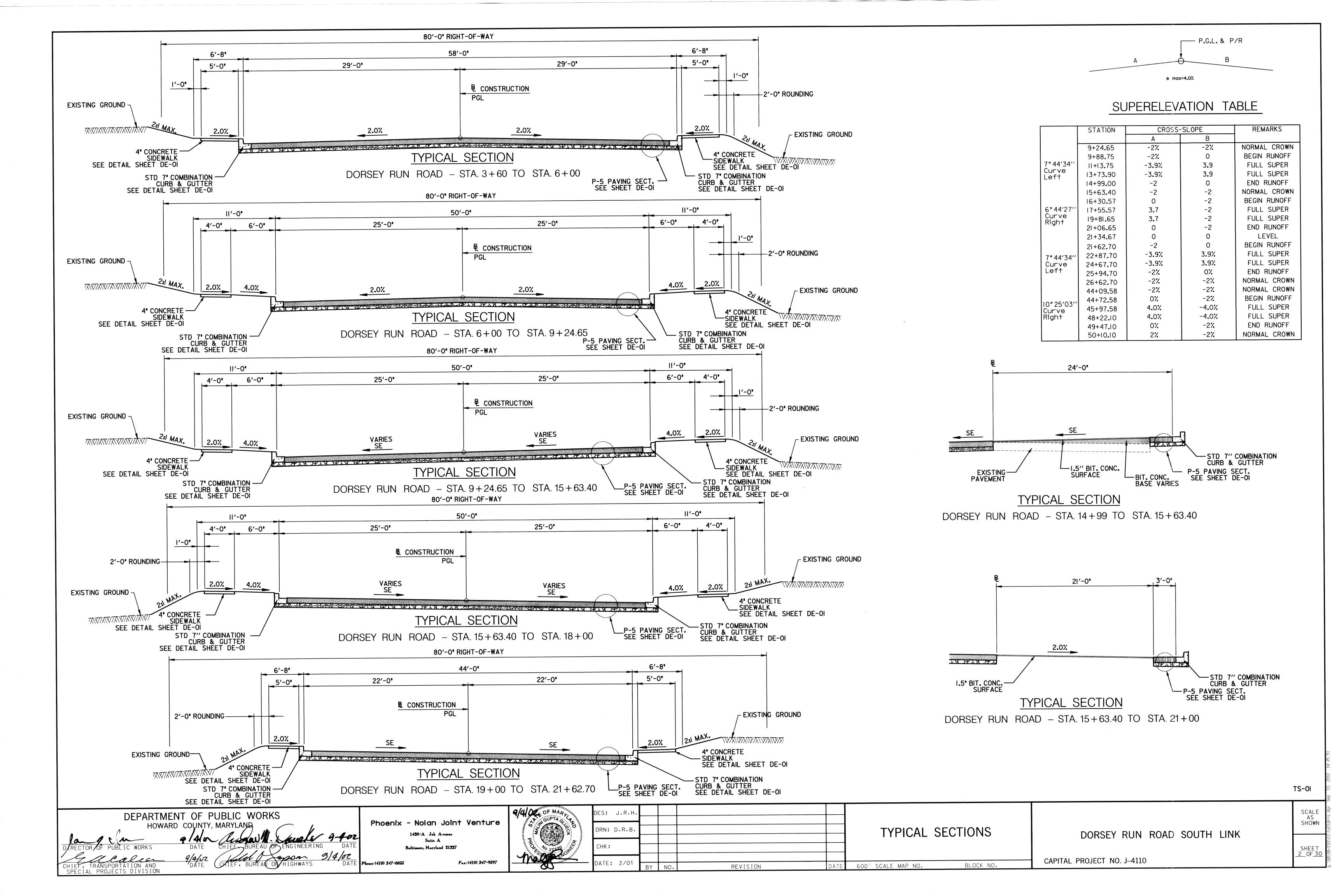
SCALE MAP NO.

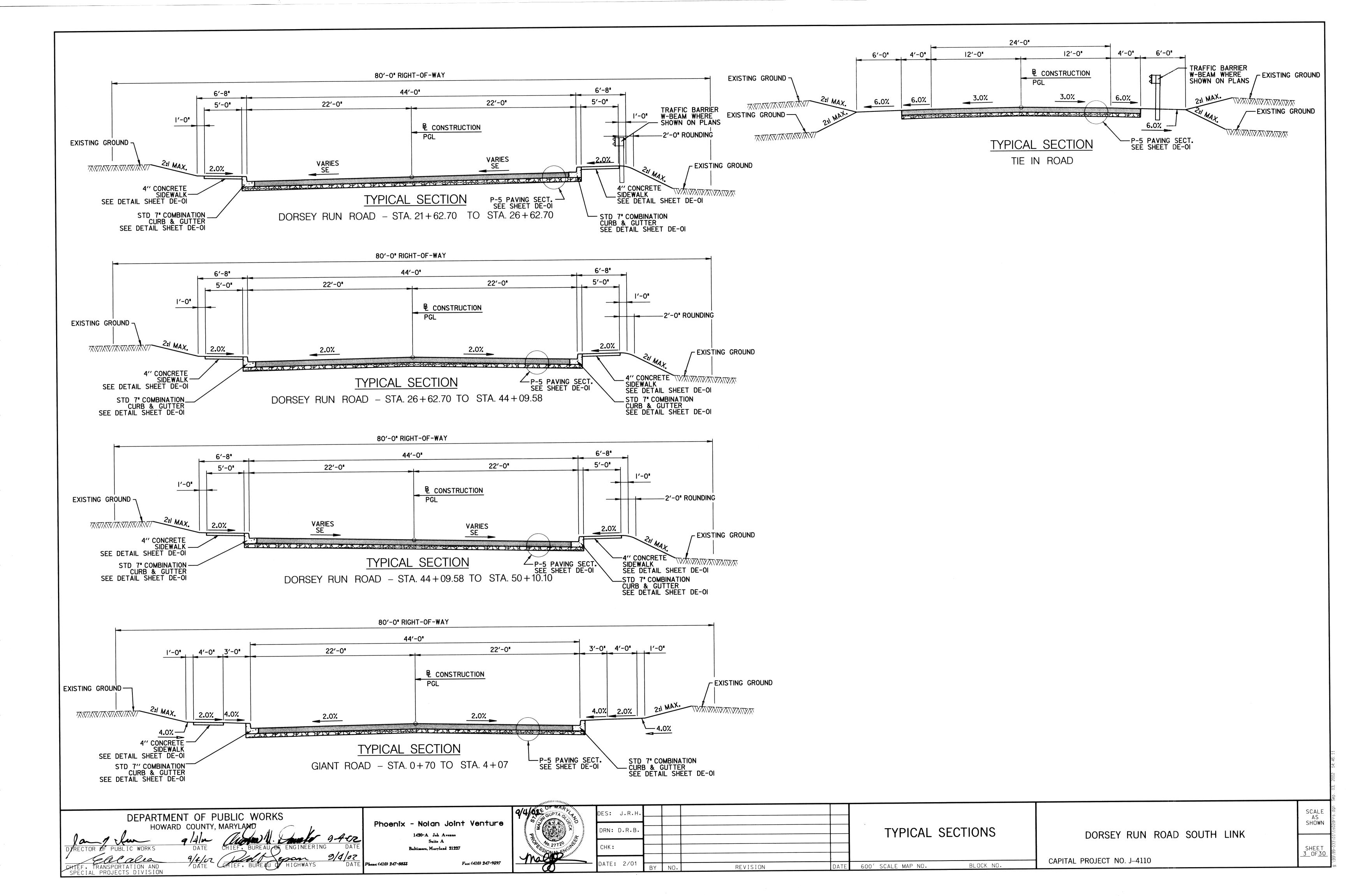
DORSEY RUN ROAD SOUTH LINK

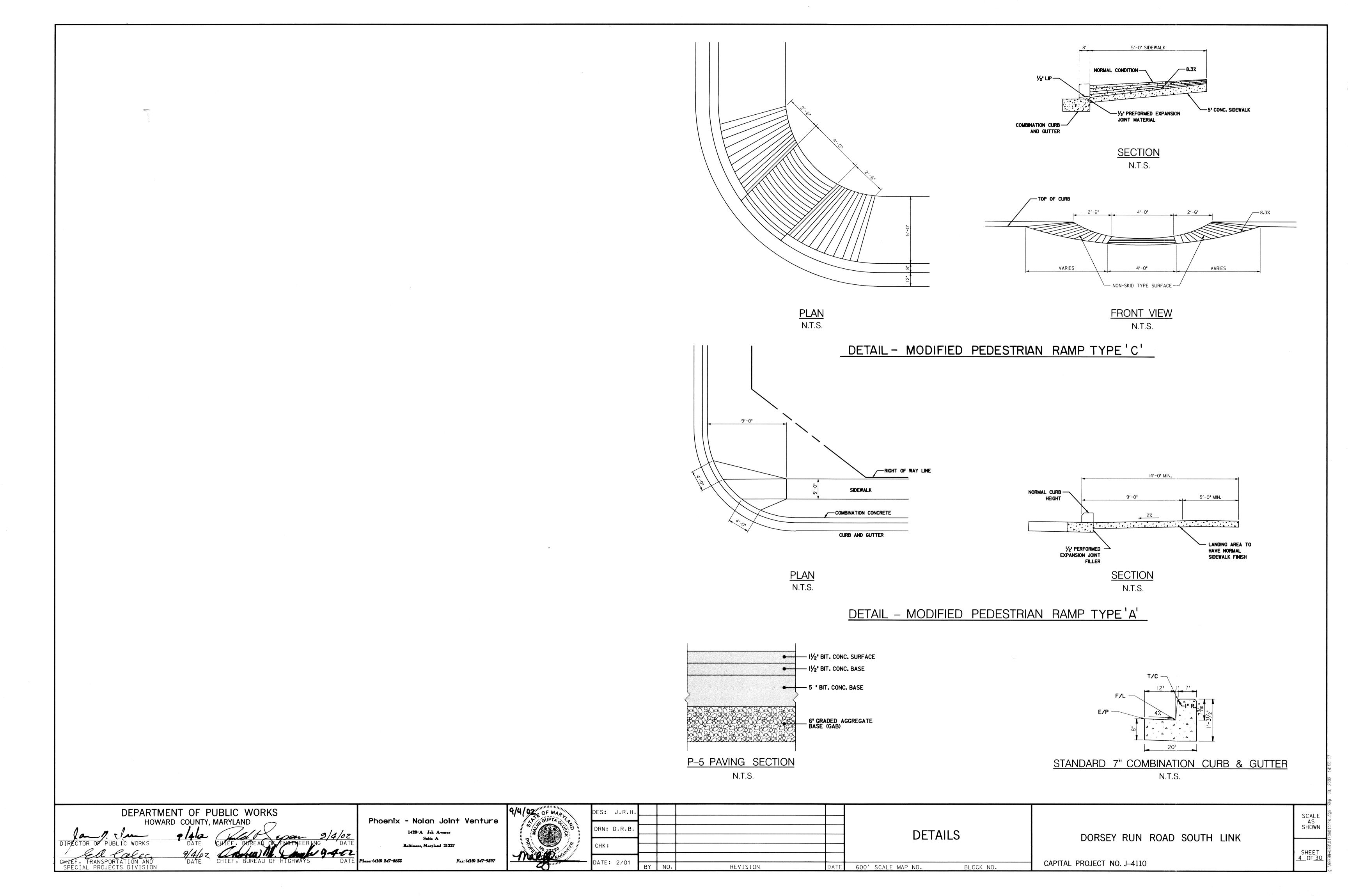
CAPITAL PROJECT NO. J-4110

SCALE AS SHOWN

SHEET 1\_0F<u>30</u>







BM 48DB

METAL DISK SET 2"BELOW SURFACE ON TOP OF CONCRETE COLUMN, 6'FROM EDGE OF DORSEY RUN RD. PAVING IN FRONT OF BLDG # 8470. DISC IS 29.6'SOUTH OF C&P POLE # 21 AND 16.7'NORTH OF A 3" MAPLE TREE.

N 475826.9 E 858587.3

ELEV. 239.559

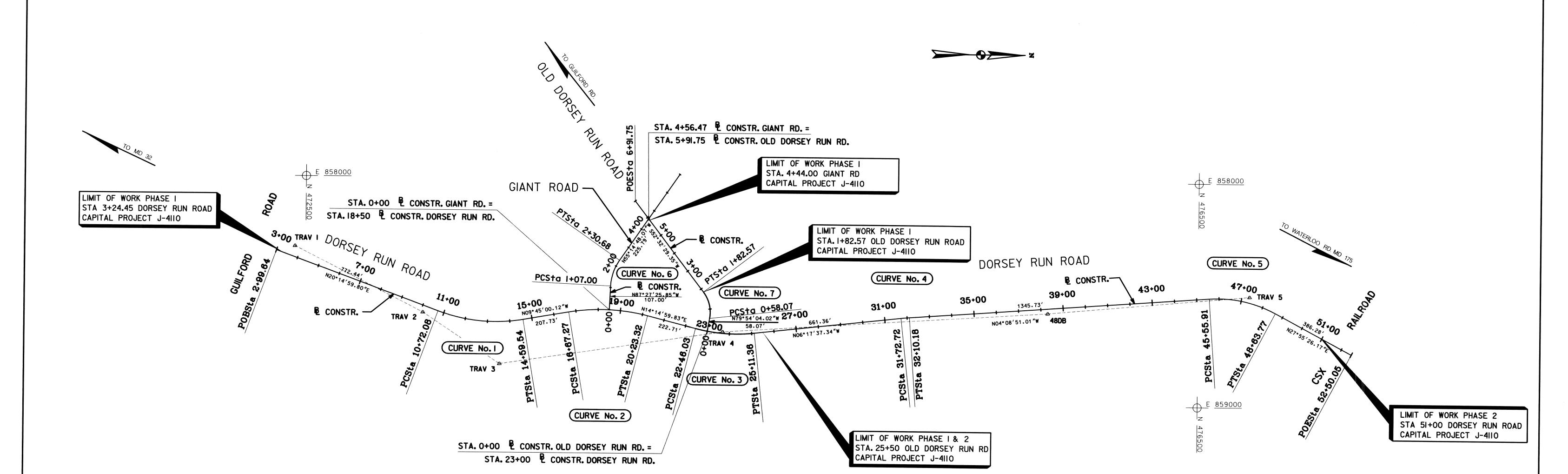
BM 48GB

METAL DISK SET ON TOP OF CONCRETE COLUMN, SET 14.4' FROM SOUTH EDGE OF PAVING OF RAMP FROM RTE #32 WEST, DISC IS 17.1' EAST OF A LIGHT POLE AT DORSEY RUN ROAD.

N 471481.4 E 858205.4

ELEV. 228.580

	TRAVERSE COORDINATES								
RAV NO.	NORTH	EAST	ELEV.	DESCRIPTION					
**************************************	472451.846	858312.322	220.91	REBAR & CAP					
2	473025.547	858605.075	216.42	REBAR & CAP					
3	473371.498	858832.178	207.81	REBAR & CAP					
4	474370.559	858681.642	207.81	REBAR					
5	476730.465	858504.146	207.55	REBAR & CAP					



	COC	DRDINA	TES-OLD DO	DRSEY F	RUN RD
	POINT TYPE	STATION	BASELINE	NORTH	ГАСТ
L	POB	0+00.00	B CONSTR.	474302.0406	EAST 858679.0741
	PC	0+58.07	₽ CONSTR.		858621.9062
	PI	1+24.16	₽ constr.	474323.8116	858556.8389
	PT	1+82.57	₽ constr.	474283.6158	858504.3761
L	POE	6+91.75	₽ CONSTR.	473973.9420	858100.1950

COORDINATES-GIANT ROAD							
POINT							
TYPE	STATION	BASELINE	NORTH	EAST			
POB	0+00.00	₽ constr.	473862.2710	858587.6330			
PC	1+07.00	₽ CONSTR.	473867.0180	858480.7420			
PI	1+07.52	₽ CONSTR.	473869.8358	858417.2826			
PT	2+30.68	₽ CONSTR.	473906.0458	858365.0925			
PI	4+56.47	₽ CONSTR.	474034.7610	858179.5740			

COORDINATES-DORSEY RUN ROAD							
POINT							
TYPE	STATION	BASELINE	NORTH	EAST			
POB	2+99.64	₽ CONSTR.	472369.7416	858331.8490			
PC	10+72.08	₽ CONSTR.	473094.4383	858599.2030			
PI	12+70.36	₽ CONSTR.	473280.4651	858667.8316			
PT	14+59.54	& CONSTR.	473475.8834	858634.2525			
PC	16+67.27	& CONSTR.	473680.6112	858599.0737			
PI	18+47.94	₽ CONSTR.	473858.6746	858568.4767			
PT	20+23.32	₽ CONSTR.	474033.7884	858612.9498			
PC	22+46.03	₽ CONSTR.	474249.6450	858667.7702			
PI	23+80.13	₽ CONSTR.	474379.6237	858700.7805			
PT	25+11.36	₽ CONSTR.	474512.9204	858686.0792			
PC	31+72.72	₽ CONSTR.	475170.2974	858613.5772			
PI	31+91.45	₽ CONSTR.	475188.9159	858611.5238			
PT	32+10.18	₽ CONSTR.	475207.5981	858610.1691			
PC	45+55.91	₽ CONSTR.	476549.8012	858512.8402			
Pl	47+13.99	₽ CONSTR.	476707.4684	858501.4017			
PT	48+63.77	₽ CONSTR.	476847.1441	858575.4363			
POE	52+50.05	₽ CONSTR.	477188.4510	858756.3316			

CURVE DATA									
CURVE									
NO.	Δ	Dc	R	L	Т	Ε			
l	29°59′59.92"	7°44′33.62"	740.00'	387.46′	198.28'	26.10'			
2	23°59′59.95"	6° 44′26.45"	850.00′	356.05'	180.67'	18.99'			
3	20° 32′37.17"	7° 44′33.62"	740.00′	265.33'	134.10'	12.05'			
4	2°08′46.33"		1000.00'	37.46′	18.73′	0.18'			
5	32°04′17.18 <b>"</b>	10°25′02 <b>.</b> 69 <b>"</b>	550.00′	307.86′	158.08'	22.27′			
6	32°12′37 <b>.</b> 55 <b>'</b>			123.68'	63.52′	8.99′			
7	47° 33′26.46"	38°11′49.87"	150.00′	124.50'	66.09′	13.91'			

DEPARTMENT OF PUBLIC WORKS

HOWARD COUNTY, MARYLAND

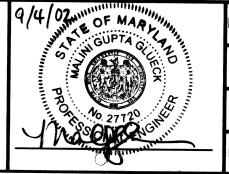
OF PUBLIC WORKS

DATE

OF PUBLIC WORKS

Phoenix - Nolan Joint Venture

1420-A Joh Avenue
Suite A



DES: J.R.H.				
	ļ			
DRN: D.R.B.				
0111/				
CHK:				
DATE:				
	BY	NO.	REVISION	DATE

GEOMETRIC LAYOUT

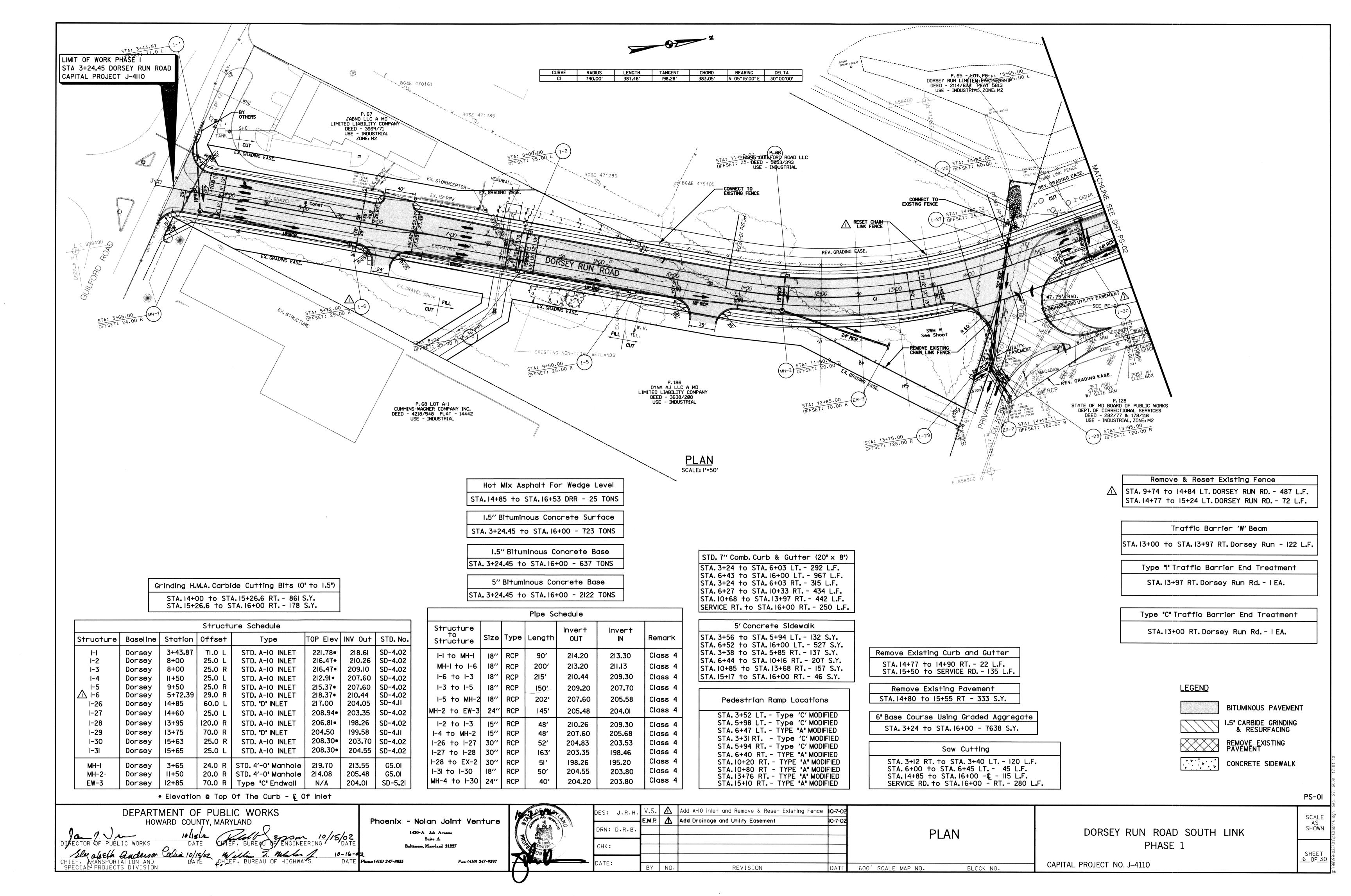
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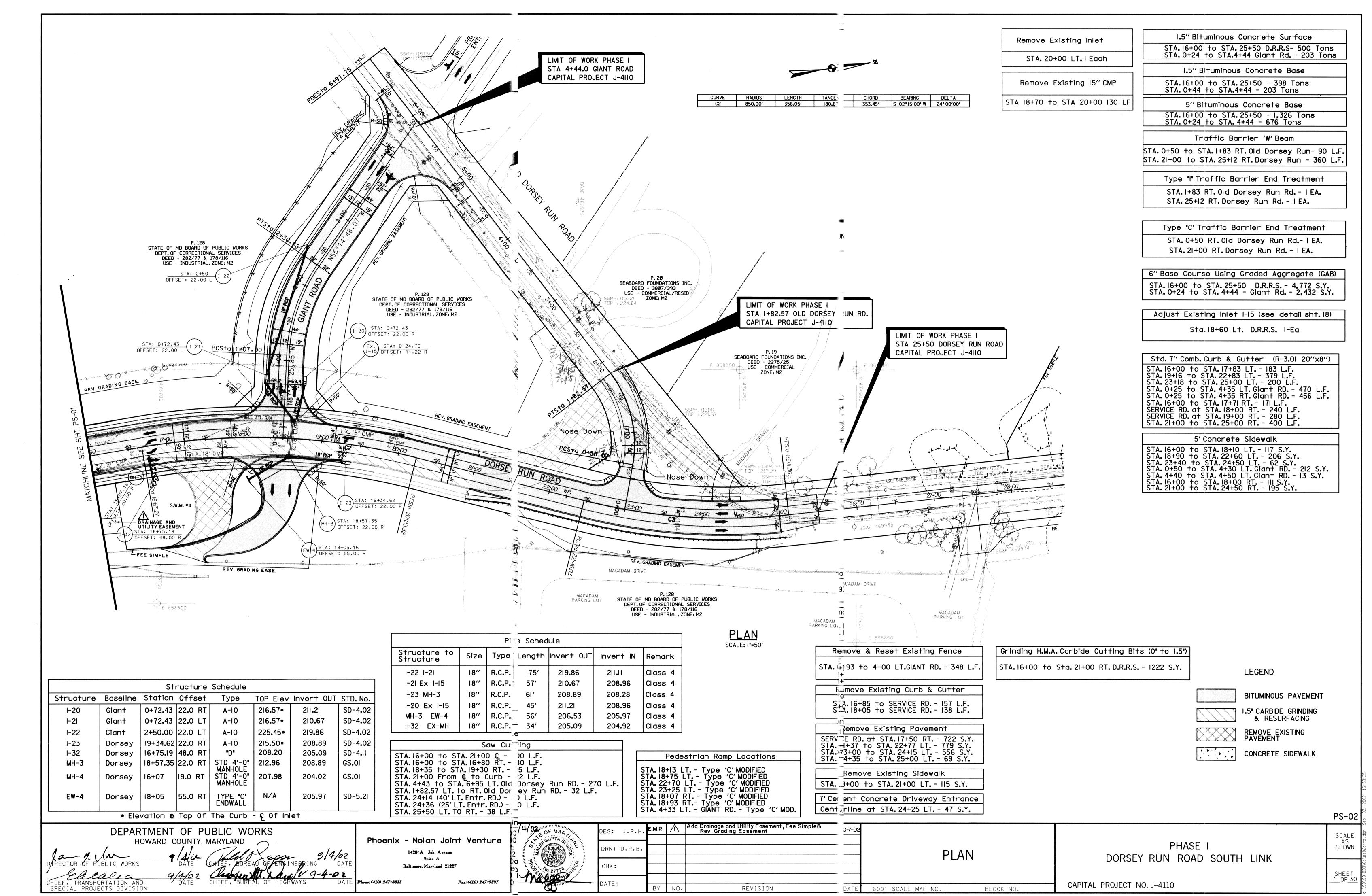
600' SCALE MAP NO.

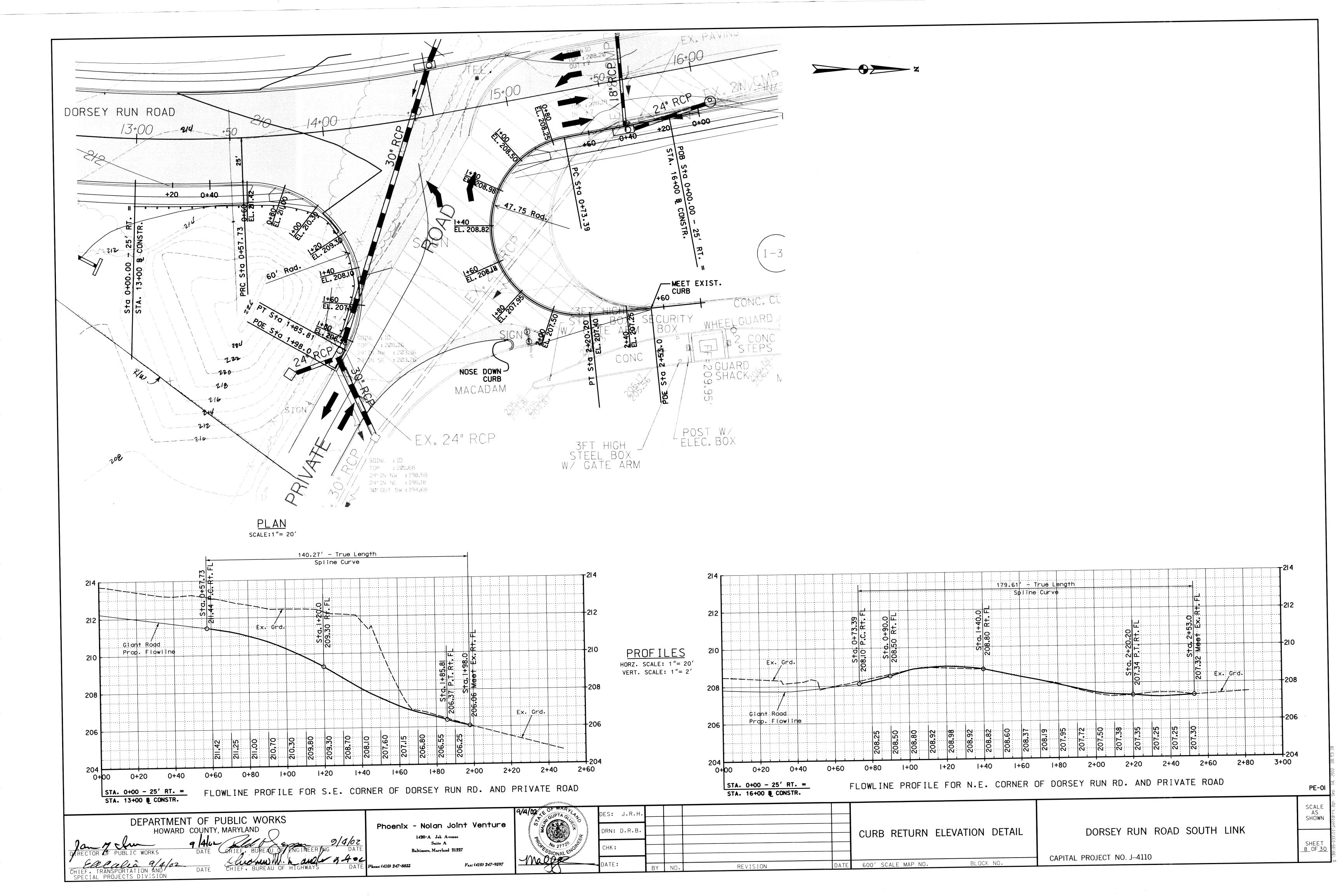
DORSEY RUN ROAD SOUTH LINK

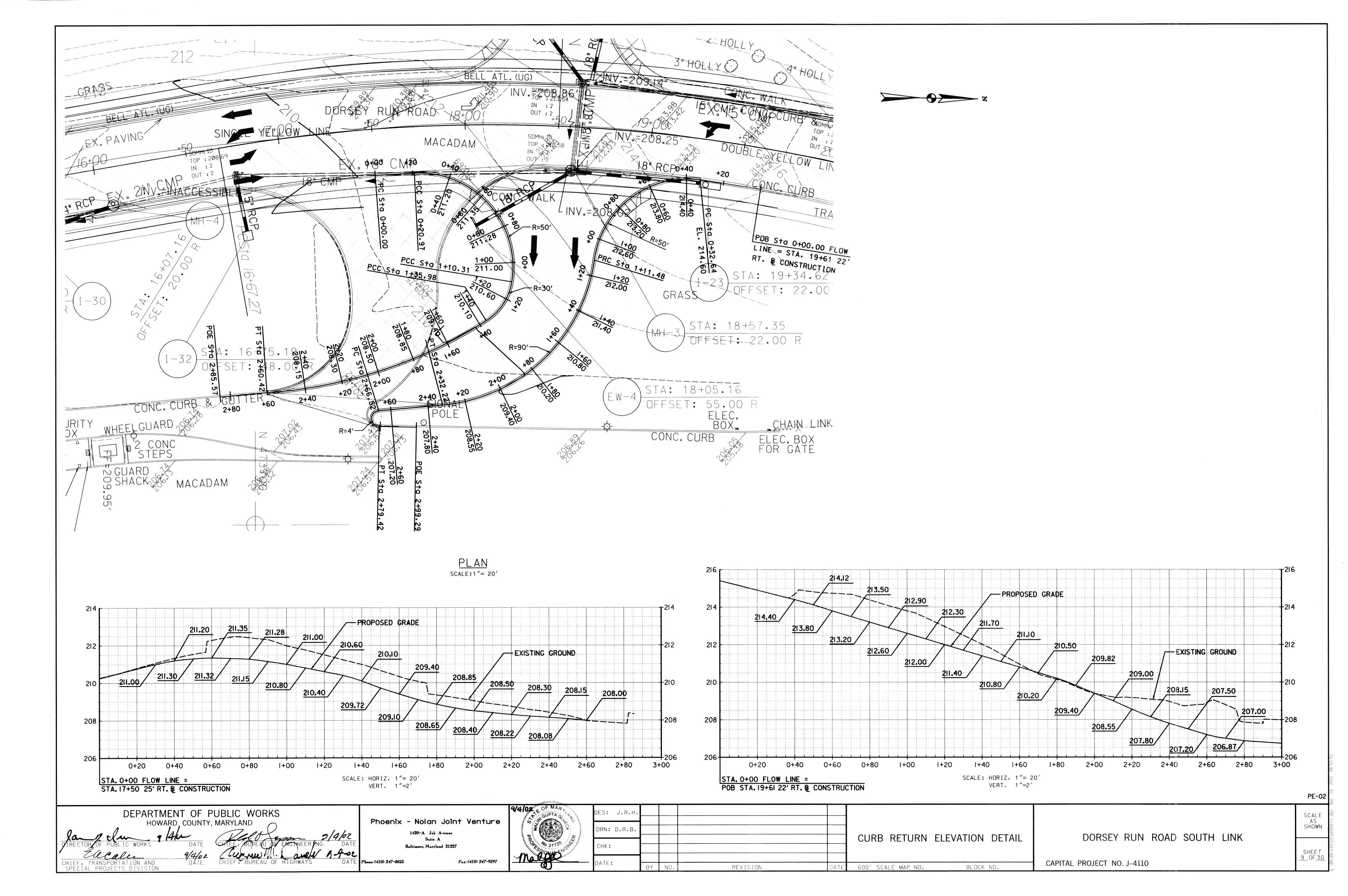
CAPITAL PROJECT NO. J-4110

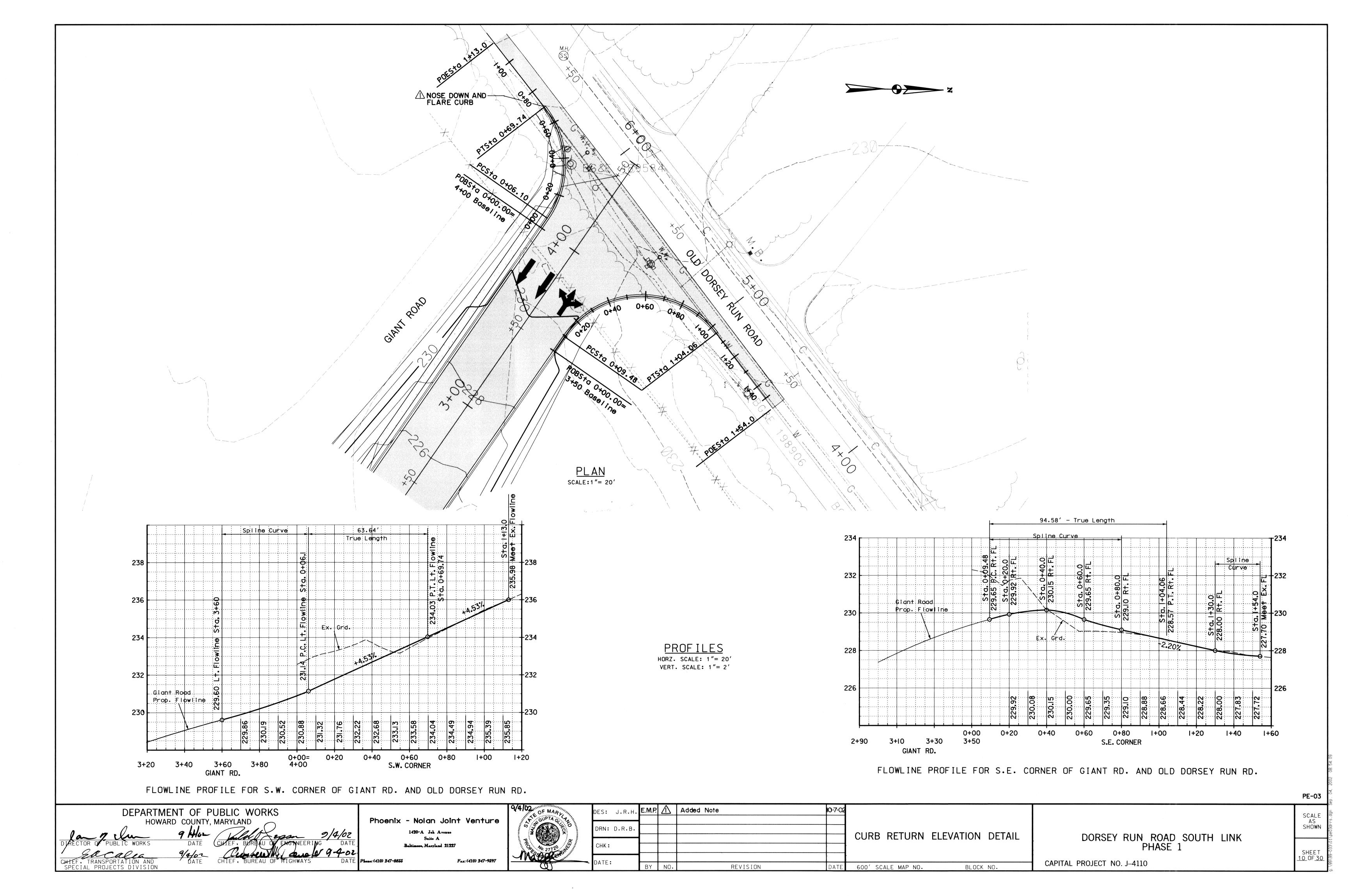
SCALE 1"= 200' SHEET 5\_0F30

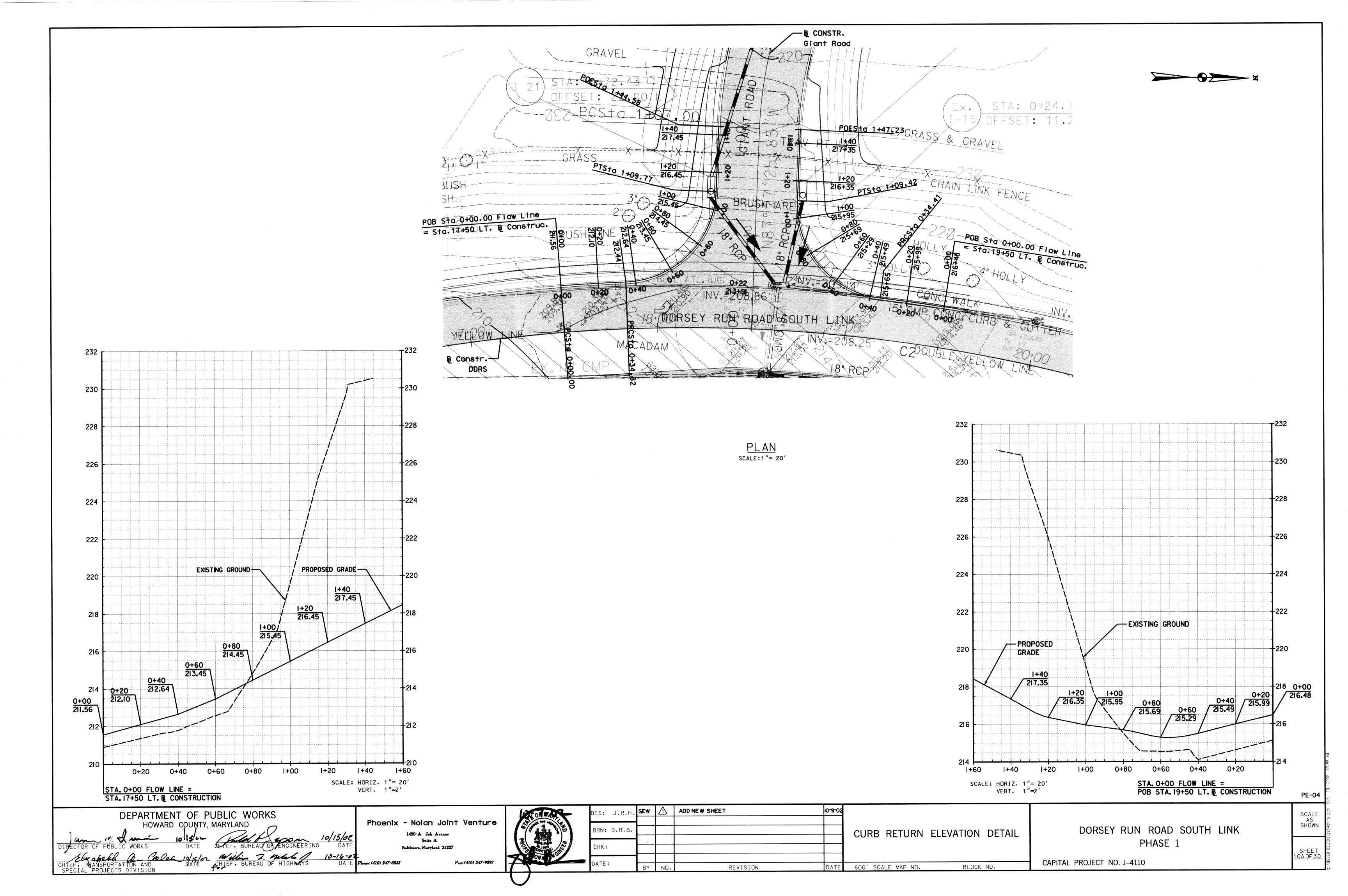


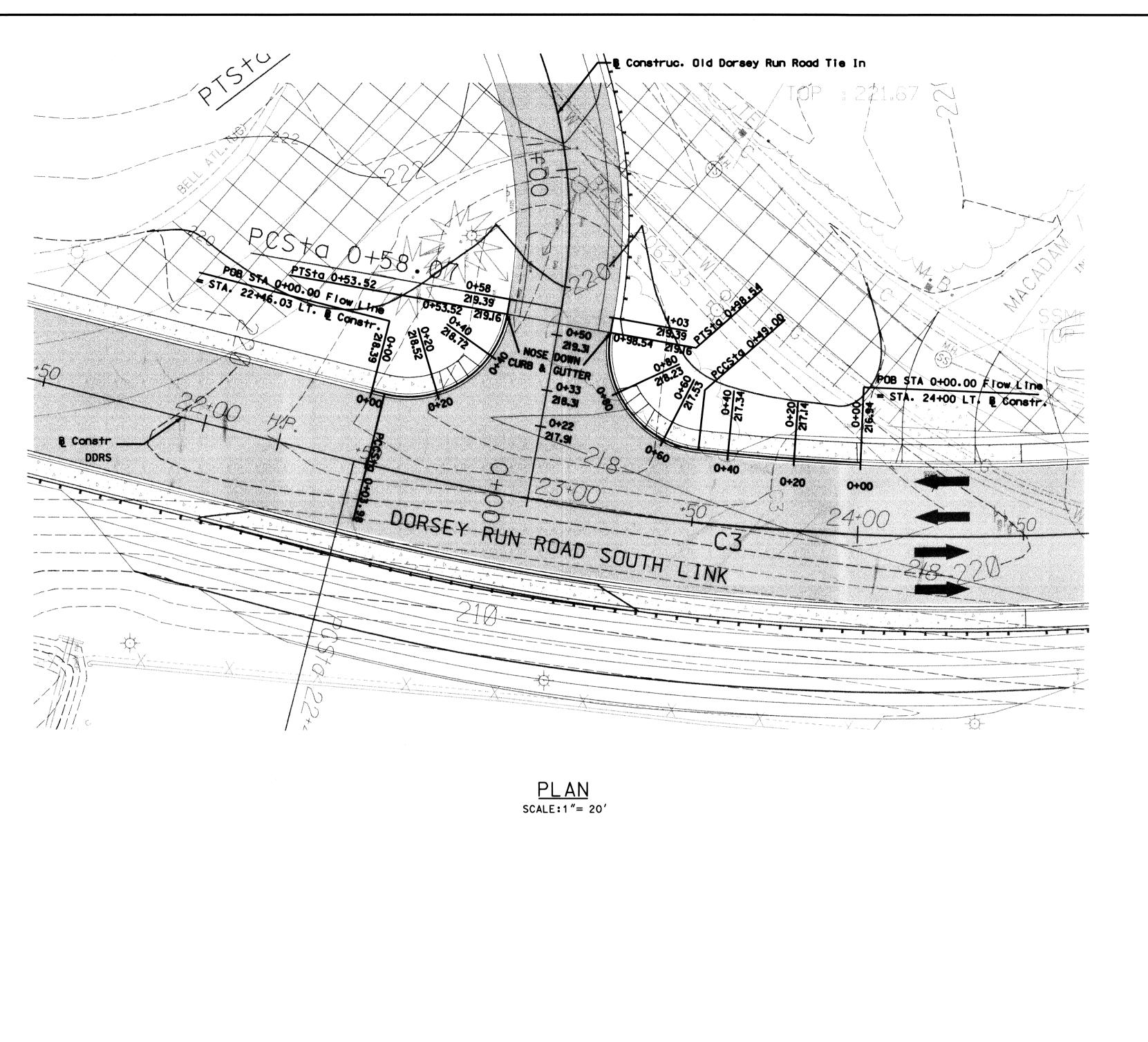


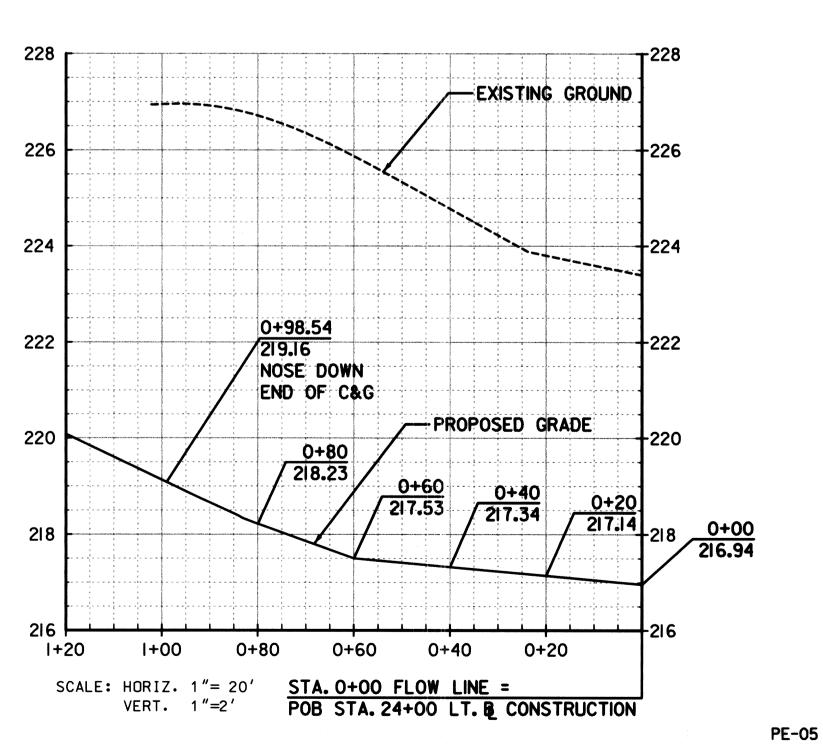


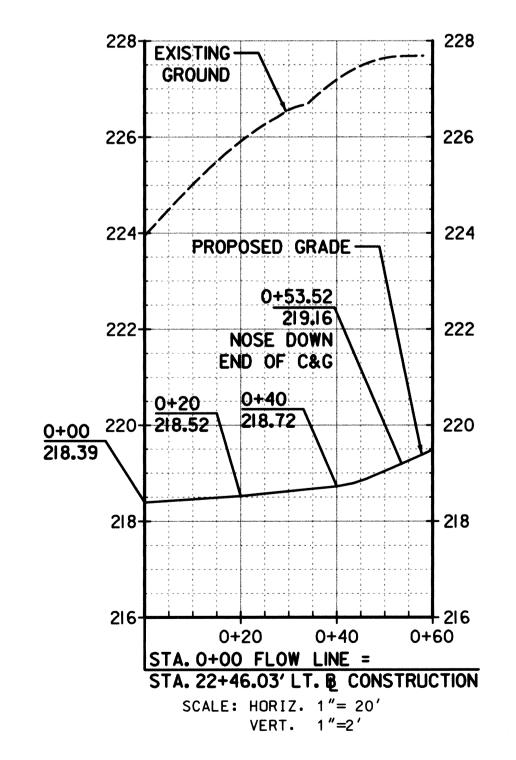












DEPARTMENT OF PUBLIC WORKS
HOWARD COUNTY, MARYLAND

CHIEF, TRANSPORTATION AND SPECIAL PROJECTS DIVISION

Phoenix - Nolan Joint Venture

1420-A Joh Avenue
Suite A
Baltimere, Maryland 21227

Phone: (410) 247-8833

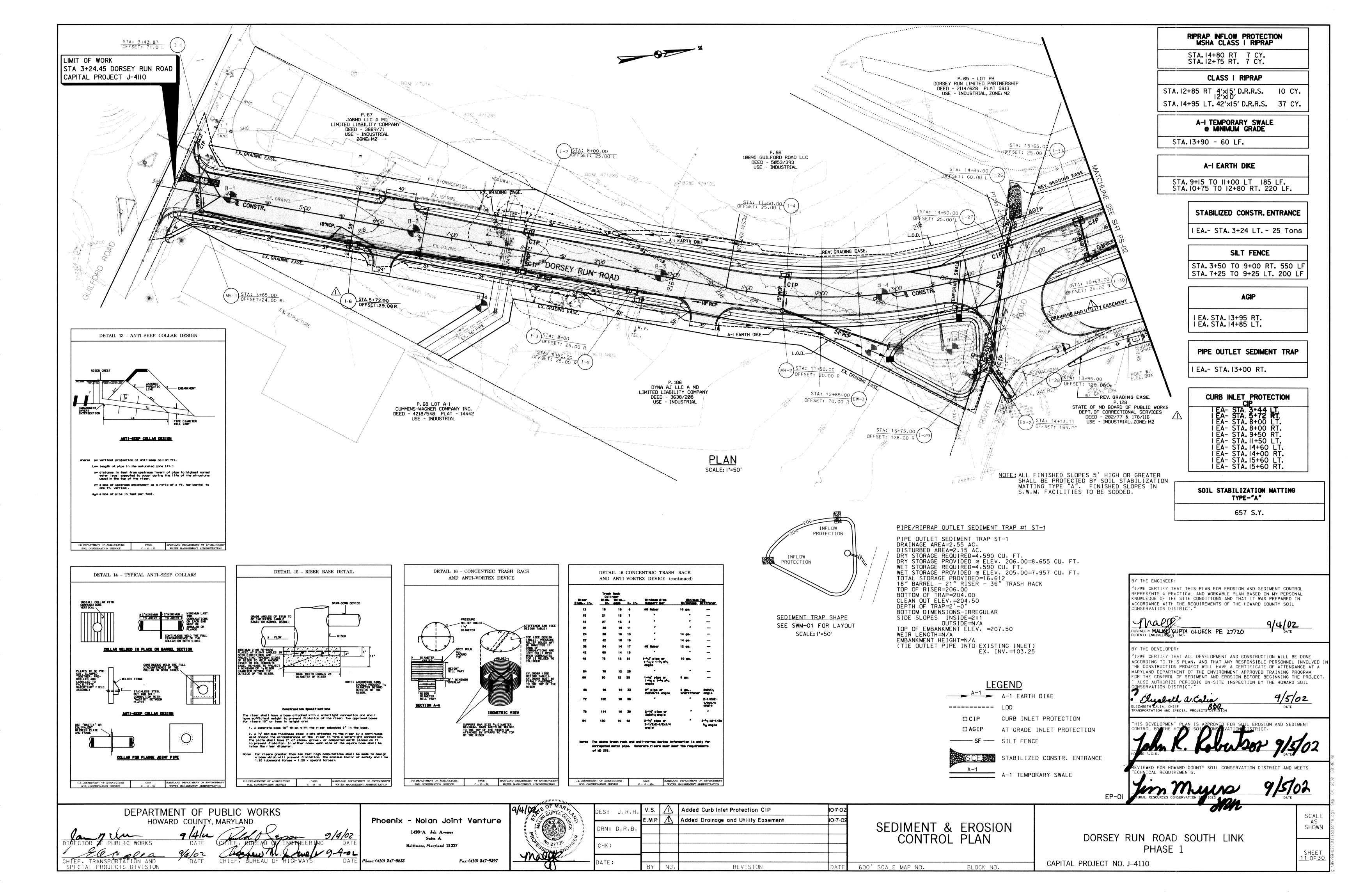
Fax: (410) 247-9397

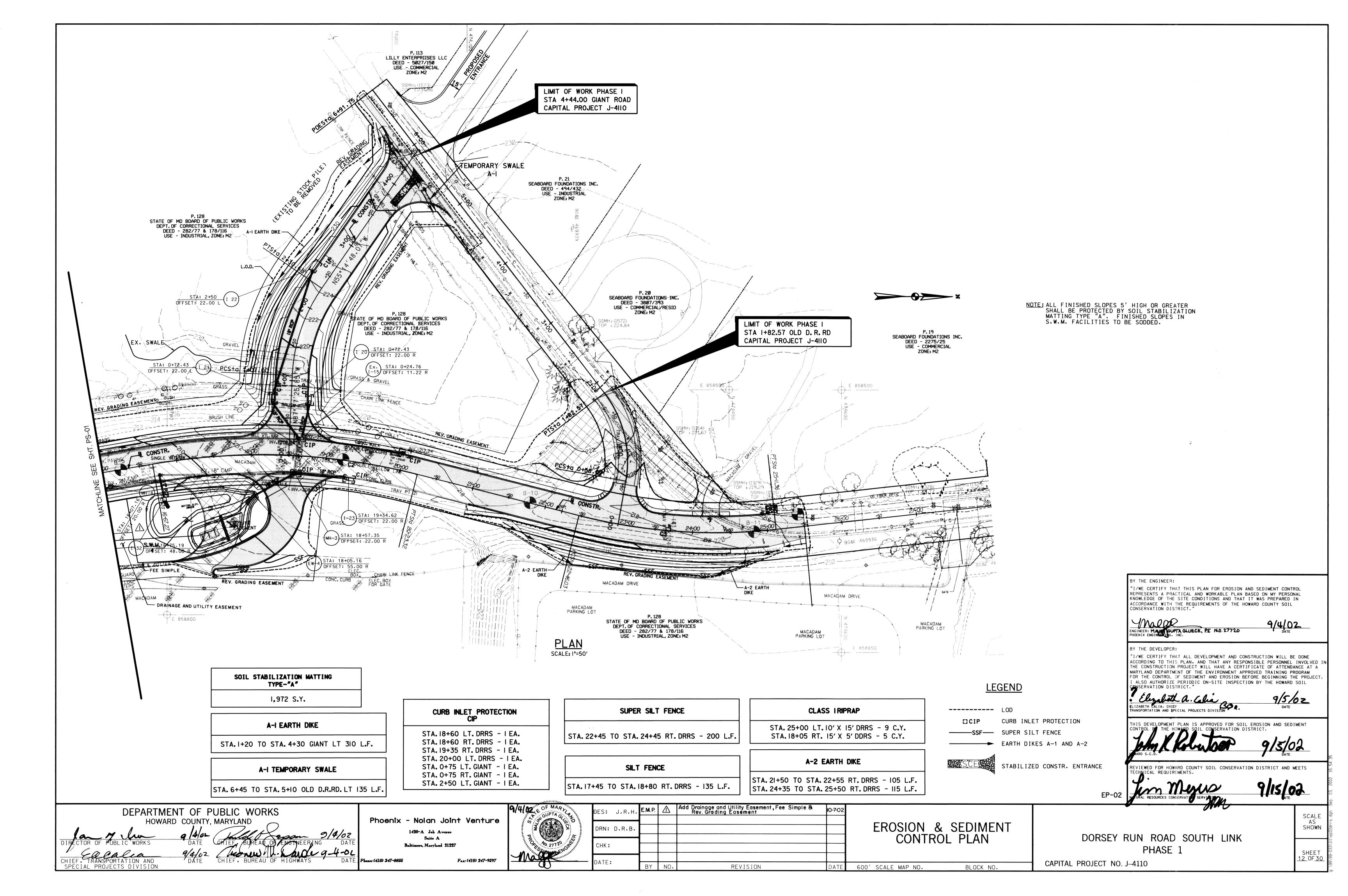
	DES: J.R.H.	SE.W.	$\triangle$
OF THE STATE OF TH	DRN: D.R.B.		
	CHK:		
TONA	DATE:		
	DATE.	BY	NO
	——————————————————————————————————————		

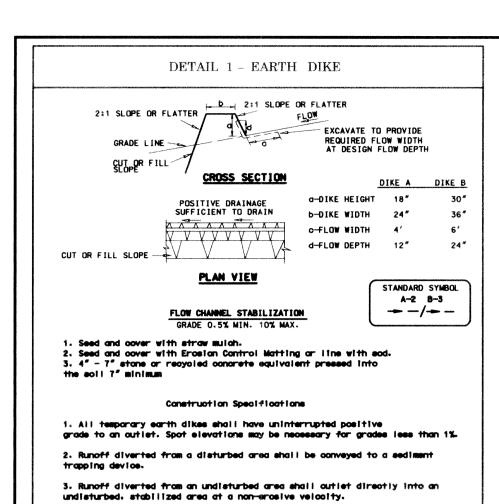
J.R.H.	S.E.W.	$\triangle$	ADD NEW SHEET	10-9-02	
					CLIDD DETLIDNI ELEVATIONI DETAIL
D.R.B.					CURB RETURN ELEVATION DETAIL OLD DORSEY RUN ROAD TIE IN
					DED DOKSET KON KOAD HE IN
	BY	NO.	REVISION	DATE	600' SCALE MAP NO. BLOCK NO.

DORSEY RUN ROAD SOUTH LINK
PHASE 1
CAPITAL PROJECT NO. J-4110

SCALE AS SHOWN SHEET 10B OF 30







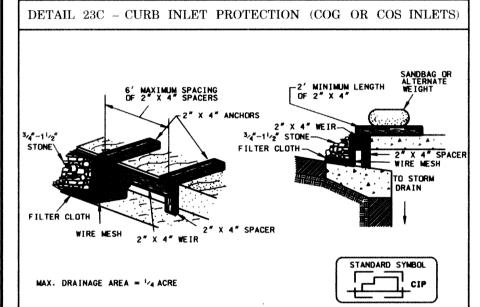
4. All trees, brush, stumps, obstructions, and other objectional material shall be removed and disposed of so as not to interfere with the proper functioning of the dike.

5. The dike shall be excavated or shaped to line, grade and cross section as required to meet the ariteria specified herein and be free of bank projections or other irregularities which will impade normal flow.

6. Fill shall be compacted by earth moving equipment-

it will not interfere with the functioning of the dike-

SOIL CONSERVATION SERVICE WATER MANAGEMENT ADMINISTRATION



. Attach a continuous piece of wire mesh (30" minimum width by throat length pius 4') to the 2" x 4" weir (measuring throat length plus 2') as shown on the standard

2. Place a continuous place of Geotextile Class E the same dimensions as the wire mesh over the wire mesh and securely attach it to the 2"  $\times$  4" weir-5. Securely nati the 2" X 4" wetr to a 9" long vertical epacer to be located between the weir and the inlet face (max. 4' apart). 4. Pigos the assembly against the injet throat and nati (minimum 2' lengths of

2" x 4" to the top of the well at spacer locations). These 2" x 4" anchors shall tend goroes the inlet top and be held in place by sandbags or alternate weig 5. The assembly shall be placed so that the end spacers are a minimum 1' beyond 6. Form the 1/2" x 1/2" wire meeh and the geotextile fabric to the concrete gutter and against the face of the curb on both sides of the inlet. Place clean  $\frac{3}{4}$  x  $1^{1}2^{2}$  stone over the wire mesh and geotextile in such a manner to prevent water from

entering the inlet under or around the geotextile-7. This type of protection must be inspected frequently and the filter cloth

and stone replaced when alagged with sediment. 8. Assure that storm flow does not bypass the injet by installing a temporary earth or asphalt dike to direct the flow to the injet.

SOIL CONSERVATION SERVICE WATER MANAGEMENT ADMINISTRATION DETAIL 23B - AT GRADE INLET PROTECTION GEOTEXTILE CLASS E -PLAN/CUT AWAY VIEW 6" - 3/4" - 11/2" STONE --- INLET GRATE -GEOTEXTILE CLASS F -WIRE TIES CROSS SECTION STANDARD SYMBOL MAX. DRAINAGE AREA = 1/4 ACRE

1. Lift grate and wrap with Geotextile Class E to completely cover all openings.

2. Place  $\frac{3}{4}$  to  $\frac{1}{2}$  stone,  $\frac{4}{-6}$  thick on the grate to secure the fabric and

PAGE

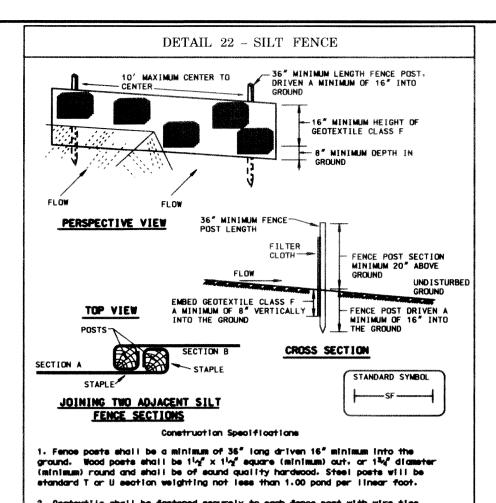
MARYLAND DEPARTMENT OF ENVIRONMEN

DEPARTMENT OF PUBLIC WORKS

HOWARD COUNTY, MARYLAND

provide additional filtration.

U.S. DEPARTMENT OF AGRICULTURE



Geotextile shall be fastened securely to each fence post with wire ties or staples at tap and mid-section and shall meet the following requirements 50 lbs/in (min.) 20 lbs/in (min.) Tensile Modulus 0.3 gal ft\*/ minute (max.) Teet: MSMT 322 . Where ends of geotextile fabric come together, they shall be overlapped folded and stapled to prevent sediment bypa 4. Slif Fence shall be inspected after each rainfall event and maintained when

bulges occur or when sediment accumulation reached 50% of the fabric height.

SOIL CONSERVATION SERVICE

MARYLAND DEPARTMENT OF ENVIRO

WATER MANAGEMENT ADMINISTRATION

	SILT FENCE	
	Stif Fence Design Cr	Iteria .
Slape Steepness	(Maximum) Slope Length	(Maximum) Siit Fence Length
Flatter than 50:1	unlimited	uni imited
50:1 to 10:1	125 <b>feet</b>	1+000 feet
10:1 to 5:1	100 <del>feet</del>	750 <del>feet</del>
5:1 to 3:1	60 feet	500 feet
3:1 to 2:1	40 feet	250 <del>feet</del>
2:1 and steeper	20 feet	125 feet
		nd elit fence length will be e the only perimeter control

DETAIL 2 - TEMPORARY SWALE

2:1 OR FLATTER -SLOPES

CROSS SECTION

FLOW

Seed and cover with straw mulch.
 Seed and cover with Erosian Control Matting or line with sod.

3. 4"-7" stone or recycled concrete equivalent pressed into soil

Construction Specifications

autlet. Spot elevations may be necessary for grades less than 1%-

5. The swale shall be excavated or shaped to line, grade and cross

6. Fill. If necessary, shall be compacted by earth moving equipment.

8. Inspection and maintenance must be provided periodically and after

that It will not interfere with the functioning of the swale.

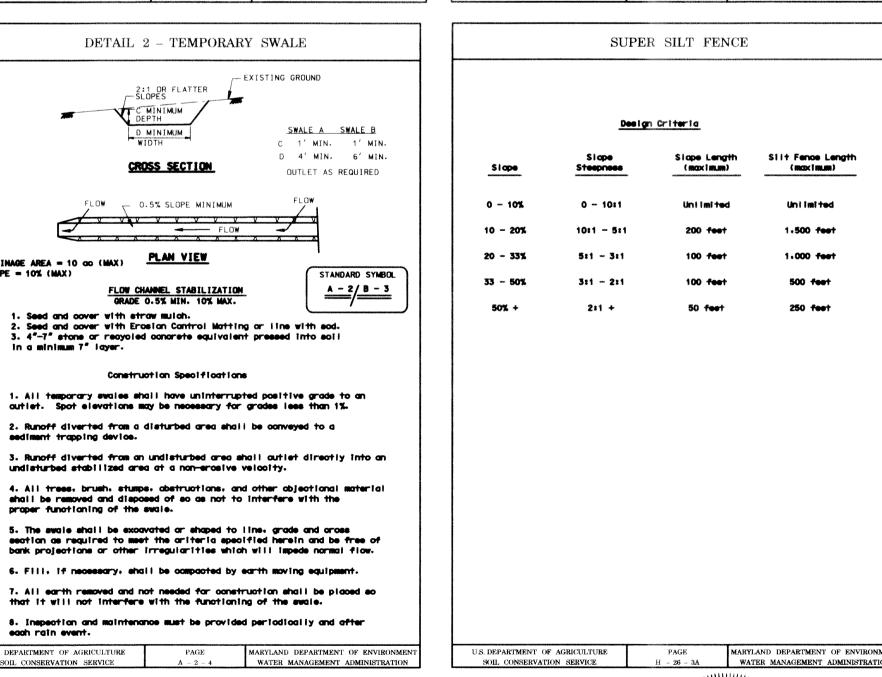
2. Runoff diverted from a disturbed area shall be conveyed to a

FLOW \_ 0.5% SLOPE MINIMUM

DRAINAGE AREA = 10 go (MAX)

SLOPE = 10% (MAX)

C MINIMUM



9/4/02/26

Phoenix - Nolan Joint Venture

420-A Joh Avenue

Suite A

Fax: (410) 247-9397

DETAIL 24 - STABILIZED CONSTRUCTION ENTRANCE

MINIMUM 6" OF 2"-3" AGGREGATE

VER LENGTH AND WIDTH OF

ISTING PAVEMENT

---- PIPE AS NECESSARY

EARTH FILL

--- 50' MINIMUM -

STRUCTURE

- \* 50' MINIMUM-

2. Width - 10' minimum, should be flared at the existing road to provide a turning

to placing stone. \*\*The plan approval authority may not require single family

4. Stone - crushed aggregate (2" to 3") or reclaimed or recycled concrete

equivalent shall be placed at least 6" deep over the length and width of the

5. Surface Water - all surface water flowing to or diverted toward construction

has no drainage to convey a pipe will not be necessary. Pipe should be sized

6. Location - A stabilized construction entrance shall be located at every point

where construction traffic enters or leaves a construction site. Vehicles leaving

the site must travel over the entire length of the stabilized construction entrance

U.S. DEPARTMENT OF AGRICULTURE | PAGE | MARYLAND DEPARTMENT OF ENVIRONMENT

DETAIL 33 - SUPER SILT FENCE

21/2" DIAMETER

OR ALUMINUM

FILTER CLOTH-

equired except on the ends of the fence.

every 24" at the top and mid section.

MBED FILTER CLOTH 8"\_\_\_\_

\* IF MULTIPLE LAYERS AR REQUIRED TO ATTAIN 42

SOIL CONSERVATION SERVICE F - 17 - 3 WATER MANAGEMENT ADMINISTRATION

34" MINIMUM

1. Fenoing shall be 42" in height and constructed in accordance with the latest Maryland State Highway Details for Chain Link Fenoing. The specification for a 6' fence shall be used, substituting 42" fabric and 6' length

Chain link fence shall be fastened securely to the fence posts with wire ties.

he lower tension wire, brace and truss rode, drive anchors and poet caps are not

3. Filter cloth shall be fastened securely to the chain link fence with ties spaced

. When two sections of filter aloth adjoin each other, they shall be overlapped

. Maintenance shall be performed as needed and silt buildups removed when "bulges"

7. Fliter aloth shall be fastened securely to each fence post with wire ties or

stables at top and mid section and shall meet the following requirements for

develop in the slif fence, or when slif reaches 50% of fence height

STANDARD SYMBOL

PROF ILE

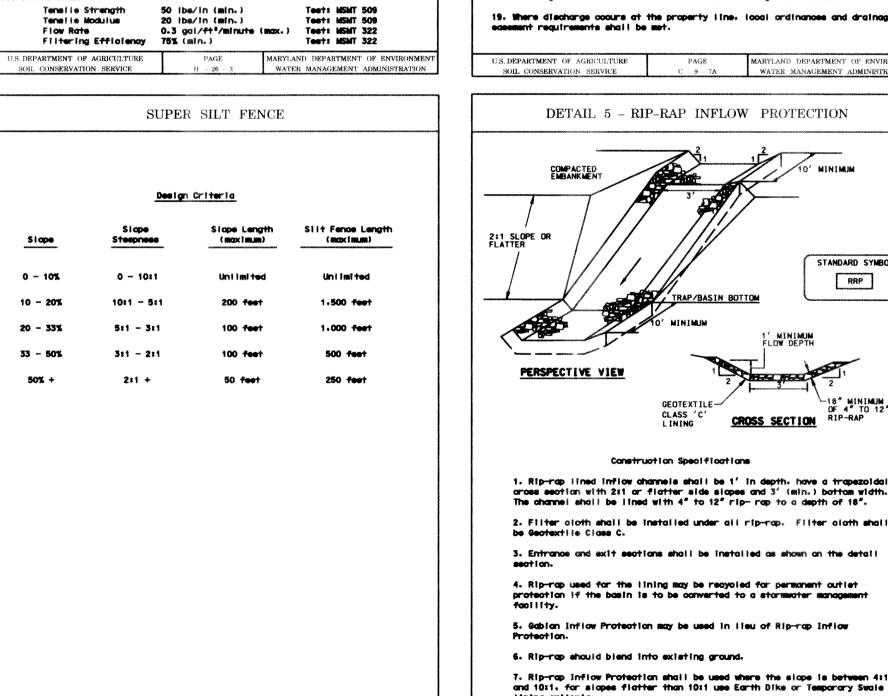
Length - minimum of 50' (\*30' for single residence lot).

\*\* GEOTEXTILE CLASS 'C'-

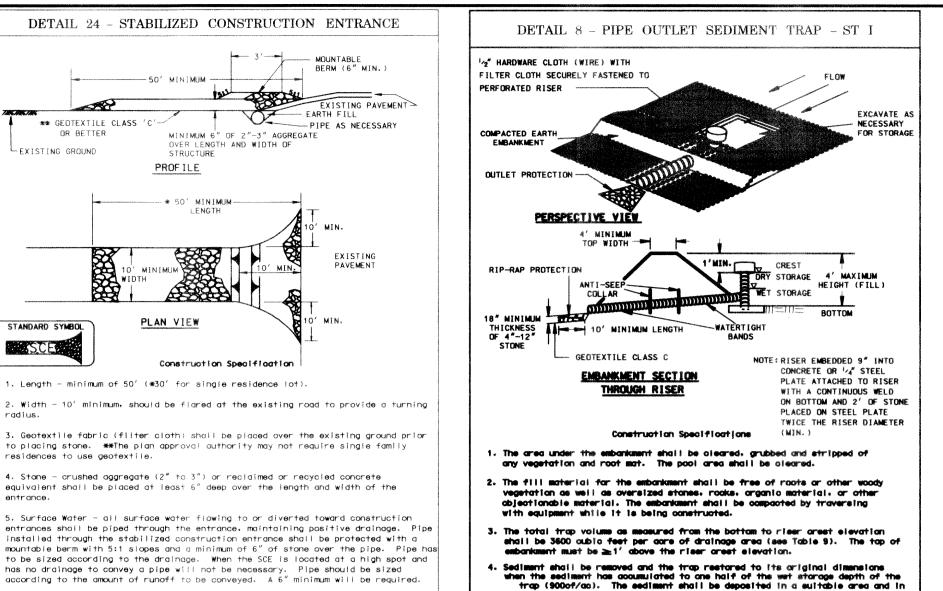
OR BETTER

LEXISTING GROUND

STANDARD SYMBOL



DRN: D.R.B



PIPE OUTLET SEDIMENT TRAP - ST I 6. Construction operations shall be corried out in such a monner that erosion and water pollution are abated. Once constructed, the top and outside face of the embankment shall be stabilized with seed and mulch. Points Stabilization Structure oritoria. The remainder of the interior slopes should be stabilized (one time) with seed and mulch upon trap completion and monitored and maintained erasion free during the life of the trap-

. The structure shall be inspected periodically and after each rain and repairs

7. The structure shall be removed and area stabilized when the drainage area has been properly stabilized.

8. All out and flil slopes shall be 2:1 or flatter. 9. All pipe connections shall be watertight.

made as necessary.

SOIL CONSERVATION SERVICE

10. Above the wet storage elevation, the riser shall be perforated with 12" wide by 6" long silts or 1" diameter holes spaced 6" vertically and horizontally.

ii. The riser shall be wrapped with  $^{1}2''$  hardware cloth (wire) then wrapped with Geotextile Ciges E. The filter cloth shall extend 6" above the highest slit and 6" below the lowest silt. Where ends of filter cloth come together. oloth shall be replaced as necessary to prevent alogging.

12. Strape or connecting bands shall be used to hold the filter cloth and wire fabric in place. They shall be placed at the top and bottom of the cloth. 13. Fill material around the pipe apillway shall be hand compacted in 4" layers. A minimum of 2' of hand-compacted backfill shall be placed over the

14. The riser shall be anahared with either a concrete base or steel plate base to prevent flotation. Canarete bases shall be at least twice the riser diameter and 12" deep with the riser embedded 9". Steel plate bases shall be at least twice the riser diameter. "4" minimum thickness and attached to the bottom of the riser by a continuous weld to form a watertight connection. Then place 2' of stone, gravel or tamped earth

pipe apiliway before arossing it with construction equipment.

15. Anti seep collars shall be constructed in accordance with plans (ref. table 16 and Details 13 and 14).

16. Cancentria track rack and anti-vartex device design details are on Detail 16. 17. Refer to Section D for dewatering requirements of sediment trape-18. Outliet - An outliet shall be provided, which includes a means of conveying

the discharge in an erosion free manner to an existing stable channel. 19. Where discharge coours at the property line, local ordinances and drainage

WATER MANAGEMENT ADMINISTRATION

STANDARD SYMBOL RRP CROSS SECTION 1. Rip-rap lined inflow channels shall be 1' in depth- have a trapezoidal

cross section with 2:1 or flatter side slopes and 3' (min.) bottom width. The channel shall be lined with 4" to 12" rip—rap to a depth of 18". 2. Filter cloth shall be installed under all rip-rap. Filter cloth shall

4. Rip-rap used for the lining may be recycled for permanent outlet protection if the basin is to be converted to a stormwater management

5. Gabian Inflow Protection may be used in itsu of Rip-rap Inflow

6. Rip-rap should blend into existing ground 7. Rip-rap Inflow Protection shall be used where the slope is between 411

PAGE MARYLAND DEPARTMENT OF ENVIRONMEN
B - 6 - 2 WATER MANAGEMENT ADMINISTRATION U.S. DEPARTMENT OF AGRICULTURE SOIL CONSERVATION SERVICE

REVISION

SEDIMENT CONTROL NOTES

1) A MINIMUM OF 24 HOURS NOTICE MUST BE GIVEN TO THE HOWARD COUNTY OFFICE OF INSPECTION AND PERMITS PRIOR TO THE START OF ANY CONSTRUCTION. (410-313-1850)

2) ALL VEGETATIVE AND STRUCTURAL PRACTICES ARE TO BE INSTALLED ACCORDING TO THE PROVISIONS OF THIS PLAN AND ARE TO BE IN CONFORMANCE WITH THE 1994 MARYLAND STANDARDS AND SPECIFICATIONS FOR SOIL EROSION AND

3) FOLLOWING INITIAL SOIL DISTURBANCE OR REDISTURBANCE. PERMANENT OR TEMPORARY STABILIZATION SHALL BE COMPLETED WITHIN: A) 7 CALENDAR DAYS FOR ALL PERIMETER SEDIMENT CONTROL STRUCTURES, DIKES, PERIMETER SLOPES AND ALL SLOPES GREATER THAN 3:1. B) 14 DAYS AS TO ALL OTHER DISTURBED OR GRADED AREAS ON THE PROJECT SITE.

4) ALL SEDIMENT TRAPS/BASINS SHOWN MUST BE FENCED AND WARNING SIGNS POSTED AROUND THEIR PERIMETER IN ACCORDANCE WITH VOL.1, CHAPTER 12, OF THE HOWARD COUNTY DESIGN MANUAL. STORM DRAINAGE.

5) ALL DISTURBED AREAS MUST BE STABILIZED WITHIN THE TIME PERIOD SPECIFIED ABOVE IN ACCORDANCE WITH THE 1994 MARYLAND STANDARDS AND SPECIFICATIONS FOR SOIL EROSION AND SEDIMENT CONTROL FOR PERMANENT SEEDINGS (SEC. 51) SOD (SEC. 54), TEMPORARY SEEDING (SEC. 50) AND MULCHING (SEC. 52.) TEMPORARY STABILIZATION WITH MULCH ALONE CAN ONLY BE DONE WHEN RECOMMENDED SEEDING DATES DO NOT ALLOW FOR PROPER GERMINATION AND ESTAB-LISHMENT OF GRASSES.

6) ALL SEDIMENT CONTROL STRUCTURES ARE TO REMAIN IN PLACE AND ARE TO BE MAINTAINED IN OPERATIVE CONDITION UNTIL PERMISSION FOR THEIR REMOVAL HAS BEEN OBTAINED FROM THE HOWARD COUNTY SEDIMENT CONTROL INSPECTOR.

7) SITE ANALYSIS: TOTAL AREA OF SITE ACRES 7.11 ACRES AREA DISTURBED 3.11 ACRES = 136.000SF AREA TO BE ROOFED OR PAVED AREA TO BE VEGETATIVELY STABILIZED 4.0 ACRES 24.536 CU. YDS. TOTAL CUT 2.043 CU. YDS. TOTAL FILL OFFSITE WASTE/BORROW AREA LOCATION IS UNKNOWN AT THIS TIME BUT WILL BE FROM A SITE WITH AN ACTIVE

8) ANY SEDIMENT CONTROL PRACTICE WHICH IS DISTURBED BY GRADING ACTIVITY FOR PLACEMENT OF UTILITIES MUST BE REPAIRED ON THE SAME DAY OF DISTURBANCE

9) ADDITIONAL SEDIMENT CONTROLS MUST BE PROVIDED. IF DEEMED NECESSARY BY THE HOWARD COUNTY DPW SEDIMENT CONTROL INSPECTOR.

10) ON ALL SITES WITH DISTURBED AREAS IN EXCESS OF 2 ACRES, APPROVAL OF THE INSPECTION AGENCY SHALL BE REQUESTED UPON COMPLETION OF INSTALLATION OF PERIMETER EROSION AND SEDIMENT CONTROLS, BUT BEFORE PROCEEDING WITH ANY OTHER EARTH DISTURBANCE OR GRADING. OTHER BUILDING OR GRADING INSPECTION APPROVALS MAY NOT BE AUTHORIZED UNTIL THIS INITIAL APPROVAL BY THE INSPECTION AGENCY IS MADE.

11) TRENCHES FOR THE CONSTRUCTION OF UTILITIES IS LIMITED TO THREE PIPE LENGTHS OR THAT WHICH SHALL BE BACKFILLED AND STABILIZED WITHIN ONE WORKING DAY, WHICHEVER IS SHORTER.

#### PERMANENT SEEDING NOTES

APPLY TO GRADED OR CLEARED AREAS NOT SUBJECT TO IMMEDIATE FURTHER DISTURBANCE WHERE A PERMANENT LONG-LIVED VEGETATIVE COVER IS NEEDED.

SEEDBED PREPARATION: LOOSEN UPPER THREE INCHES OF SOIL BY RAKING, DISKING OR OTHER ACCEPTABLE MEANS BEFORE SEEDING, IF NOT PREVIOUSLY LOOSENED

SOIL AMENDMENTS: IN LIEU OF SOIL TEST RECOMMENDATIONS, USE ONE OF THE FOLLOWING SCHEDULES:

1) PREFERRED -- APPLY 2 TONS PER ACRE DOLOMITIC LIMESTONE (92 LBS/1000 SQUARE FT) AND 600 LBS PER ACRE 10-10-10 FERTILIZER (14 LBS/1000 SQ FT) BEFORE SEEDING. HARROW OR DISC INTO UPPER THREE INCHES OF SOIL. AT TIME OF SEEDING, APPLY 400 LBS PER ACRE 30-0-0 UREAFORM FERTILIZER (9 LBS/1000 SQ FT.)

2) ACCEPTABLE --- APPLY 2 TONS PER ACRE DOLOMITIC LIMESTONE (92 LBS/1000 SQ FT) AND 1000 LBS PER ACRE 10-10-10 FERTILIZER (23 LBS/1000 SQ FT) BEFORE SEEDING. HARROW OR DISC INTO UPPER THREE INCHES OF SOIL.

SEEDING - FOR THE PERIODS MARCH 1 THRU APRIL 30. AND AUGUST 1 THRU OCTOBER 15. SEED WITH 60 LBS PER ACRE (1.4 LBS/1000 SQ FT) OF KENTUCKY 31 TALL FESCUE. FOR THE PERIOD MAY 1 THRU JULY 31, SEED WITH 60 LBS KENTUCKY 31 TALL FESCUE PER ACRE AND 2 LBS PER ACRE (.05 LBS/1000 SQ FT) OF WEEPING LOVEGRASS. DURING THE PERIOD OF OCTOBER 16 THRU FEBRUARY 28. PROTECT SITE BY: OPTION (1) 2 TONS PER ACRE OF WELL ANCHORED STRAW MULCH AND SEED AS SOON AS POSSIBLE IN THE SPRING. OPTION (2) USE SOD. OPTION (3) SEED WITH 60 LBS/ACRE KENTUCKY 31 TALL FESCUE AND MULCH WITH 2 TONS/ACRE WELL ANCHORED STRAW.

MULCHING -- APPLY 1 1/2 TO 2 TONS PER ACRE (70 TO 90 LBS/1000 SQ FT) OF UNROTTED SMALL GRAIN STRAW IMMEDIATELY AFTER SEEDING. ANCHOR MULCH IMMEDIATELY AFTER APPLICATION USING MULCH ANCHORING TOOL OR 218 GALLONS PER ACRE (5 GAL/1000 SQ FT) OF EMULSIFIED ASPHALT ON FLAT AREAS. ON SLOPES 8 FEET OR HIGHER, USE 348 GALLONS PER ACRE (8 GAL/1000 SQ FT) FOR ANCHORING.

MAINTENANCE -- INSPECT ALL SEEDED AREAS AND MAKE NEEDED REPAIRS. REPLACEMENTS AND RESEEDINGS.

#### TEMPORARY SEEDING NOTES

APPLY TO GRADED OR CLEARED AREAS LIKELY TO BE REDISTURBED WHERE A SHORT-TERM VEGETATIVE

SEEDBED PREPARATION: LOOSEN UPPER THREE INCHES OF SOIL BY RAKING, DISKING OR OTHER ACCEP-TABLE MEANS BEFORE SEEDING, IF NOT PREVIOUSLY LOOSENED.

SOIL AMENDMENTS: APPLY 600 LBS PER ACRE 10-10-10 FERTILIZER (14 LBS/1000 SQ. FT.).

SEEDING: FOR PERIODS MARCH 1 THRU APRIL 30 AND FROM AUGUST 15 THRU NOVEMBER 15, SEED WITH 2 1/2 BUSHEL PER ACRE OF ANNUAL RYE (3.2 LBS/1000 SQ FT). FOR THE PERIOD MAY 1 THRU AUGUST 14. SEED WITH 3 LBS PER ACRE OF WEEPING LOVEGRASS (.07 LBS/1000 SQ FT). FOR THE PERIOD NOVEMBER 16 THRU FEBRUARY 28, PROTECT SITE BY APPLYING 2 TONS PER ACRE OF WELL ANCHORED STRAW MULCH AND SEED AS SOON AS POSSIBLE IN THE SPRING, OR USE SOD.

MULCHING: APPLY 1 1/2 TO 2 TONS PER ACRE (70 TO 90 LBS/1000 SQ FT) OF UNROTTED SMALL GRAIN STRAW IMMEDIATELY AFTER SEEDING. ANCHOR MULCH IMMEDIATELY AFTER APPLICATION USING MULCH ANCHORING TOOL OR 218 GAL PER ACRE (5 GAL/1000 SQ FT) OF EMULSIFIED ASPHALT ON FLAT AREAS. ON SLOPES 8 FT OR HIGHER, USE 348 GAL PER ACRE (8 GAL/1000 SQ FT) FOR ANCHORING.

REFER TO THE 1994 MARYLAND STANDARDS AND SPECIFICATIONS FOR SOIL EROSION AND SEDIMENT CONTROL FOR RATE AND METHODS NOT COVERED.

SEDIMENT CONTROL

**DETAILS** 

BLOCK NO

600' SCALE MAP NO.

#### SEQUENCE OF CONSTRUCTION

DBTAIN A GRADING PERMIT AND ALL OTHER APPLICABLE PERMITS NECESSARY TO COMMENCE CONSTRUCTION ACTIVITIES.

CONTACT THE HOWARD COUNTY SEDIMENT CONTROL INSPECTOR AT 410-313-1855

48 HOURS PRIOR TO COMMENCING CONSTRUCTION. CLEAR WHERE NECESSARY TO INSTALL REQUIRED EROSION AND SEDIMENT CONTROL

INSTALL PERIMETER SEDIMENT CONTROL DEVICES, STABILIZED CONSTRUCTION

DAY 5 - DAY 12 ENTRANCES, SILT FENCE, SUPER SILT FENCE, PERIMETER DIKES AND INLET

DAY 13 - DAY 20 INSTALL SEDIMENT TRAP WITH INFLOW PROTECTION

PROTECTION ON EXISTING INLET.

UPON APPROVAL OF THE SEDIMENT CONTROL INSPECTOR, BEGIN GRADING FOR STAGE I CONSTRUCTION. GRADE STAGE ONE TO SUBGRADE IN SUCH A WAY THAT INSURES POISTIVE DRAINAGE TO THE SEDIMENT TRAP AND SUPER SILT FENCE. AS THE GRADE OF THE RDADWAY PROGRESSES, INSTALL A TEMPORARY SWALE NEAR STA. 14+00 TO DIRECT FLOW TO THE TRAP.

STABLIZE ALL SIDE SLOPES IN ACCORDANCE WITH THE TOPSOIL & PERMANENT SEEDING NOTES AS SOON AS POSSIBLE AFTER FINAL GRADE IS ACHIEVED.

DAY 56 - DAY 77 INSTALL STORM DRAIN, INLETS, CURB & GUTTER, AND REQUIRED INLET PROTECTION. WITH THE APPROVAL OF THE SEDIMENT CONTROL INSPECTOR, REMOVE THE DAY 77 - DAY 87 TEMPORARY SWALE AND INSTALL THE STAGE I BASE COURSES FOR THE ROADWAY

GRADE STAGE II AREA TO SUBGRADE, INSTALL CURB & GUTTER, AND INSTALL ROADWAY BASE COURSES. STABLIZE SIDE SLOPES IN ACCORDANCE WITH TOPSOIL & PERMANENT SEEDING NOTES AS SOON AS POSSIBLE.

REMOVE REMAINING EXISTING PAVING, FINISH REMIANING CONSTRUCTION. DAY 110 - DAY 140 PERFORM FINE GRADING AND STABLIZE ALL REMAINING DISTURBED AREAS IN ACCORDANCE WITH TOPSOIL & PERMANENT SEEDING NOTES AS SOON AS POSSIBLE

> WHEN THE WORK AREA IS COMPLETELY STABILIZED, INSTALL SPLITTER DEVICES AND PERFORM FINAL GRADING AND CONSTRUCTION OF THE WATER QUALITY

STABILIZE REMAINING DISTURBED AREAS IN ACCORDANCE WITH TOPSOIL & PERMANENT SEEDING NOTES AS SOON AS POSSIBLE.

WITH THE APPROVAL OF THE SEDIMENT CONTOL INSPECTOR, REMOVE REMAINING DAY 175 - DAY 180 SEDIMENT CONTROL DEVICES AND STABLILZE REMAINING AREAS.

EARTHWORK SUMMARY

CLASS I EXCAVATION

TOPSOIL REMOVED UNDER FILL 140 C.Y. TOTAL CLASS I EXCAVATION 24,676 C.Y.

24,536 C.Y.

25 C.Y.

0 C.Y.

CLASS 2 EXCAVATION TOTAL CLASS 2 EXCAVATION

EXCAVATION AVAILABLE FOR EMBANKMENT 20,040 C.Y. TOTAL CLASS I EXCAVATION

140 C.Y. TOPSOIL REMOVED UNDER FILL UNUSEABLE EXCAVATION DORSEY RUN RD. S. LINK 12,070 C.Y.

12,466 C.Y. CUT ADJUSTED 10,596 C.Y. CUT DENSIFIED (85%)

CLASS 2 EXCAVATION AVAILABLE FOR EMBANKMENT

TOTAL EXCAVATION AVAILABLE FOR **EMBANKMENT** 12,466 C.Y. EMBANKMENT REQUIRED

2,038 C.Y. EMBANKMENT - INCLUDING TEMPORARY ROAD 140 C.Y. REFILL FOR TOPSOIL REMOVED UNDER FILL 2.178 C.Y. TOTAL EMBANKMENT REQUIRED 12,466 C.Y. EXCAVATION AVAILABLE FOR EMBANKMENT

0 C.Y. COMMON BORROW REQUIRED SUMMARY OF QUANTITIES 24,536 C.Y. CLASS I EXCAVATION CLASS 2 EXCAVATION

25 C.Y. 0 C.Y. COMMON BORROW THE ENGINEER:

I/WE CERTIFY THAT THIS PLAN FOR EROSION AND SEDIMENT CONTROL

EPRESENTS A PRACTICAL AND WORKABLE PLAN BASED ON MY PERSONAL KNOWLEDGE OF THE SITE CONDITIONS AND THAT IT WAS PREPARED IN CCORDANCE WITH THE REQUIREMENTS OF THE HOWARD COUNTY SOIL ONSERVATION DISTRICT.

NOTNEER: MALINY GUPTA GLUECK P.E. 27720

Y THE DEVELOPER:

/WE CERTIFY THAT ALL DEVELOPMENT AND CONSTRUCTION WILL BE DONE COORDING TO THIS PLAN, AND THAT ANY RESPONSIBLE PERSONNEL INVOLVED I HE CONSTRUCTION PROJECT WILL HAVE A CERTIFICATE OF ATTENDANCE AT A ARYLAND DEPARTMENT OF THE ENVIRONMENT APPROVED TRAINING PROGRAM OR THE CONTROL OF SEDIMENT AND EROSION BEFORE BEGINNING THE PROJECT ALSO AUTHORIZE PERIODIC ON-SITE INSPECTION BY THE HOWARD SOIL

Elizabeth a. Calva PROJECT ENGINEER AND WATERSHED MANAGEMENT DIVISION

PLAN IS APPROVED FOR SOIL EROSION AND SEDIMENT

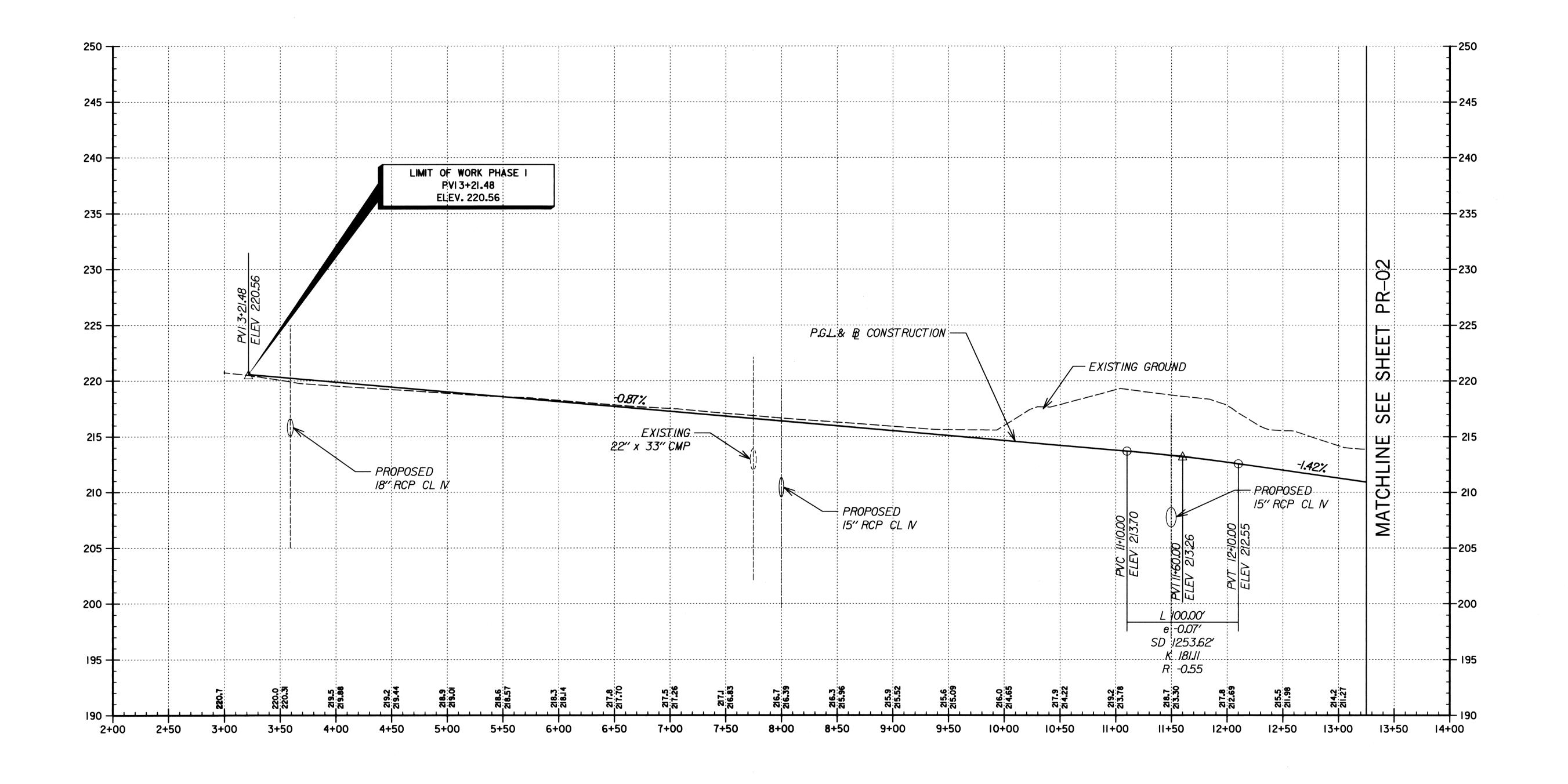
HNICAL REQUIREMENTS.

DORSEY RUN ROAD SOUTH LINK

CAPITAL PROJECT NO. J-4110

SCALE SHOWN

SHEET



9/4/02 F OF MARY DEPARTMENT OF PUBLIC WORKS
HOWARD COUNTY, MARYLAND Phoenix - Nolan Joint Venture CHIEF, TRANSPORTATION AND SPECIAL PROJECTS DIVISION Faz: (410) 247-9397

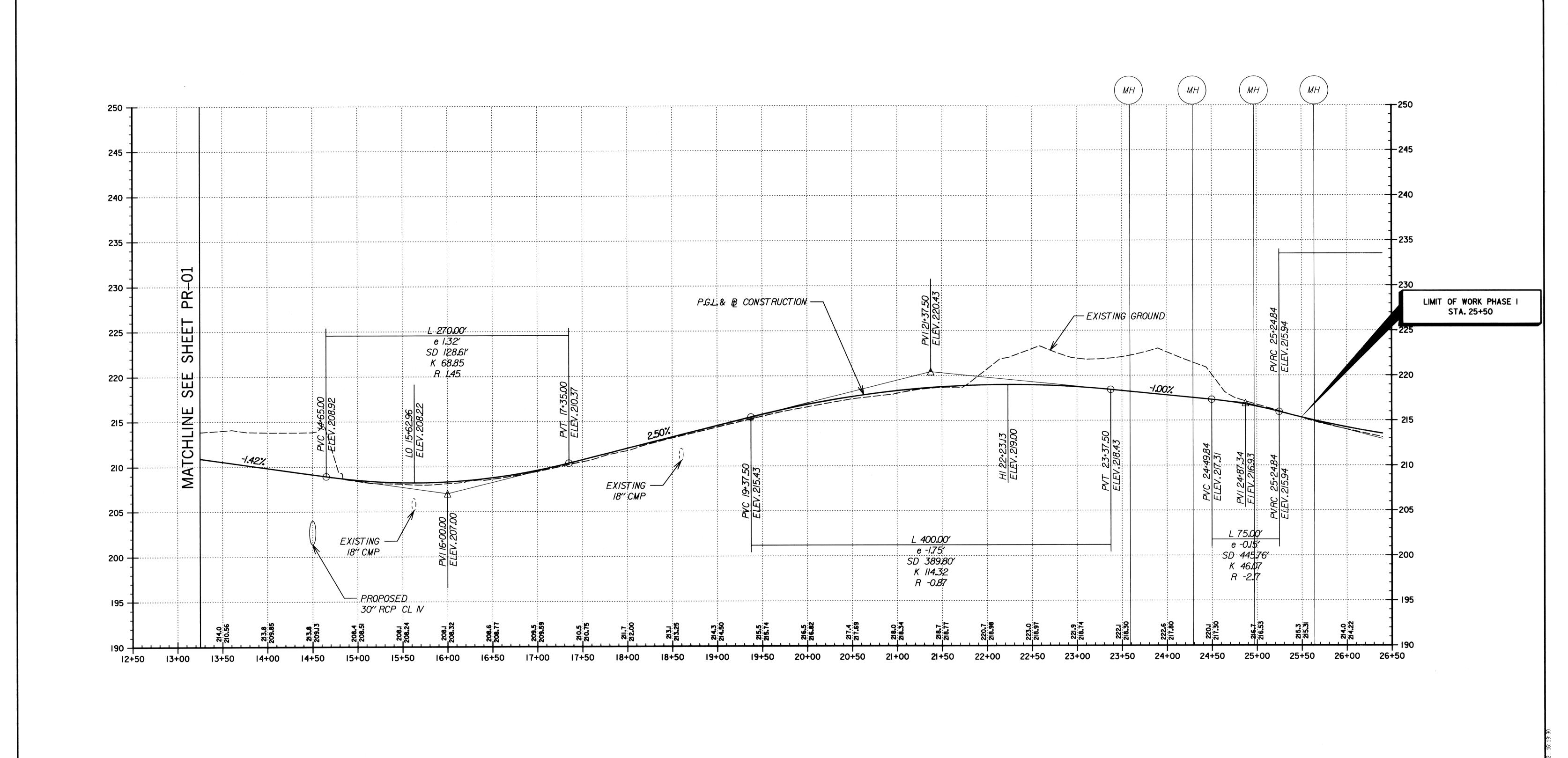
J.R.H.						
D.R.B.					PROFILE OF DRRS	
					PROFILE OF DRKS	
. •	BY	NO.	REVISION	DATE	600' SCALE MAP NO. BLOCK NO.	

DORSEY RUN ROAD SOUTH LINK PHASE 1 CAPITAL PROJECT NO. J-4110

PR-01

SCALE AS SHOWN

SHEET <u>14</u> OF <u>30</u>



DEPARTMENT OF PUBLIC WORKS
HOWARD COUNTY, MARYLAND CHIEF, TRANSPORTATION AND SPECIAL PROJECTS DIVISION

Phoenix - Nolan Joint Venture

Fax: (410) 247-9397

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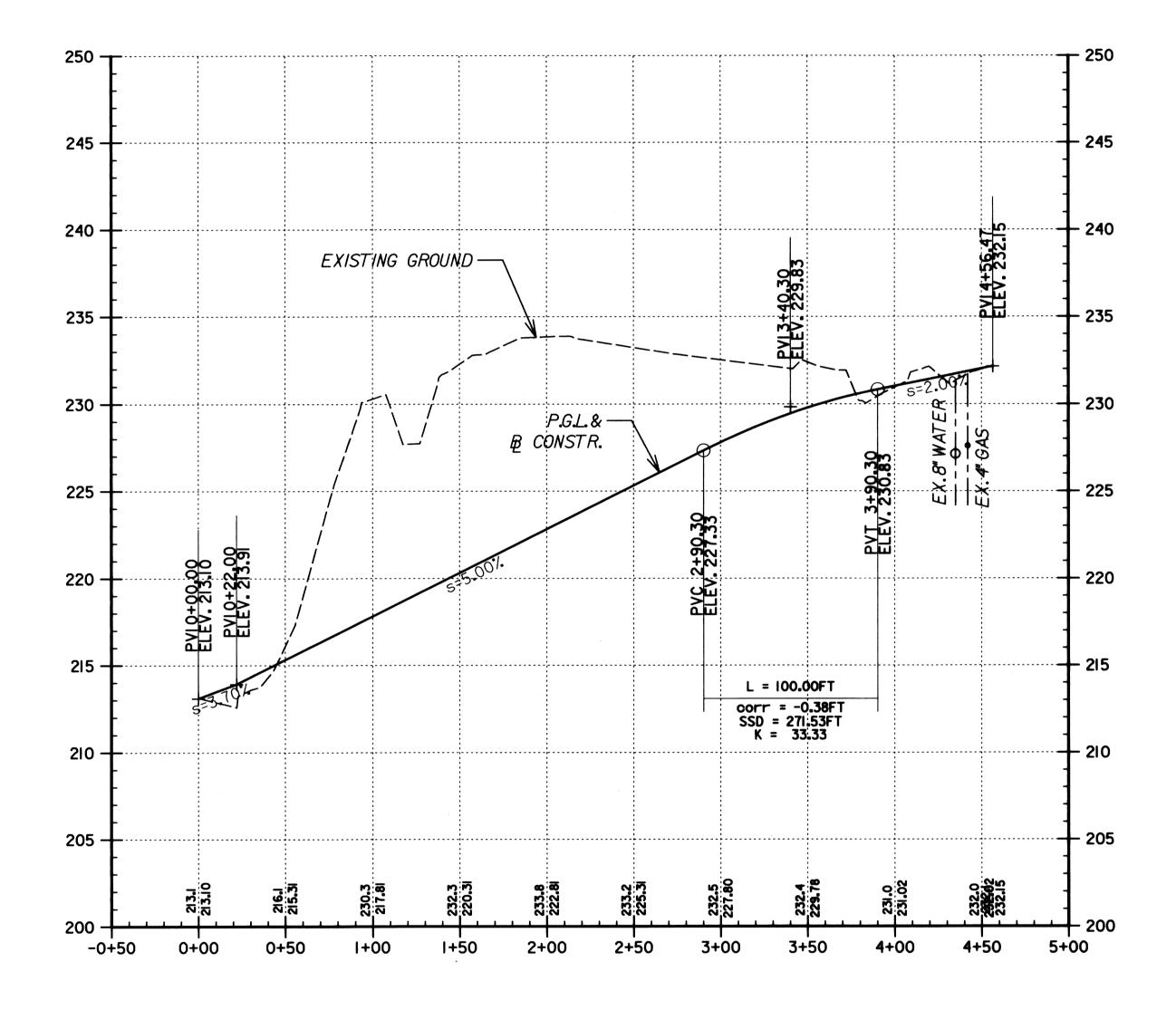
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 DATE:	BY	NO.	REVISION	DATE	600' SCALE MAP NO.
5.475					
CHK:					
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DRN: D.R.B.					PROFILI
DES: J.R.H.					

PROFILE OF DRRS DORSEY RUN ROAD SOUTH LINK PHASE 1 CAPITAL PROJECT NO. J-4110

BLOCK NO.

SCALE AS SHOWN SHEET 5 15 OF 30

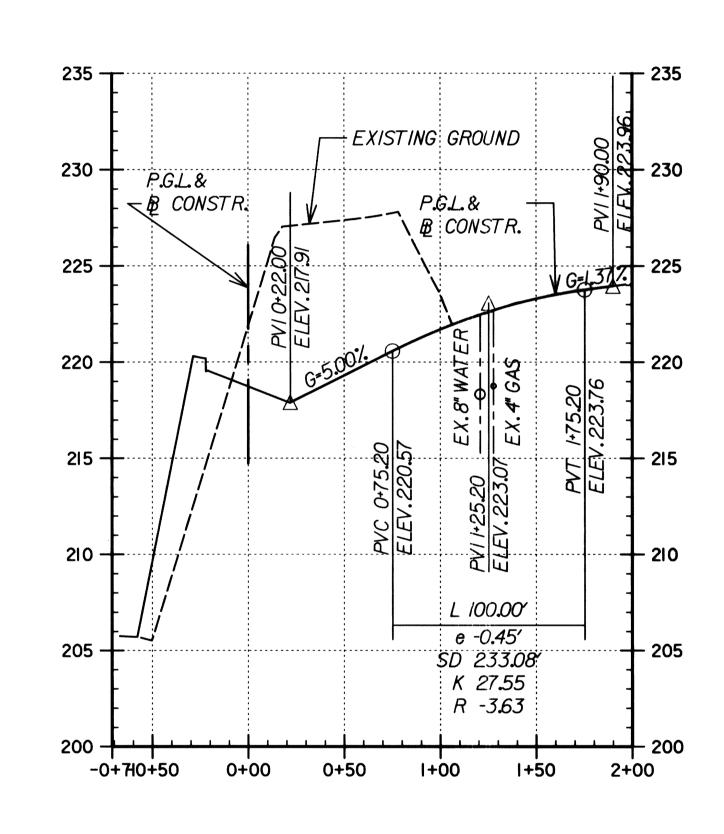
PR-02



GIANT ROAD ENTRANCE

SCALE: HORIZ: | = 50'

VERT: | = 5'



OLD DORSEY RUN ROAD

SCALE: HORIZ: I' = 50'
VERT: I' = 5'

DEPARTMENT OF PUBLIC WORKS

HOWARD COUNTY, MARYLAND

DIRECTOR OF PUBLIC WORKS

DATE

CHIEF, TRANSPORTATION AND
SPECIAL PROJECTS DIVISION

DEPARTMENT OF PUBLIC WORKS

HOWARD COUNTY, MARYLAND

GREAT OF PUBLIC WORKS

PATE

CHIEF, BUREAU OF HIGHWAYS

DATE

CHIEF, BUREAU OF HIGHWAYS

DATE

Phoenix - Nolan Joint Venture

1420-A Joh Avenue
Suite A
Baltimere, Maryland 21227

9/4/02 OF MARY OF MARY

DRN: D.R.B.

CHK:

BY NO. REVISION

PROFILE
AND OLD D

REVISION

DATE 600' SCALE MAP NO.

PROFILE OF GIANT ROAD AND OLD DORSEY RUN ROAD

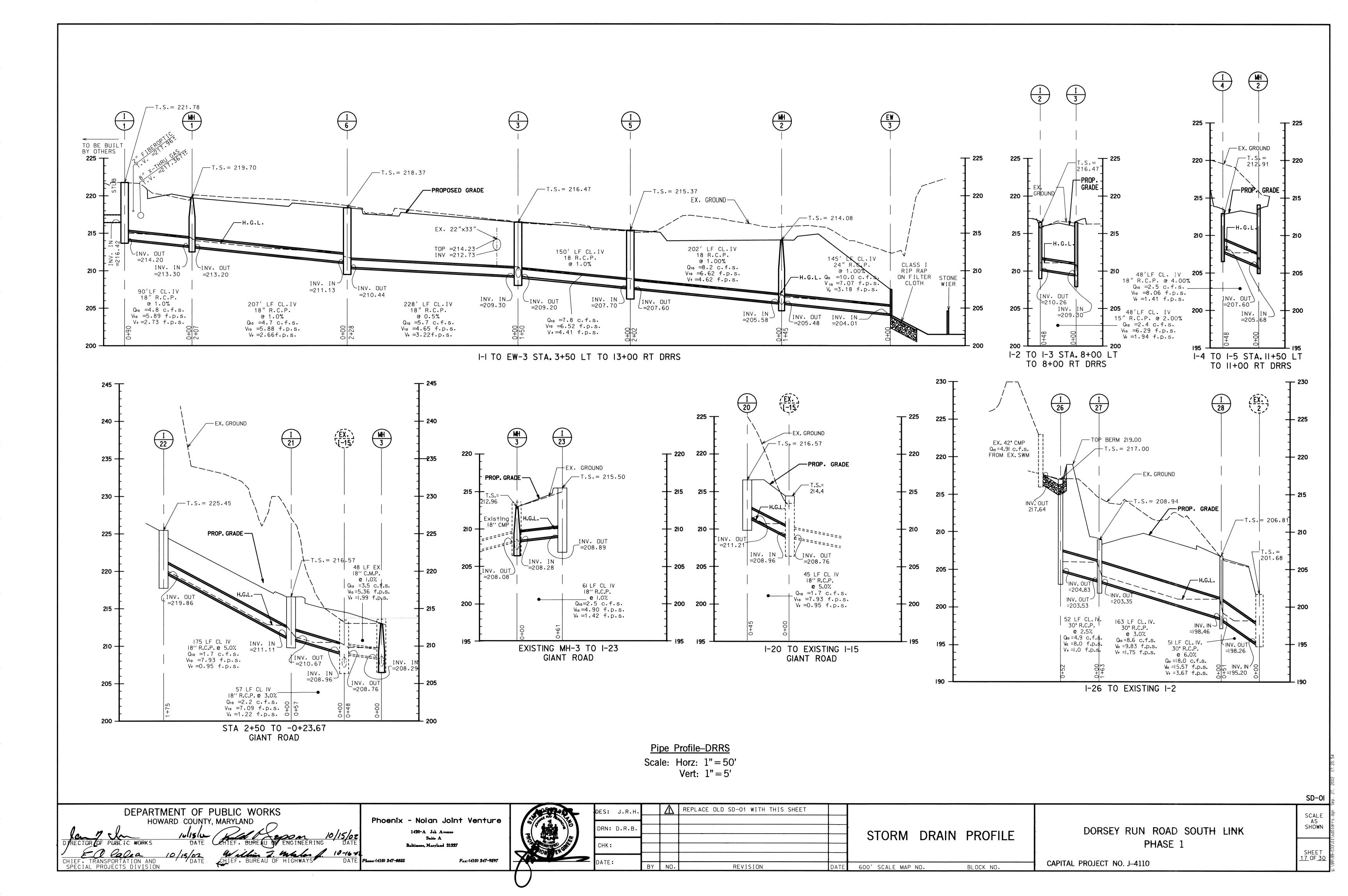
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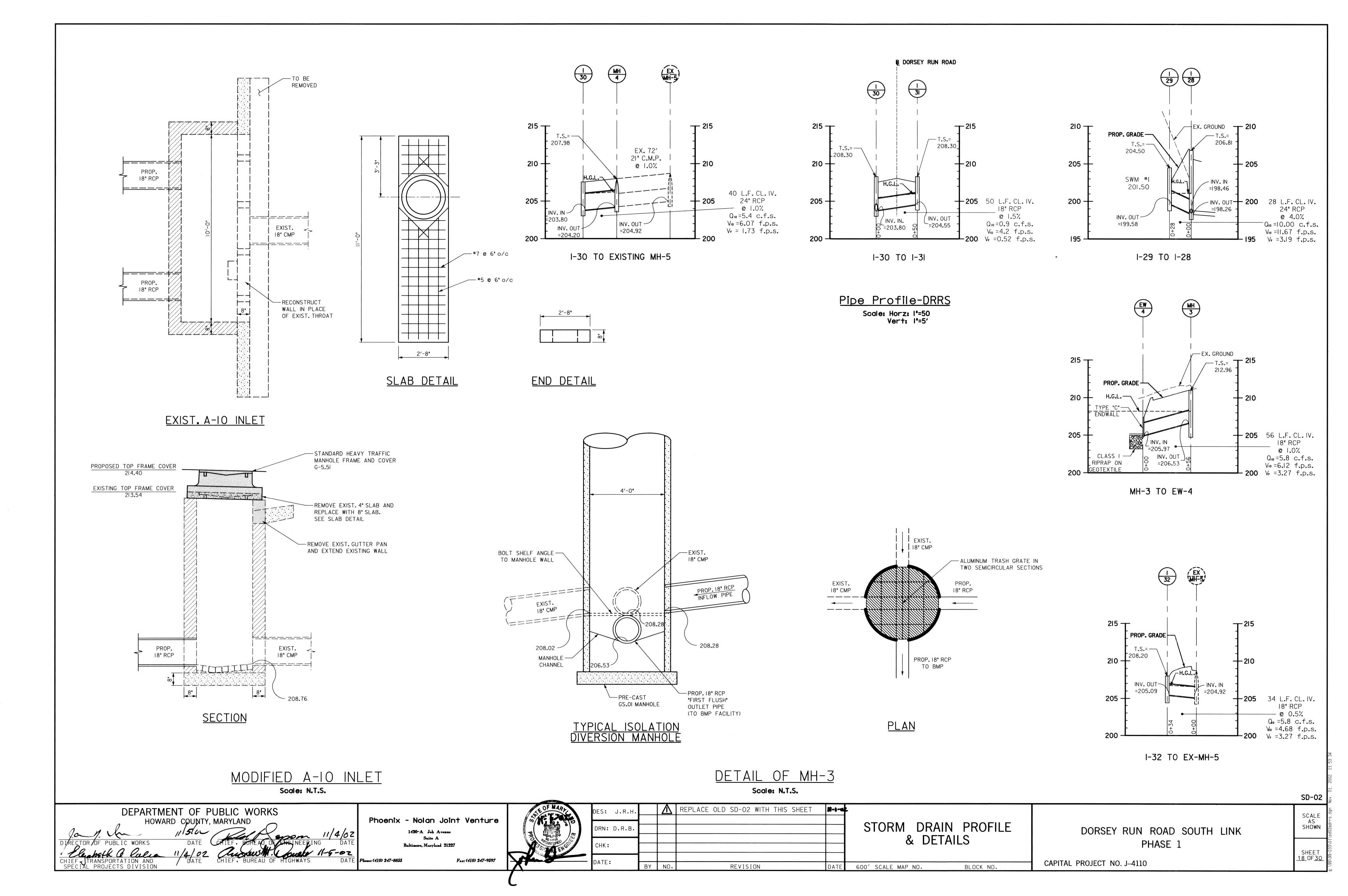
DORSEY RUN ROAD SOUTH LINK

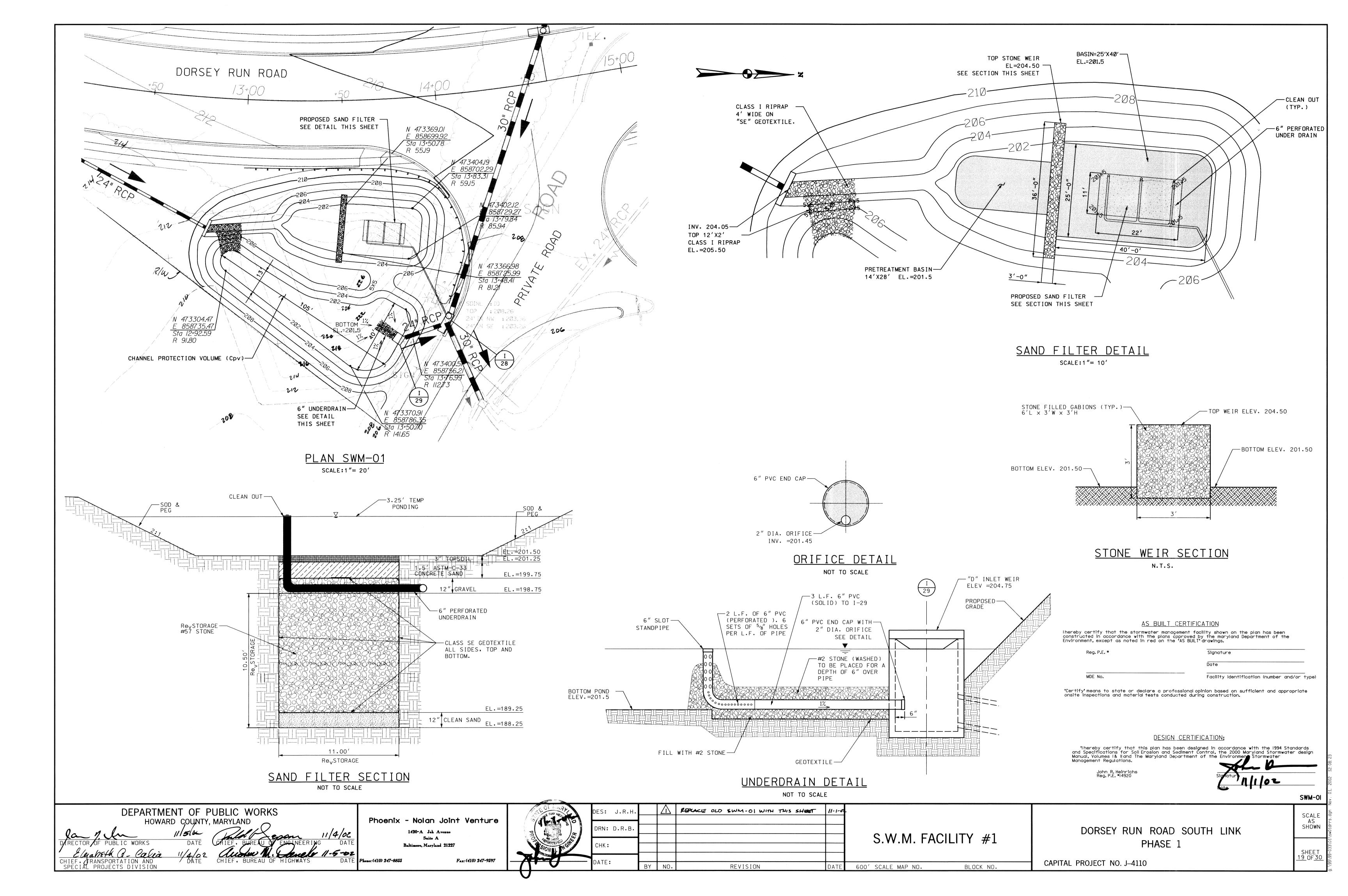
CAPITAL PROJECT NO. J-4110

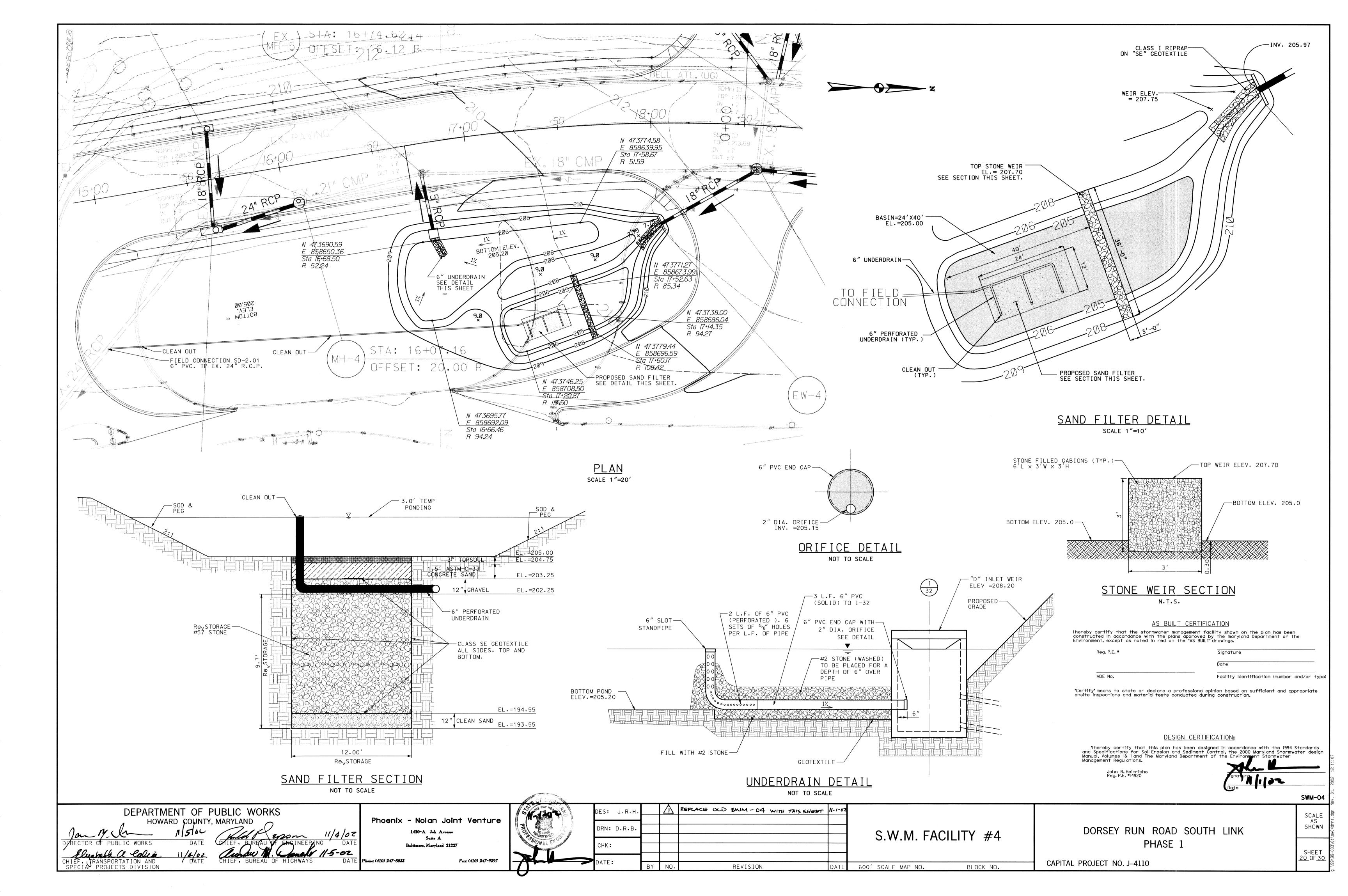
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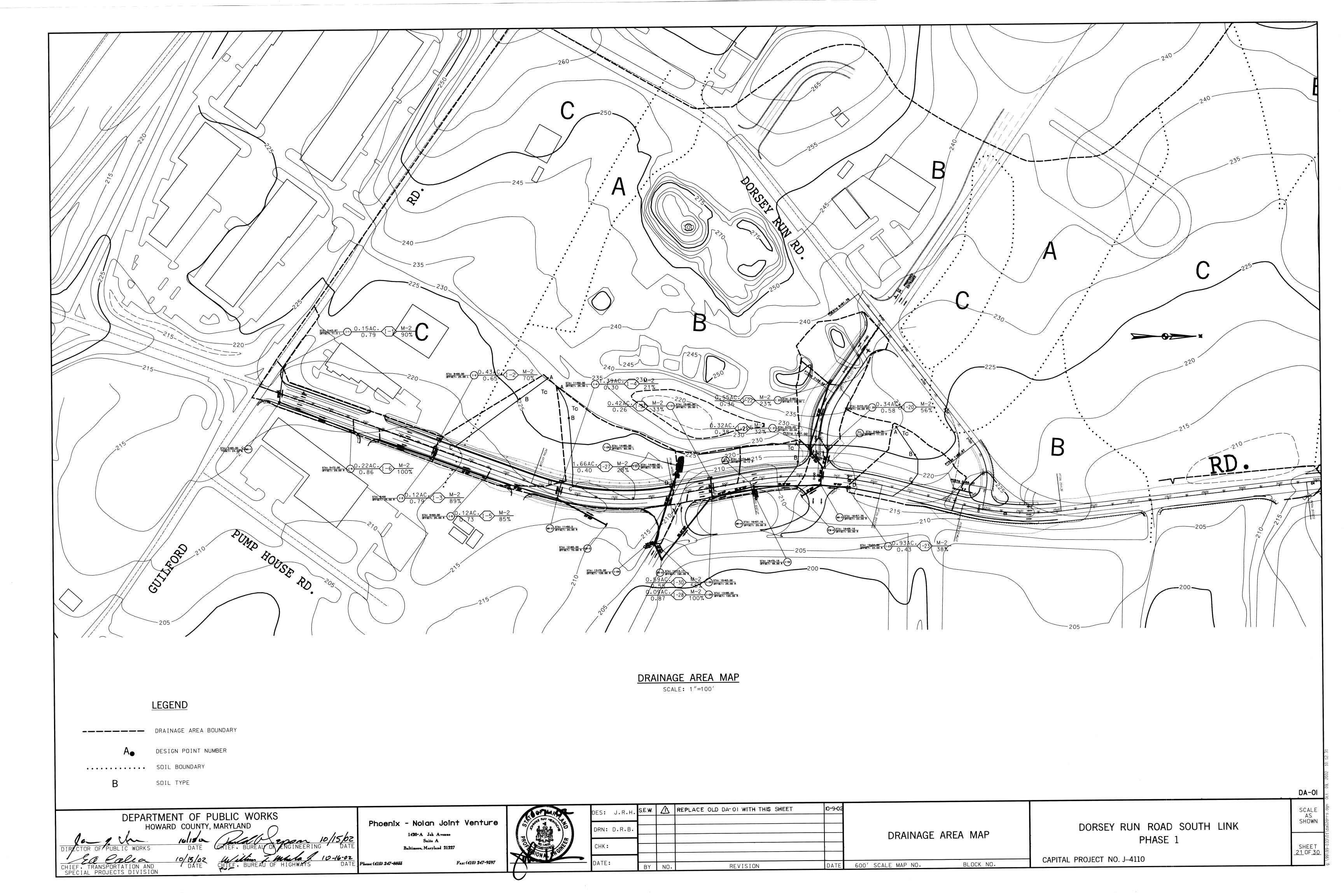
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16 OF 30

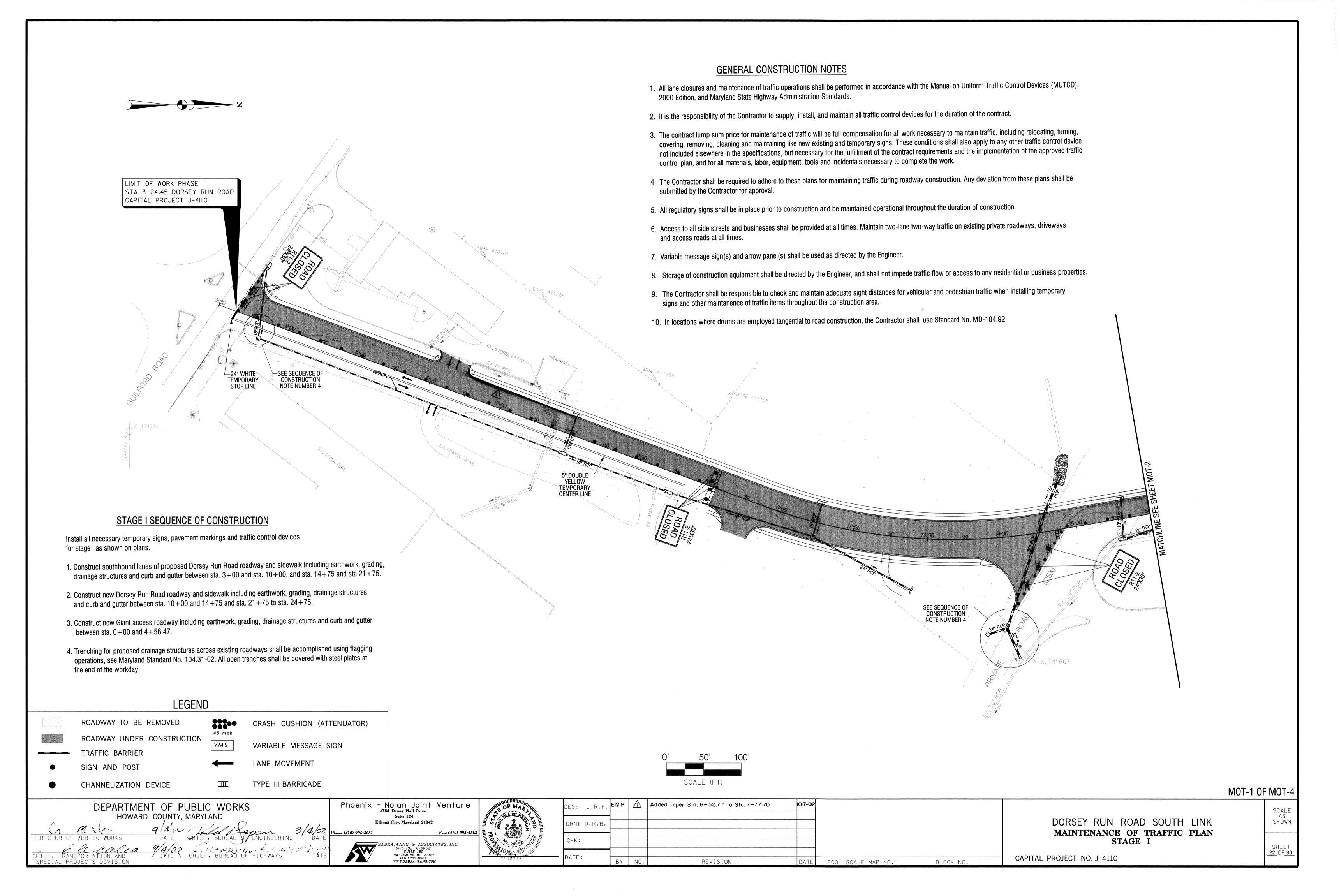


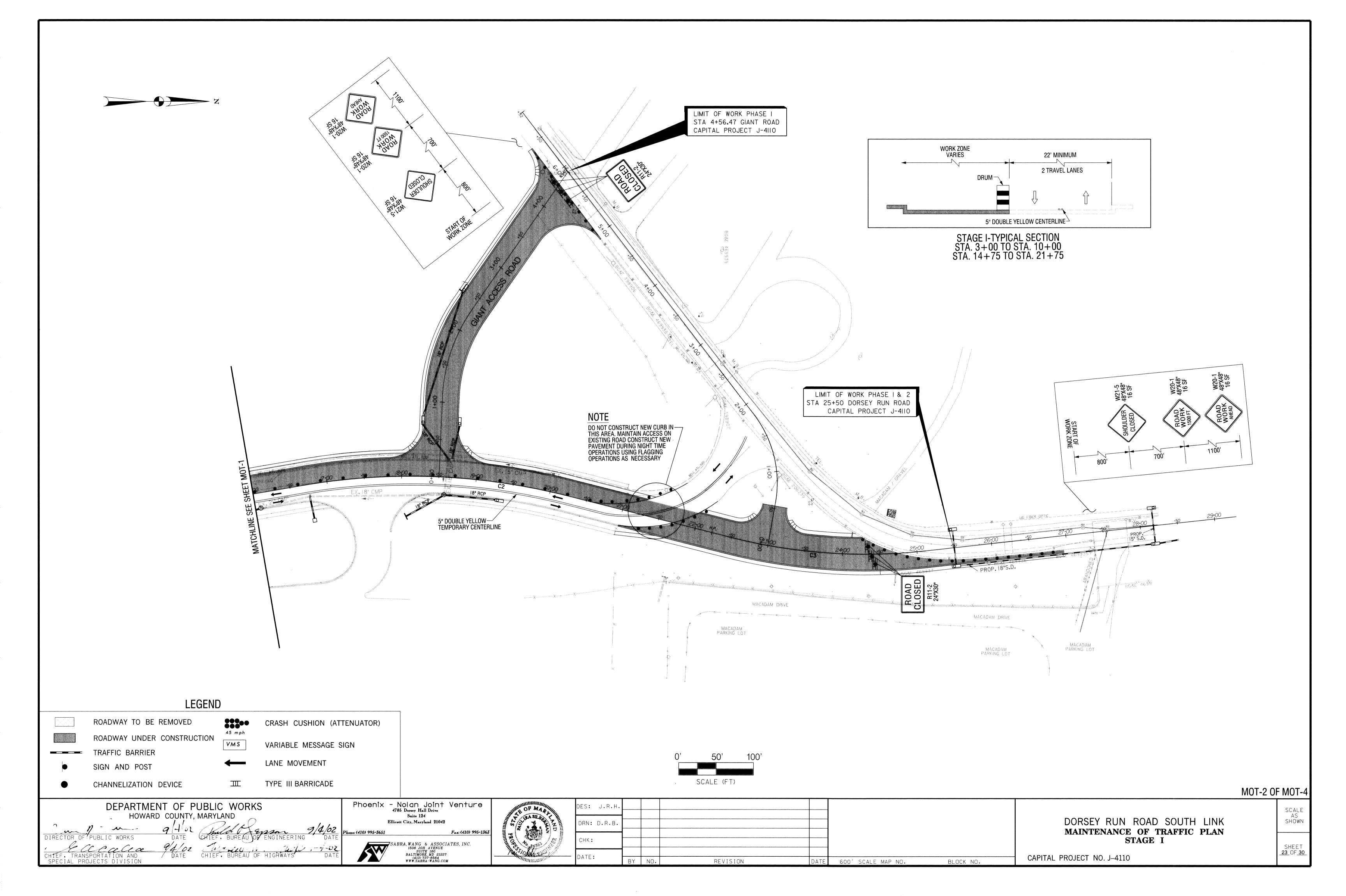


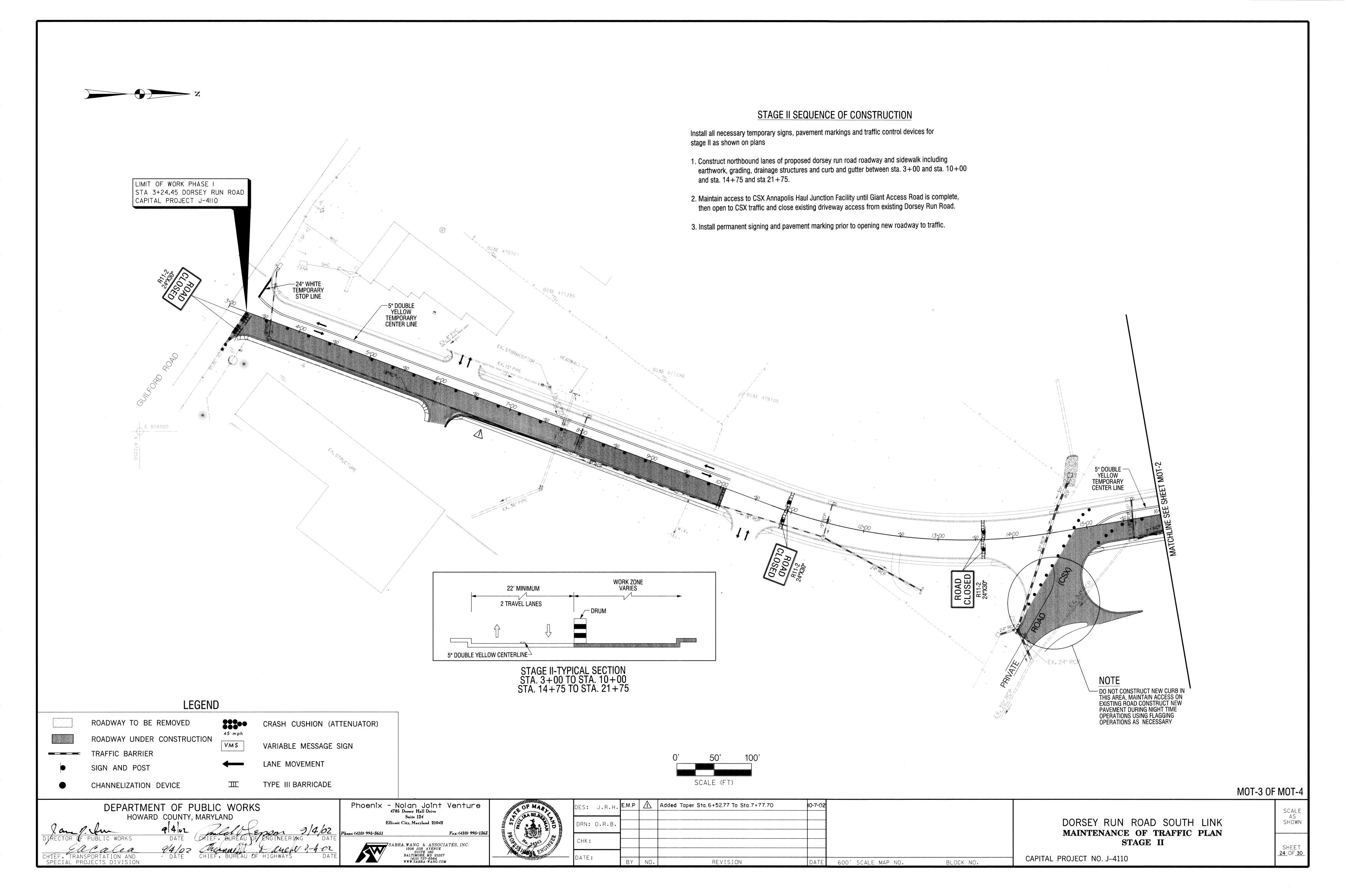


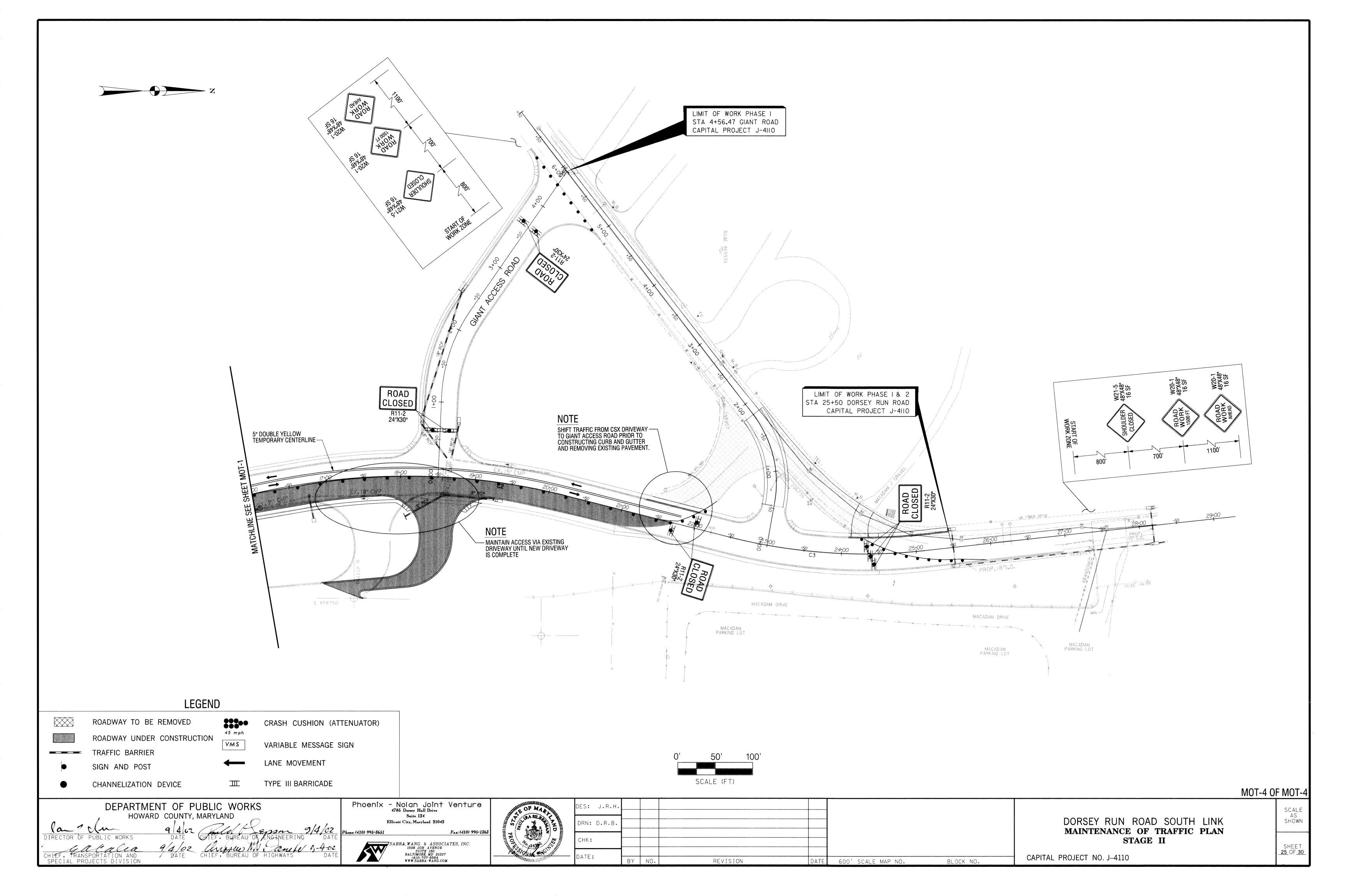




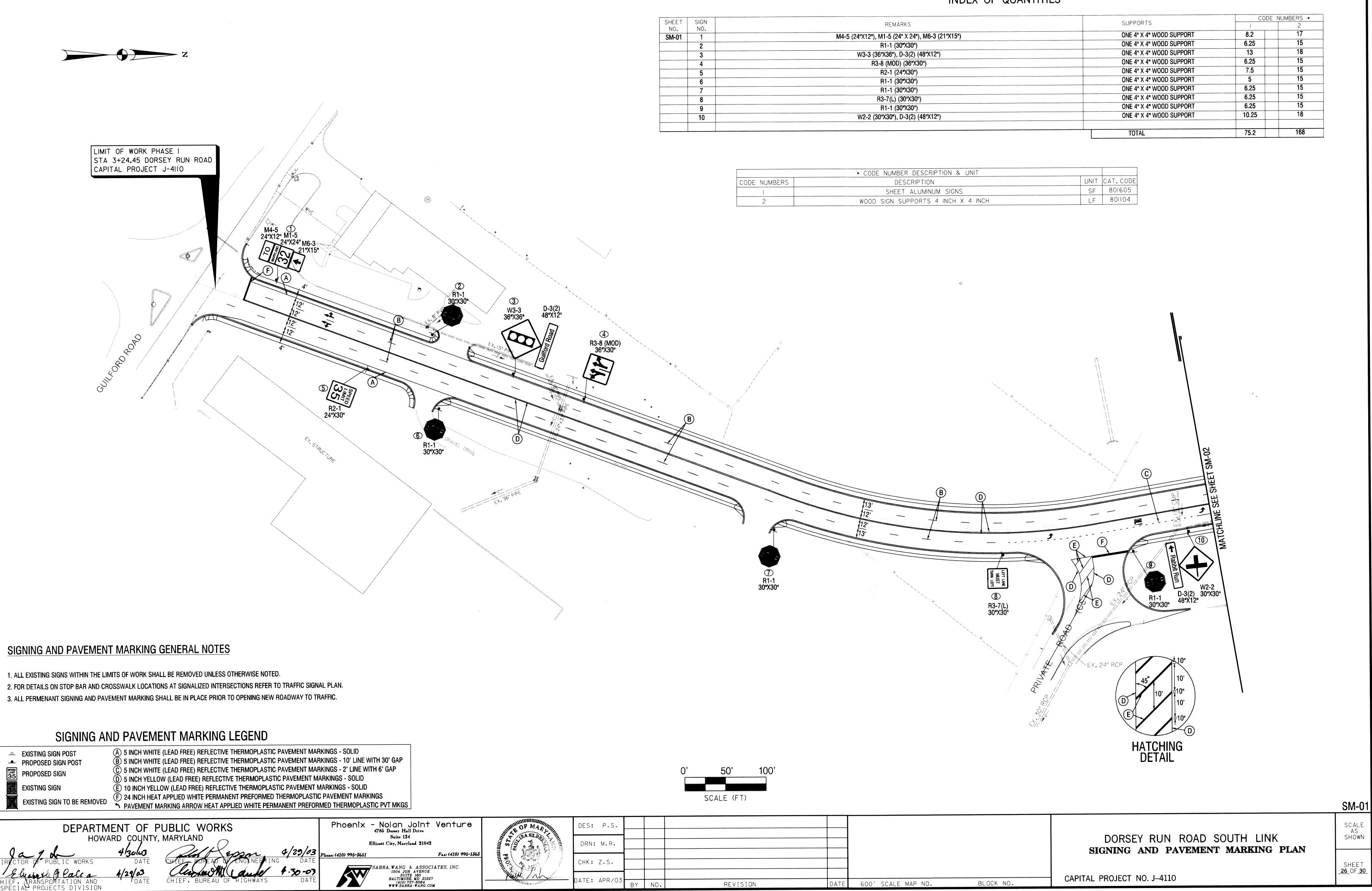


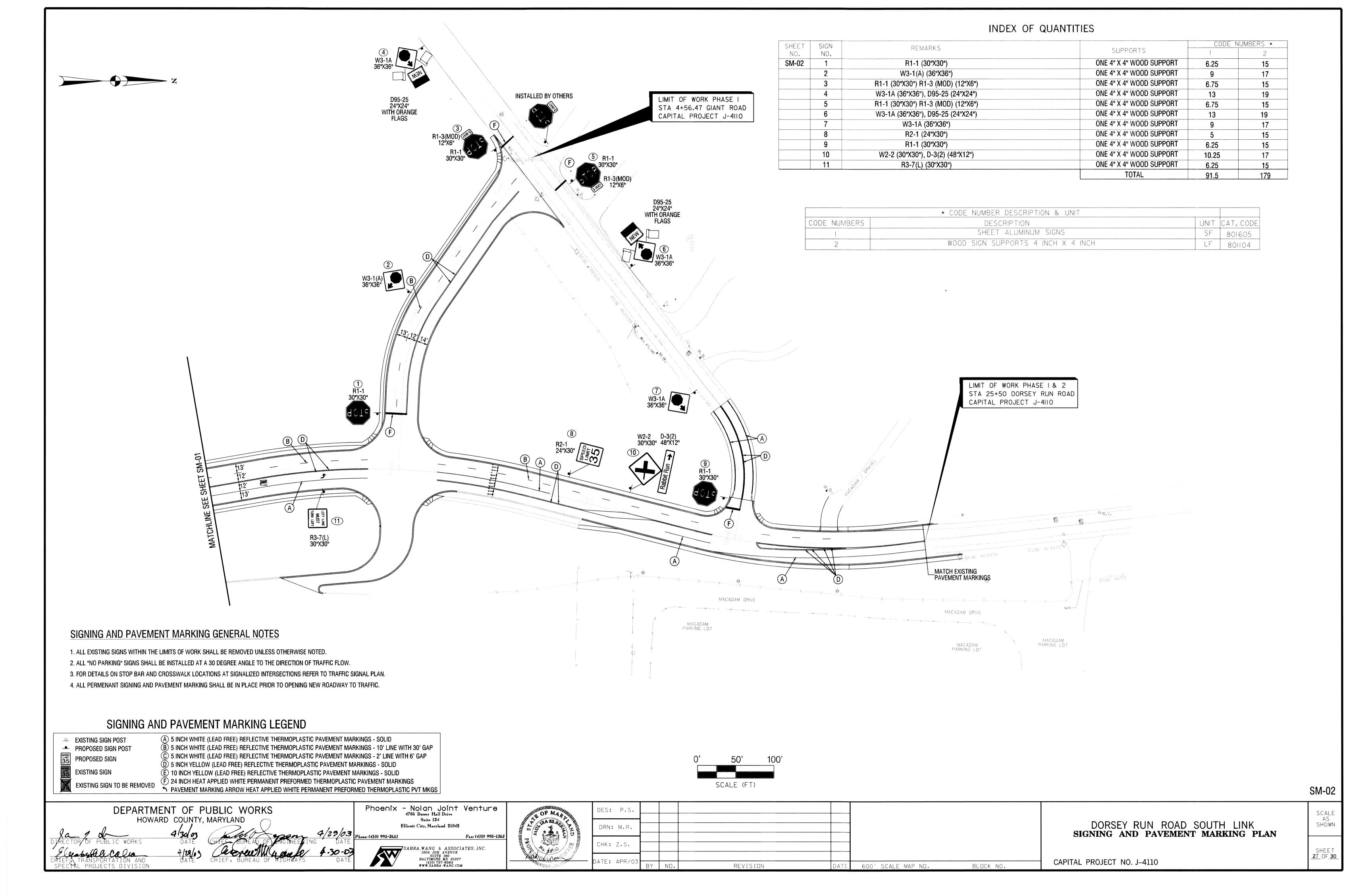


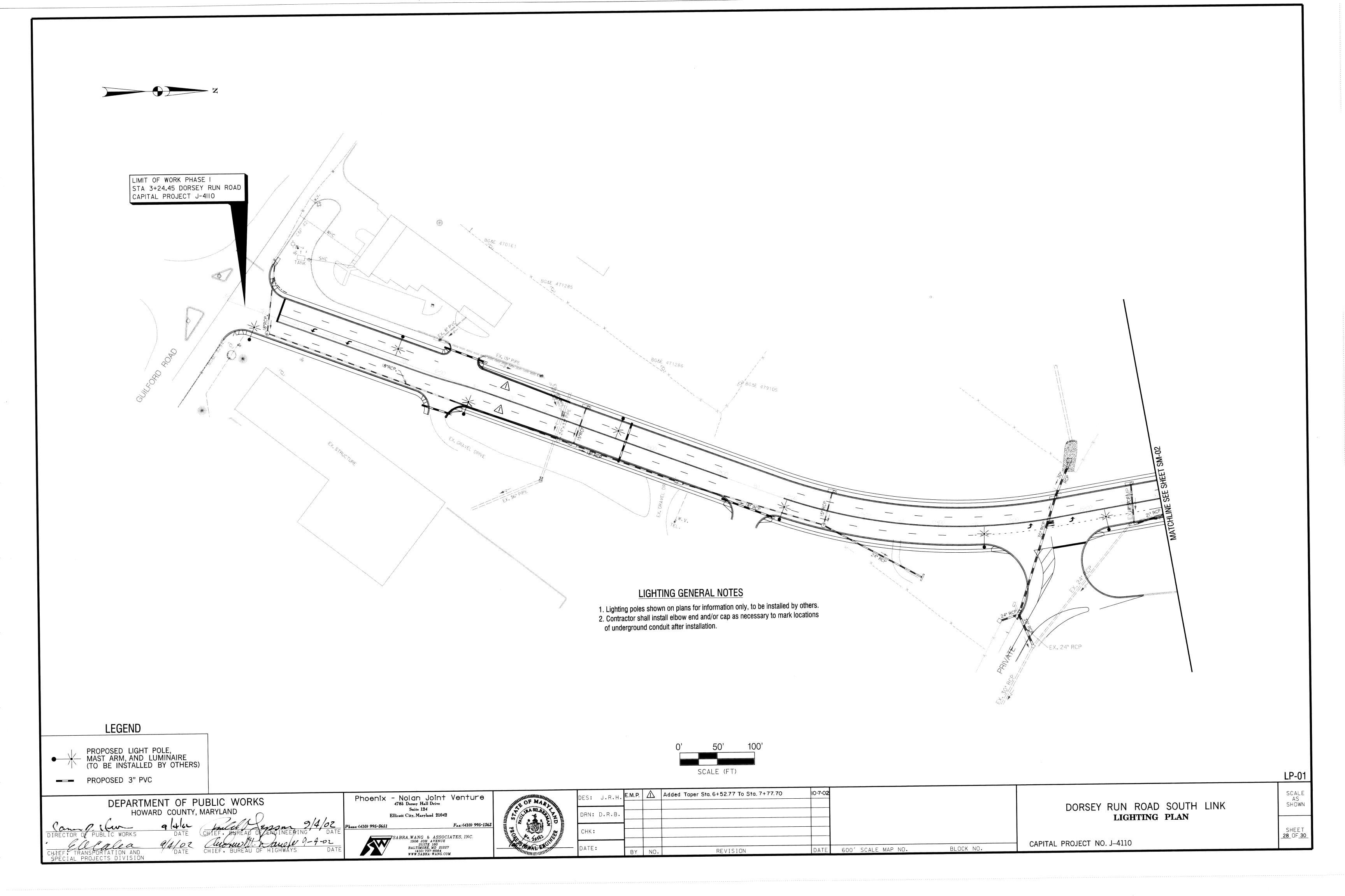


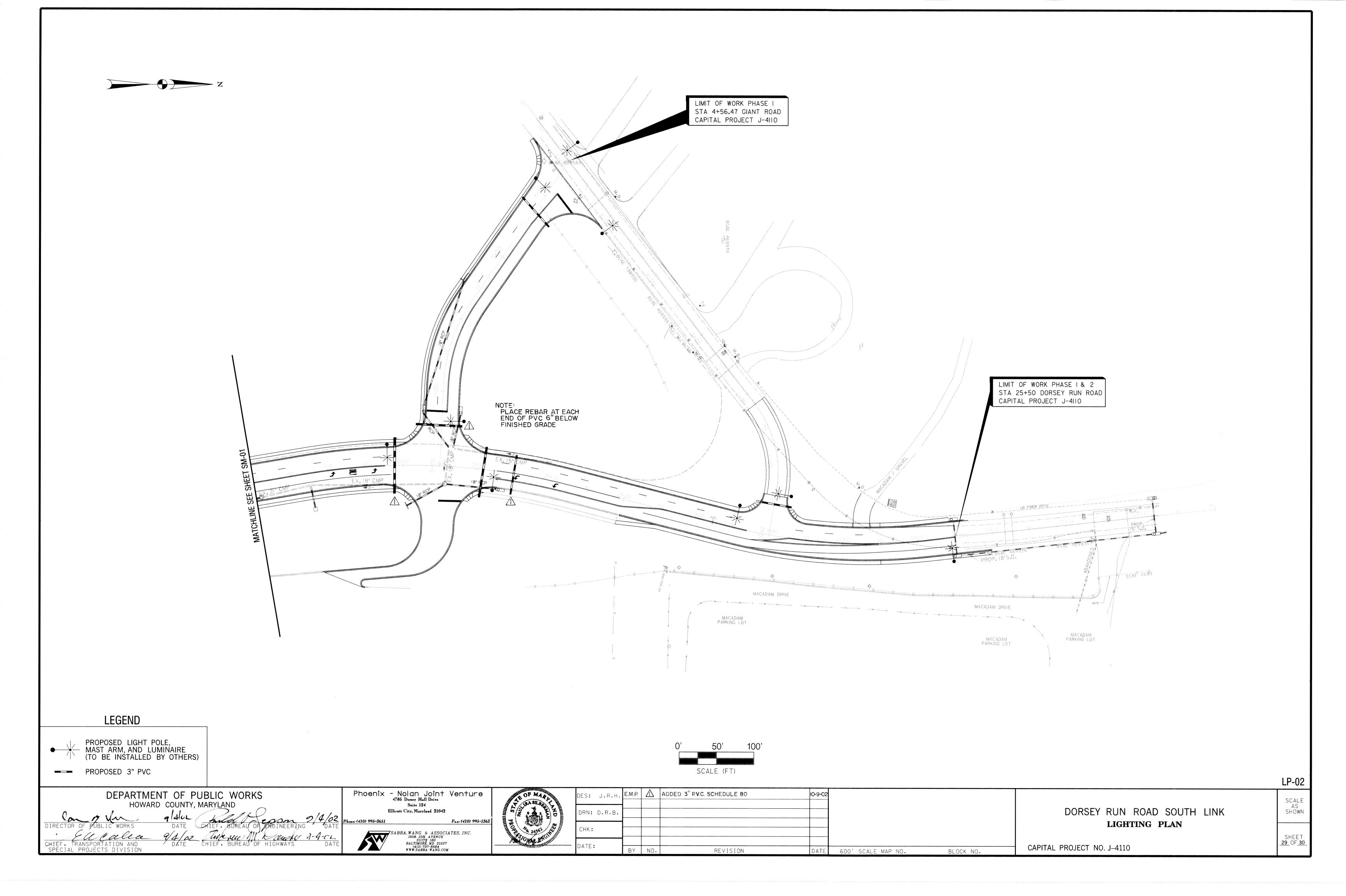


#### INDEX OF QUANTITIES









#### CAPITAL PROJECT NO. J-4110, PHASE 1 PAVEMENT ELEVATIONS

T. HINGE POINT	LT. TOP OF CURB ELEV.	LT. GUTTER ELEVATION	LT. EDGE OF PAV'T	LT. PAV'T SLOPE IN %		CENTER STA.	LINE ELEV.	RT. PAV'T SLOPE IN %	RT. EDGE OF PAV'T	RT. GUTTER ELEVATION	RT. TOP OF CURB ELEV.	RT. HINGE POINT	CENTERLINE STATION	LT.&RT. EL GUTTER
						3 +00.00 3 +10.00							300 310	
					POT	3 +20.00 3 +21.48	220.56						320 321.48	
			220.92 220.83	1.38 <u>00</u> 1.2135		3 +24.45 3 +30.00	220.53 220.49	-1 <i>3</i> 8 -1 <i>5</i> 465	220 <b>.</b> 14 220 <b>.</b> 06				324,45 330	
			220,66 220,63	0 <b>.</b> 9135	RT/CR	3 +40.00 3 +41.30	220,40	-1.8465 -1.8855	219.88 219.86				340 341.3	,
			220.54	0.7599		3 +45.12	220.33	-2,0000	219,77	219.73	220.33	220.46	345.12	,
			220.48 220.31	0.3135		3 +50.00 3 +60.00	220,22	- 2 - 2	219 <b>.</b> 75 219. <b>6</b> 6	219.71 219.62	220 <i>3</i> 1 220 <i>2</i> 2	220.44 220.35	350 360	
220,82	220.69	220.09	220 <b>.</b> 14 220 <b>.</b> 13	0.0135 -0.0105		3 +70.00 3 +70.80	220 <b>.</b> 1 220 <b>.</b> 13	- 2 - 2	219.58 219.57	219 <i>5</i> 4 219 <i>5</i> 3	220 <b>.</b> 14 220 <b>.</b> 13	220,27 220,26	370 370.8	
220.66 220.48	220.53 220.35	219.93 219.75	219.97 219.80	-0,2865		3 +80.00 3 +90.00	220.05	- <u>2</u> - 2	219.49 219.40	219.45 219.36	220.05	220.18 220.09	380 390	
220.321	220,19	219.59	219.63	-0,8864		4+00.00	219,88	- 2 - 2	219.32	219 <b>,2</b> 81	219,881	220,01	400	
220.15 219.97	220.02 219.84	219.42 219.24	219.46 219.28	-1.1864 -1.4864		4 +10.00 4 +20.00	l 219 <b>.</b> 701	-2	219.23 219.14	219 <b>.</b> 19 219 <b>.</b> 10	219 <b>.</b> 79 219.70	219.92 219.83	410 420	
219.81 219.66	219.68 219.53	219.08 218.93	219.12 218.97	-1.7864 -2.0000		4 +30.00 4 +37.12	219.53	- 2 - 2	219.06 218.97	218.93	219.62 219.53	219 <b>.</b> 75 219 <b>.</b> 66	430 437 <b>.</b> 12	
219.66 219.57	219.53 219.44	218.93 218.84	218.97 218.88	-2 -2		4 +40.00 4 +50.00	219.53 219.44	- 2 - 2	218.97 218.88	218.93 218.84	219.53 219.44	219.66 219.57	440 450	
219.48 219.21	219.35 219.08	218.75 218.48	218 <b>.</b> 79 218 <b>.</b> 52			4 +60.00 4 +70.00	219.44 219.35 219.08	- 2 - 2	218.79 218.52	218.75 218.48	219.44 219.35 219.08	219,48 219,21	460 470	
219.31	219 <b>.</b> 18	218.58	218.62	-2		4 +80.00	219.18	- 2	218.62 218.53	218.581	219 <b>.</b> 18	219.31	480	
219 <i>2</i> 2 219.14	219.09 219.01	218.49 218.41	218.53 218.45	-2 -2	***************************************	4 +90.00 5 +00.00	219.01	- 2 - 2	218.45	218.49 218.41	219.09 219.01	219.22 219.14	490 500	
219.05 218.96	218.92 218.83	218.32 218.23	218 <i>3</i> 6 218 <i>2</i> 7	-2		5 +10.00 5 +20.00	218.92 218.83	- 2 - 2	218.36 218.27	218.32 218.23	218.92 218.83	219.05 218.96	510 520	
218.87 218.79	218.74 218.66	218.14 218.06	218.18 218.10	-2		5 +30.00 5 +40.00	218.74 218.66	- <u>2</u> - 2	218.18 218.10	218.14 218.06	218.74 218.66	218.87 218.79	530 540	
218.70	218.57	217.97	218.01	- <u>2</u> - 2		5 +50.00	218.57	- <u>2</u>	218,01	217.97	218.57	218.70	550	
218.61 218.53	218.48 218.40	217.88 217.80	217.92 217.84	- <u>2</u>		5 +60.00 5 +70.00	218.48 218.40	- 2 - 2	217.92 217.84	217.88 217.80	218.48 218.40	218.61 218.53	560 570	
218.46 218.44	218 <i>3</i> 3 218 <i>3</i> 1	217.71	217.75	-2		5 +80.00	218,31	- 2 - 2	217.75	217.73 217.71	218.33	218.46	580	
218.35 218.33	218 <i>2</i> 2 218 <i>2</i> 0	217.62 217.60	217.66 217.65	-2 -2		5 +90.00	218,22	- 2 - 2	217.66 217.65	217.62 217.60			590 593	27. 27.
			217.59 217.50	-2		6+000	l 218 <b>.</b> 141	-21	217.59 217.50	217.55 217.46			600 610	27. 27.
			217.42	-2		6 +10.00 6 +20.00	217.96	-2 -2	217.42 217.33	217.38 217.29	PORTING AND		620 630	27.
			217.33 217.25	- <u>2</u>		6 +30.00 6 +40.00	217.79	-2	217.25	217 <b>,2</b> 11			640	26
			217.17 217.16	-2	RT/CR	6 +50.00 6 +51.62	217.69	-2 -2	217.17 217.16	217.13 217.12	217.72	218.08	650 651.52	26
218.07 218.00	217.71 217.64	217.11 217.04	217 <b>.1</b> 5 217 <b>.0</b> 8	-2	LT/CR	6 +52.77 6 +60.00	217,68	-2 -2	217.15 217.08	217.11 217.04	217.71 217.64	218.07 218.00	652.77 660	
217.93 217.84	217.57	216.97	217.01	-2		6 +70.00 6 +80.00	217.53	-2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2	217.01 216.92	216.97 216.88	217.57 217.48	217.93 217.84	670 680	26.
217.75 217.67	21739 21731	216.79 216.71	216.83 216.75	-2 -2		6 +90.00	217.35 217.26	-2	216.83 216.75	216.79 216.71	21739 21731	217.75 217.67	690 700	25.
217.59 217.51	217.23 217.15	216.63 216.55	216.67	-2		7 + 10.00	l 217 <b>.</b> 181	- 2	216.67	216.63	217 <b>.</b> 231	217.59	710	25.
217 <b>.4</b> 21	217.06 216.98	216.46	216.59 216.50	2		$7 \pm 30 \Omega$	217.09 217.00	-2 -2	216.59 216.50	216.55 216.46	217 <b>.</b> 15 217.06	21759 21751 21742	720 730	24.
217.34 217.26	216.98 216.90	216.46 216.38 216.30	216.42 216.34	-2 -2		7 +40,00 7 +50,00	216.92 216.83	-2 -2	216.42 216.34	216.38 216.30	216.98 216.90 216.81	217.26	740 750	24.
217.17 217.10	216.81 216.74	216.21 216.14	216.25 216.18	- 2 - 2		7 +40.00 7 +50.00 7 +60.00 7 +70.00 7 +77.70	216.74 216.66	-2 -2	216.25 216.18	216,211	216.81 216.74	217.34 217.26 217.17 217.10 217.03	760 770	24.
217.03 217.01	216.67 216.65	216.07	216.11	-2	E/T	7 +77.70	216.59	-2 -2	216.111	216.07 216.05	216.67 216.65	217.03 217.01	777.7 780	24.
216.92	216.56	215.96	216,00	-2		7 +90.00	216.57 216.48	-2	216,00	215 <b>.</b> 961	216.56	216.92	790	
216.83 216.75	216.47 216.39	215.87 215.79	215.91 215.83	-2 -2 -2 -2 -2 -2		8 +00.00 8 +10.00	216.31	-2 -2	215.91 215.83	215.87 215.79	216.47 216.39	216.83 216.75	800 810	
216.66 216.57	216 <i>3</i> 0 216 <i>2</i> 1	215.61	215.74 215.65	-2 -2		8 +20.00 8 +30.00	216.13	- 2 - 2	215.74 215.65 215.57	215.70 215.61	216 <i>3</i> 0 216 <i>2</i> 1	216.66 216.57	830	
216.49 216.40	216.13 216.04	215.53 215.44	215.57 215.48	-2		8 +40.00 8 +50.00	216.05 215.96	-2 -2 -2 -2 -2 -2	215 <b>.4</b> 81	215.53 215.44	216.13 216.04	216.49 216.40	840 850	
216.31 216.22	215.95 215.86	215.35 215.26	215 <i>3</i> 9 215 <i>3</i> 0	- <u>2</u> -2		8 +60.00	215.87 215.78	-2 -2	215.39 215.30	215.35 215.26	215.95 215.86	216 <i>3</i> 1 216 <i>2</i> 2	860 870	
216.14 216.05	215.78	215.18	215.22 215.13	-2		8 +80.00 8 +90.00	215.70	- <u>2</u>	215.22 215.13	215.18 215.09	215.78 215.69	216.14 216.05	880 890	
215.96	215.60	215.00	215.04	-2		$\alpha \perp m m$	215 52	-2 -2	215.04	215.00	215.60	215.96	900 910	
215.88 215.79	215.52 215.43	214.83	214.96 214.87	-2		9 +1000 9 +2000 9 +2465 9 +3000 9 +4000 9 +5000 9 +7000	215.44	-2 -2	214.96 214.87	214.83	215.52 215.43	215.88 215.79	920	
215 <b>.</b> 75 215 <b>.</b> 70	215 <i>3</i> 9 215 <i>3</i> 4	214.74	214.78	-2		9 +24.65 9 +30.00	215.26	-2 -1.8331	214.83 214.82	214 <b>.</b> 79 214 <b>.</b> 78	215.39 215.38	215.75 215.74	924.65 930	
215.62 215.53	215.26 215.17	214.66	214.70 214.61	-2 -2		9 +40.00 9 +50.00	215.18 215.09	-1.5211 -1.2091	214.81 214.80	214 <b>.</b> 77 214 <b>.</b> 76	215.37 215.36	215.73 215.72	940 950	
215.44 215.35	215.08	214.48	214.52	- <u>2</u> -2		9 +60.00 9 +70.00	215.00	-0.8971 -0.5851	214.78 214.77	214.74 214.73	215.34 215.33	215.70 215.69	960 970	
215.27	214,91	214.31	214 <b>.3</b> 5	-2		コ エロいれい	1 / 14.001	-021311	214.76 214.75	214.72 214.71	215.32	215.68 215.67	980 988.75	
215.19 215.18	214.82	214,22	214.27 214.26	- <u>- 2</u> - 2	H/L	9 +88.75 9 +90.00	214.74	0.0000 0.0390	214.75	214.71	215.31 215.31	215.67	990	
215.09 215.02	214.66	214.06	214 <b>.</b> 17 214 <b>.</b> 10	-2 -2	RT/CR	9 +90.00 10 +00.00 10 +07.90	214.65 214.58	03510 05975	214.73 214.72	214.69 214.68	215.29 215.28	215.65 215.64	1000 1007.9	
215.01 214.92	214 <b>.</b> 65	214.05	214.09	-2	1	10 +10.00 10 +20.00	12145/1	0,6630 0,9750	214 <b>.</b> 73 214 <b>.</b> 71	214.69 214.67			1010 1020	
214.83 214.74	214.47	213.87	213 <b>.</b> 91	-2		10 +30 00 10 +40 00	214.39	1.2870 1.5990	214.70 214.68	214.66 214.64			1030 1040	
214,66	21430	213.70	213.74	-2	R/C	10 +50.00	214,22	1.9110	214,68	214,64			1050	
214.63 214.51	214.15	213.55	213.71 213.60	-2 -2 <i>2</i> 231		10 +52.85 10 +60.00	l 214 <b>.</b> 131	2,000 2,2231	214,67 214,66	214.63 214.62			1052.85 1060	
214 <i>3</i> 5 214 <i>3</i> 1	213.99 213.95	21339 21335	213.43 213.40	-2.6000	PC	10 +70.00 10 +72.08	214.04 214.02	2,5351 2,6000	214,65 214,64	214,60			1070 1072.08	
214.20	213.84	213,24	213,28	-2.8471		10 +80.00	213.96	2.8471	214.64	214.60			1080	

POINT	LT. TOP OF CURB ELEV.	LT. GUTTER ELEVATION	LT. EDGE OF PAV'T	LT. PAY'T SLOPE IN %		CENTER STA.	ELEV.	RT. PAV'T SLOPE IN %	RT. EDGE OF PAV'T	RT. GUTTER ELEVATION	RT. TOP OF CURB ELEV.	RT. HINGE POINT	CENTERLINE STATION	LT. EDGE GUTTER	RT. EDG GUTTER
214.03 214.00	213 <b>.</b> 641	213.07 213.04	213.11 213.08	-3.1591 -3.1903 F	RT/CR 1	10 +90.00 10 +91.00	213.85	3.1591 3.1903	214.63 214.62	214.59 214.57	215.17	215.53	1090 1091	24 24	
213.87 213.71	213.51 213.35	212.91 212.75	212.95 212.79	-3.4711 -3.7831	PVC 1	11 +00.00 11 +10.00	213.78 213.70	3.4711 3.7831	214.61 214.61	21457 21457	215.17 215.17	215. <b>5</b> 3 215. <b>5</b> 3	1100 1110	24 24	
213.62	213 <b>.2</b> 6	212,66	212.70	-3.9000	<b>F/S</b> 1	11 +13.75	213.64	3.9000 3.9	214.58	214.53	215 <b>.</b> 13	215.49	1113.75 1120	24	
213.59 213.49	213.23 213.13	212.63 212.53	212.67 212.57	- 3.9 - 3.9		11 +30.00	213.51	3.9	214.55 214.45	214.50 214.40	215.10 215.00	215 <b>.3</b> 6	1130	24 24	
213.39 213.28	213.03 212.92	212.43 212.32	212.47 212.36	- 3.9 - 3.9	1	11 +40.00 11 +50.00	213.41 213.30	3.9 3.9	214.35 214.24	214.30 214.19	214 <b>.9</b> 0 214 <b>.</b> 79	215.26 215.15	1140 1150	24 24	
213.17	212.81	212.21	212,25	- 3.9	PVI 1	11 +60.00	213.19	3.9	214.13	214.08	214,68	215.04	1160	24	
213.05 212.93	212.69 212.57	212.09 211.97	212.13 212.01	- 3.9 - 3.9		11 +70.00 11 +80.00	213.07 212.95	3.9 3.9	214.01 213.89	213.96 213.84	214.56 214.44	214.92 214.80	1170 1180	24 24	
212.80	212.44	211.84	211.88	- 3.9		11 +90.00	212.82	3.9	213.76	213.71	214.31	214.67	1190	24	
212.67 212.53	212.31 212.17	211.71 211.57	211.75 211.61	- 3.9 - 3.9	PVT 1	12 +00.00 12 +10.00	212.69 212.55	3.9 3.9	213.63 213.49	213.58 213.44	214 <b>.</b> 18 214 <b>.</b> 04	214.40	1200 1210	24 24	
212.39 212.24	212.03	211.43 211.28	211.47 211.32	- 3.9 - 3.9	1	12 +20.00 12 +30.00	212.41	3.9 3.9	213 <i>3</i> 5 213 <i>2</i> 0	213.30 213.15	213 <b>.9</b> 0 213 <b>.</b> 75	214.26 214.11	1220 1230	24 24	
212.10	211.74	211.14 211.00	211.18 211.04	- 3.9	1	12 +40.00	212.12	3.9	213.06	213.01	213.61	213.97	1240	24	
211.96 211.82	211.60 211.46	211.00 210.86	211.04 210.90	- 3.9 - 3.9	1	12 +50.00 12 +60.00	211.98 211.84	3.9 3.9	212.92 212.78	212.87 212.73	213.47 213.33	213.83 213.69	1250 1260	24 24	
211.67	211.31	210.71	210.75	- 3.9	1	12 +70.00	211,69	3.9	212.63	212.58	213 <b>.</b> 18	213.54	1270	24	
211.53 211.39	211 <b>.</b> 17 211 <b>.</b> 03	210.57 210.43	210.61 210.47	- 3.9 - 3.9	1	12 +90.00	211.41	3.9 3.9	212.49 212.35	212.44 212.30	213.04 212.90	213.40 213.26	1280 1290	24 24	
211.25 211.11	210.89 210.75	210.29 210.15	210.33 210.19	- 3.9 - 3.9	1	13 +00.00 13 +10.00	211.27	3.9 3.9	212.21 212.07	212 <b>.</b> 16 212 <b>.</b> 02	212.76 212.62	213.12	1300 1310	24 24	
210.96	210.60	210,00	210.041	- 3.9	1	13 +20.00	210.98	3.9	211.921	211.87	212 <b>.4</b> 7	212,83	1320	24	
210.82 210.68	210.46 210.32	209.86 209.72	209.90 209.76	- 3.9 - 3.9		13 +30.00 13 +40.00	210,84	3.9 3.9	211.78 211.64	211.73 211.59	212.33 212.19	212. <u>69</u> 212. <u>5</u> 5	1330 1340	24 24	
210.54	210 <b>.</b> 181	209.58	209.62	- 3.9	1	13 +50.00	210.56	3.9	211.50	211.45	212.05	212.41	1350	24	
210.44 210.39	210.03	209.48 209.43	209.52 209.47	- 3.9 R - 3.9	1	13 +57.00 13 +60.00	210.41	3.9 3.9	211.40 211.35	211.35 211.30	211.95	212.31	1357 1360	24 24	
210.25 210.19	209.89 209.83	209.29 209.23	209.33 209.27	- 3.9	1	13 +70.00 13 +74.30	210.27	3.9 3.9	211.21 211.15	211.16 211.10			1370 1374 <i>3</i>	24 24	
210.11	209.75	209.15	209.19	- 3.9	1	13 +80.00	210.13	3.7222	211.02	210.98			1380	24	
209.97 209.83	209.61 209.47	209.01 208.87	209.05 208.91	- 3.9 - 3.9		13 +90.00 14 +00.00	209.99	3.4102 3.0982	210.81 210.59	210 <b>.</b> 77 210 <b>.</b> 55			1390 1400	24 24	### THE PARTY OF T
209.68	209.32	208.72	208.76	- 3.9	1	14 +10,00	209.70	2.7862	210.37	210.55 210.33 210.15			1410	24	
209.56 209.56	209,20	208.60 208.60	208.64 208.64	-3.8335	1	14 +17.87 14 +20.00	209.561	2.5407 2.4742	210.19 210.15	210 <b>.</b> 111			1417.87 1420	24 24	
209.49 209.43	209 <b>.</b> 13 209 <b>.</b> 07	208.53 208.47	208.57 208.51	-3.5215 -3.2095	1	14 +30.00 14 +40.00	209.42	2.1622 1.8502	209.94 209.72	209.90 209.68			1430 1440	24 24 24 24 24 24 24 24 24 24 24	***************************************
209.35	208.99	208.391	208.431	-2.8975	- 11	14 +50.00	209.13	1.5383	209.50	209,46 209,25			1450	24	
209.28 209.29	208.92 208.93	208.32 208.33	208.37 208.37	-2.5999 -2.5855	PT 1	14 +59.54 14 +60.00	208.99	1,2406 1,2263	209.29 209.28	209.25 209.24			1459.54 1460	<u>24</u> 24	
209.26	208.90	208.30	208.341	-2.4295	PVC 1	14 65.00	208.92	1.0703	209.18	209.14			1465	24	
209,22 209,26	208.86 208.90	208.26 208.30	208.30 208.34	-2 <b>2</b> 735 -2 -2	1	14 +70.00 14 +72.36	208.82	0.9143 0.8406	209.07 209.02	209.03 208.98			1470 1472 <i>3</i> 6	<u>24</u> 24	
209.16 209.53	208.80	208.20 208.57	208.24 208.61	-2	1	14 +80.00 14 +90.00	208.72	0.6023 0.2903	208.86 208.68	208.82 208.64	Market Control of the		1480 1490	24	
209,44	209.08	208.48	208.52		H/L 1	14 +99,30	208.52	0.0000	208.52	208.48			1499.3	24	
209.43 209.35	209.07 208.99	208.47 208.39	208.51 208.43			15 +00.00 15 +10.00	208.51	- 0.0218 - 0.3338	208.50 208.35	208.46 208.31			1500 1510	24 24 24	
209.28	208.92	208.321	208.361		′	15 +20.00	208.36	- 0.6458	208,21	208.16	200 C7	200.07	1520	24	***************************************
209.24 209.22	208.88 208.86	208.28 208.26	208.32 208.30		′	15 +26,60 15 +30,00	208.30	- 0.8517 - 0.9578	208.12 208.07	208.07 208.03	208.67 208.63	209.03 208.99	1526.6 1530	24 24	
209.18 209.16	208.82 208.80	208,22 208,20	208.26 208.24			15 +40.00 15 +50.00	208.26	1.2698 1.5818	207.96 207.86	207.91 207.82	208.51 208.42	208.87 208.78	1540 1550	24 24	
209.14	208.78	208,181	208,22			15 +50.00 15 +60.00	208,22	- 1,8938	207.77	207.721	208.32	208.68	1560	24	
208.66 208.67	208. <b>3</b> 0 208. <b>3</b> 1	207.70 207.71	207.75	-1.9867	LP /	15 +62.96 15 +63.41	208.22 208.23	-1.9861 -2.0000	207.74 207.75	207.70 207.71	208 <i>3</i> 0 208 <i>3</i> 1	208.66 208.67	1562.96 1563.41	24 24	
208.72	208.36	207.761	207.80	-1.7916	′	15 +70,00	208.23	- 2 - 2	207.75	207.71	208.31	208.67	1570	24	
208.80 208.91	208.55	207.84 207.95	208-22 207.74 207.75 207.80 207.88 207.99 208.10	- 1.4956 - 1.1996		15 +80.00 15 +90.00	208.28	- 2	207.76 207.80	207.72 207.76	208.32 208.36	208.72	1580 1590	<u>24</u> 24	***************************************
209.02 209.15	208.66 208.79	208.06 208.19	208.10 208.23	0.9036 0.6076	PVI	16 +00.00 16 +10.00	208.32	- 2 - 2	207.84 207.90	207.80 207.86	208.40 208.46	208.76	1600 1610	24 24 24 24 24 24 24 24 24 24 24 24 24 2	23
20930	208,94	208.34	208.391	-03116		16 +20,00	208.46	- 2	207.98	207.94	208.54	208.90	1620	24	
209.46 209.64	209.28	208.50 208.68	208.55 208.72	-0.0156 0.2804		16 +30,00 16 +40,00	208.65	<u> </u>	208.07 208.17	208.03 208.13	208.63 208.73	209.09	1630 1640	24	
209.83 210.04	209.47 209.68	208.87 209.08	208.91 209.12	05764 0.8724		16 +50.00 16 +60.00	208.77	- 2 - 2	208.29 208.43	208.25 208.39	208.85 208.99	209,21	1650 1660	24 24 24	
210,18	209,82	209.22	209,26	1.0876	PC '	16 +67 <i>-</i> 27	209,00	- 2	208.52	208.48	209,08	209,44	1667.27	24 24	
210 <i>2</i> 6 210 <i>4</i> 9	209.90 210.13	209.30 209.53	209.34 209.57	1.1684 1.4644		16 +70 00 16 +80 00 16 +90 00	209.22	- 2 - 2	208.58 208.74	208.54 208.70	209.14 209.30	209.50 209.66	1670 1680	24 24	
210,74	210 <b>.3</b> 81	209.781	209,821	1.7604		16 +90.00	209.40	- 2 - 2	208,92	208.88	209 <i>.</i> 48	209.84	16901	24	
211.00 211.25	210 <b>.8</b> 91	210.04 210.29 210.31	210.08 210.33	2,0564 2,3210 2,3524	1 '	17 +00.00 17 +08.94	209.77	- 2	209.11 209.29	209.07 209.25	209.67 209.85	210,21	1700 1708.94	24 24	
211.27 211.56	210.91	210.31 210.60	210.35 210.65	2,3524 2,6484		17 +10.00 17 +20.00 17 +30.00	209.79	- 2 - 2	209.31 209.53	209.27 209.49	209.87 210.09	210,23	1710	24 24 24 24 24 24 24	
211.87	211.51	210,911	210,961	2,94441		17 +3000	21025	- 2	209.77	209.73	210.33	210.69	1730	24	
212.03 212.20	211.84	211.07 211.24	211 <b>.</b> 11 211 <b>.</b> 28	3,2404	PVI (	17 +35 <b>,0</b> 0 17 +40 <b>,0</b> 0	210.50	- 2 - 2	209.89 210.02	209.85 209.98	210.45 210.58	210.94	1735 1740	24 24	
212.52 212.70	212.16	211.56 211.74	211.60 211.78	3.5364 3.7000	E/C	17 +5000 17 +55.52	210.75	- 2 - 2	210.27 210.41	210.23 210.37	210.83 210.97	211.19	17501	24	
212.81	212 <b>.4</b> 5	211.85	211.78 211.89 212.14	3.7	′	17 +60,00	211,00	- 2	210.52	210 <i>4</i> 81	211.08	211.44	1760	24 24	
213.06 213.08	212 <b>.</b> 70 212 <b>.</b> 72	212 <b>.</b> 10 212 <b>.</b> 12	212 <b>.1</b> 4 212 <b>.1</b> 6	3.7 3.7 R	T/CR	17 +70,00 17 +70,97	211.25 211.27	- 2 - 2	210 <b>.</b> 77 210 <b>.</b> 79	210 <b>.</b> 73 210 <b>.</b> 75	211.33 211.35	211.69 211.71	1770 1770.97	24 24	***************************************
213.31	212.95	212.35	212,391	3 <b>.</b> 71	T./05	17 +8000	21150	- 2	211,02	210,98	<u> </u>	<u> </u>	1780	24 24 24 24 24 24 24	23
213.40	213.04	212,44	212.48 212.63	3.7  3.7	.T/CR	17 +80 00 17 +83 51 17 +90 00 18 +00 00	211.75	- 2 - 2	211.11 211.28 211.53	211.07 211.24			1783.51 1790	24 23.85	23 23
			212.63 212.87 213.12	3.7 3.7 3.7		18 +00.00 18 +10.00	212.00	- <u>2</u> - 2	211.53 211.78	211.24 211.49 211.74			1800 1810	23.85 23.63 23.40	23
			213.36	3.7		18 +10.00 18 +20.00 18 +30.00	21250	- 2	212,04	212,001			1820	23.40 23.18	23 23 23 23 23 23
			213.60 213.84	3.7 3.7		18 +30,00 18 +40,00	212.75 213 M	- 2 - 2	212.29 212.55	212.25 212.50			1830 1840	22.95 22.73	22 22
			214.08 214.32	3.7	1	18 +50,00	213,25	- 2	212,80	212.76			1850	22.50	22
			214.57	3.7 3.7		18 +60,00 18 +70,00	213 <b>.</b> 75	- 2 - 2	213.05 213.31	213.01 213.27			1860 1870	22.27 22.05	22 22
			214.81 215.05	3.7 3.7		18 +70 00 18 +80 00 18 +90 00	214.00	- 2 - 2	213.56 213.82	213.52 213.77	THE THE PARTY OF T		1880	21.82	21
			215.29	3.7	1	9 +00.00	21450	- <u>2</u> - 2	214.07	214.03			1890 1900	21.60 21.37	21 21

T. HINGE POINT	LT. TOP OF CURB ELEV.	LT. GUTTER ELEVATION	LT. EDGE OF PAV'T 215.53	LT. PAV'T SLOPE IN %		CENTERL INE  STA. ELEV. 9 +10.00 214.75	RT. PAY'T SLOPE IN %	RT. EDGE OF PAV'T	RT. GUTTER ELEVATION 21/1/28	RT. TOP OF CURB ELEV.	RT. HINGE POINT	centerline station 1910	LT. EDGE GUTTER 21.15	RT. EDG GUTTER
216.38	216.25	215.65	215.69	3.1 3.7	LT/CR /	9 +16.43   214.91		214.49	214.28 214.44			1916.43	21.00	21. 21.
16.47 16.69	216.34 216.56	215 <b>.</b> 74 215 <b>.9</b> 6	215.78 216.00	<u>3.1</u> 3.7	RT/CR/	9 +20.00   <u>215.00</u>   9 +28.80   <u>215.22</u>	- 2	214 <b>.58</b> 214. <b>80</b>	214.53 214.76	215. <b>3</b> 6	215.49	1920 1928.8	21 21	21.
16.72	216.59	215 <b>.</b> 99 216.17	216.03 216.21	3.7 3.7	′	9 +30.00 215.25 9 +37.50 215.43	-2	214.83 215.01	214.79	215.39 215.57	215.52	1930	21 21	
216.90 216.96	216.77 216.83	216.23	216.27	3.7		9 +40.00 215.49	1 2	215.07	214.97 215.03	215.63	215.70 215.76	1937. <u>5</u> 1940	21	
217.21 217.44	217.08 217.31	216,48 216,71	216.52 216.75	3.7 3.7	,	9 +50.00 215.74 9 +60.00 215.97	2	215. <b>32</b> 215. <b>5</b> 5	215.28 215.51	215.88 216.11	216.01 216.24	1950 1960	21 21	
217.67	217.54	216.94	216.98	3.7		9 +70.00 216.20	1 2	215.78	215.74	216.34	216.47	1970	21	
217.89 217.92	217.76 217.79	217.16 217.19	217.20 217.23	3.7 3.7	F/S	9 +80.00 <u>216.42</u> 9 +81.65 <u>216.45</u>	- <u>2</u>	216.00 216.03	215.96 215.99	216.56 216.59	216.69 216.72	1980 1981 <b>.</b> 65	21 21	
218.03	217.90	217.30	217.35	3.4528	1	9 +90.00   216.62	$-\frac{2}{2}$	216.20	216.16	216.76	216.89	1990	21	
218.17 218.30	218.04 218.17	217.44 217.57	217.48 217.61	3.1568 2.8608		20 +00.00 <u>216.82</u> 20 +10.00 <u>217.01</u>	- <u>2</u>	216.40 216.59	216.36 216.55	216.96 217.15	217.09 217.28	2000 2010	21 21	<del></del>
218.43	218.30	217.70	217.74	2,5648		20 +20 00   217 20	- 2	216.78	216.74	217.34	217.47	2020	21	
218.46 218.53	218.33 218.40	217.73 217.80	217.77 217.85	2.4666 2.2688	PT 2	20 +23 32   217 25 20 +30 00   217 37	- 2 - 2	216.83 216.95	216.79 216.91	217.39 217.51	217.52 217.64	2023.32 2030	21 21	
218.63	218.50	217.90	217.94	2.0001	2	20 +39,08   217,52	- 2 - 2	217.10	217.06	217.66	217.79	2039.08	21	
218.63 218.73	218.50 218.60	217.90 218.00	217.94 218.04	1,9728 1,6768		20 +40.00 <u>217.53</u> 20 +50.00 <u>217.69</u>	1 - 2	217.11 217.27	217.07 217.23	217.67 217.83	217.80 217.96	2040 2050	21 21	
218.82 218.90	218.69 218.77	218.09 218.17	218.13 218.21	1 3808 1 0848	2	20 +60.00 <u>217.84</u> 20 +70.00 <u>217.98</u>	- 2	217.42 217.56	217.38 217.52	217.98 218.12	218.11 218.25	2060 2070	21 21	
218.96	218.83	218,23	218.28	0.7888		20 +80,001 218,11	-2	217,69	21.7.65	218.25	218 <i>3</i> 8	2080	21	
219.02 219.06	218.89 218.93	218.29 218.33	218.33 218.37	0.4928 0.2386		20 +90.00 218.23 20 +98.59 218.32	- 2 - 2	217.81 217.90	217.77 217.86	218.37 218.46	218 <i>5</i> 0 218 <i>5</i> 9	2090 2098.59	21 21	
219.07	218.94	218.341	218.38	0.1968	2	$\frac{21}{1000} + \frac{21834}{21834}$	- 1.9560	217.93	217.89	218 <b>.</b> 49 I	218.62	2100	21	
219.10 219.11	218.97 218.98	218 <i>3</i> 7 218 <i>3</i> 8	218.41 218.42	0 <b>.0000</b> - 0 <b>.0</b> 992	H/L	21 +00.00   <u>218.34</u> 21 +06.65   <u>218.41</u> 21 +10.00   <u>218.44</u>	- 1.7485 - 1.6440	218.04 218.09	218.00 218.05	218.60 218.65	218.73 218.78	2106.65 2110	21 21	
219.15	219.02	218 <b>.4</b> 21	218.46	- 0.3952		21 +20.00 218.54	- 1.3320	218.26	218,22	218.82	218.95	2120	21	
219.16 219.18	219.03 219.05	218.43 218.45	218.47 218.49	- 0.6912 - 0.9132	PVI	21 +30.00 <u>218.62</u> 21 +37.50 <u>218.68</u>	- 1.0200 - 0.7861	218.41 218.51	218.36 218.47	218.96 219.07	219.09 219.20	2130 2137 <b>.</b> 5	21 21	
219.18	219.05	218.45	218.49	- 0,9872	2	21 +40.00 218.70	- 0.7081	218.55	218.51	219.11	219 <b>.</b> 24	2140	21	
219 <b>.</b> 19 219 <b>.</b> 19	219.06 219.06	218.46 218.46	218.50 218.50	- 1,2832 - 1,5792		21 +50.00 <u>218.77</u> 21 +60.00 <u>218.83</u>	- 0.3961 - 0.0841	218.69 218.81	218.65 218.77	219 <i>2</i> 5 219 <i>3</i> 7	219 <i>3</i> 8 219 <i>5</i> 0	2150 2160	21 21	
219.18	219,05	218. <b>4</b> 5	218.49 218.49	- 1,6591	H/L 2	21 +62.70   218.84	0.0000	218.84 218.93 218.98 219.03 219.13 219.22 219.30 219.38 219.40 219.42 219.44 219.50 219.53 219.54 219.54	218.80 218.89	219.49 219.49 219.53	219.53 219.62	2162.7	21 21	
219.17 219.17	219.04 219.04	218.44	218 <b>.4</b> 81	- 1.8752 - 2		21 +70.00 <u>218.88</u> 21 +74.22 <u>218.90</u>	0,2278 0,3594	218.98	218.93	219.49	219.66	2170 2174 <i>2</i> 2	21	
219.17 219.19 219.22 219.25 219.26 219.27 219.27 219.27 219.17 219.12 219.09 219.08	219.06 219.09	218 <b>.4</b> 6	218.50 218.53	<u> </u>	4	21 +70.00   218.88 21 +74.22   218.90 21 +80.00   218.95 22 +00.00   218.95 22 +10.00   218.99 22 +20.00   218.99 22 +23.13   219.00 22 +26.80   219.00 22 +40.00   218.99 22 +46.03   218.98 22 +50.00   218.97 22 +50.00   218.97 22 +60.00   218.97 22 +60.00   218.97 22 +60.00   218.97	0.5397 0.8517	219.03	218.99 219.09	219,59	219.72	2180 2190	21 21	
219.25	219.12	218.52	218.56	- 2		2 +00.00 218.98	1.1637	219.22	219.18	219.69 219.78	219.82 219.91 219.99	2200	21	
219.26	219.13 219.14	218.531	218.57 218.58	<u>- 2</u>		22 +10.00 <u>  218.99</u> 22 +20.00   219.00	1.4757 1.7877	219 <u>30</u>	219.26 219.33	219.86 219.93	219.99 220.06	2210 2220	21 21	
219.27	219.14	218.54	218.58	- 2	HP	2 +23.13 219.00	1.8853	219.40	219.35	219.95	220,08	2223.13	21	
219,27	219.14 219.12	218.54 218.52	218.58 218.56	<u> </u>		22 +26.80   <u>219.00</u> 22 +30.00   219.00	1.9998 2.0997	219.42 219.44	219.38 219.40	219.95 219.98 220.00	220 <b>.</b> 11 220 <b>.</b> 13	2226.8 2230	21 21	
219.17	219,04	218.441	218.48	- 2.4118		2 +40.00 218.99	2.4117	21950	219.45	220 <b>.</b> 0b l	220.18	2240	21	
219.12	218.99 218.96	218 <i>3</i> 9 218 <i>3</i> 6	218.43 218.40	2,6000 2,7238	PC 2	22 +46.03   <u>218.98</u> 22 +50.00   218.97	2.5998 2.7237	219.53 219.54	219.48 219.50	220.08 220.10	220.18 220.21 220.23	2246.03 2250	21 21	
219.08	218.95	218.35	218.39	- 2 <b>.7</b> 391	LT/CR 2	2 +50.49 218.97	2.7389	21954	219.50	220,10	220,23	2250,49	21	
			218 <i>3</i> 0 218 <i>2</i> 1	- <u>3.0358</u> - 3.3478		22 +60.00 <u>218.94</u> 22 +70.00 <u>218.91</u>	3.0356 3.3476	219.58 219.61	219.54 219.57	220 <b>.</b> 14 220 <b>.</b> 17	220,27 220,30	2260 2270	21 21	
			218.09	- 3 <b>.</b> 6598	F /6	22 +80 001 218 86	3,6596	219.63	219.57 219.59	220.19	22030 22032	2280	21 21	
			218.00 217.99	- 3.9000 - 3.9	F/S	22 +87.70 <u>218.82</u> 22 +90.00 <u>218.81</u>	3.9	219.63	219,50 219,59	220.20 220.19	22033 22032	2287.7 2290	21	
			217.92 217.85	- <u>3</u> .9		23 +00.00 <u>218.74</u> 23 +10.00 <u>218.67</u>	3.9	219.56	219.59 219.52 219.45	220 <b>.</b> 12	220,25	2300 2310 2320 2330	21	
	one of the second secon		217,771	- 3.9 - 3.9		23 +10.00 218.59 23 +20.00 218.59	3.9	219.49	219.37	220.05 219.97	220 <b>.</b> 18 220 <b>.</b> 10	2320	21 21	
			217.68 217.61	- 3.9 - 3.9	DVT	23 +2000 21859 23 +3000 21850 23 +3750 21843	3.9	219.32	219,28 219,21	219.97 219.88 219.81 219.78 219.68 219.58 219.48 219.48 219.38	220,01	2330	21 21	***********
			217.58	- 3.9	· · · · · · · · · · · · · · · · · · ·	23 +40.00 218.40 23 +49.47 218.31	3.9	219.22	219,18	219.78	219.94 219.91	2337.5 2340	21	
218.17	218.04 218.04	217.44	217.58 217.49 217.48 217.38	- 3.9 - 3.9	LT/CR	23 +49.47   <u>218.31</u> 23 +50.00   218.30	3.9	219.12	219,08	219.68 219.68	219.81 219.81	2349.47	21	
218.07	217,941	21734	21738	- <u>3.</u> 9		23 +50,00 21830 23 +60,00 21820 23 +70,00 21810	3.9	219.02	219.08 218.98	219.58	219.71	2360	21	
217.97	217.84 217.74	217.44 217.44 217.34 217.24 217.14	217.18	- 3.9 - 3.9		23 +70,00   218,10 23 +80,00   218,00	3.9	218.92 218.82	218.38 218.78	219.48 219.38	219.61 219.51	2370	21 21	
217.77	217.64 217.54	217.04	217.08	- 3.9		23 +90.00 217.90	3.9 3.9 3.9 3.9 3.9 3.9 3.9 3.9	218.72	218,68 218,58	219.28 219.18	219.41	2350 2360 2370 2380 2390 2400	21	
218.17 218.17 218.07 217.97 217.87 217.67 217.67 217.57 217.47 217.37	21 (54) 217,44	217.04 216.94 216.84 216.74	217.08 216.98 216.88 216.78	<u> </u>		23 +90 00 217 90 24 +00 00 217 80 24 +10 00 217 70 24 +20 00 217 60	3.9	219.58 219.61 219.63 219.64 219.63 219.63 219.64 219.63 219.63 219.72 219.72 219.72 219.72 219.72 218.72 218.72 218.62 218.62 218.62 218.62 218.62 218.62 218.62 218.62	218.58 218.48	219.18 219.08	219 <i>3</i> 1 219 <i>2</i> 1	2400	21 21	***************************************
217.47	217.44 217.34	216.74	216.78	<u> </u>		24 +20.00 217.60	3.9 3.9	218.42	218.38	219.08 218.98	219.11	2420 2430	21	
217.27 217.18	217.24 217.14 217.05	216.64 216.54	216.68 216.58 216.49	- 3.9 - 3.9 - 3.9 - 3.9 - 3.9 - 3.9 - 3.9 - 3.9 - 3.9		22 +90.00   218.81 23 +00.00   218.74 23 +10.00   218.67 23 +20.00   218.59 23 +30.00   218.50 23 +37.50   218.40 23 +49.47   218.31 23 +50.00   218.30 23 +60.00   218.20 23 +70.00   218.10 23 +80.00   217.90 24 +00.00   217.70 24 +20.00   217.70 24 +20.00   217.70 24 +30.00   217.70 24 +40.00   217.70 24 +40.00   217.70 24 +40.00   217.70 24 +40.00   217.70 24 +40.00   217.70	3.9	218.22	218.28 218.18	218.88 218.78	219.01 218.91	2440	21	
217.18 217.17	217.05 217.04	216.45 216.44	216.49 216.48	- 3.9 - 3.9	PVC	24 +49.84   217.31 24 +50.00   217.30	3.9	218.22 218.13 218.12	218.18 218.09 218.08	218.69 218.68	218.82 218.81	2449,84	<u>21</u>	***
217.06	216.93 216.81	216.33	216.37	- 3.9		24 +60.001 217.19	3.9	218.01	217.97	218.57	218.70	2450 2460	21	
216.94 216.93 216.84	216.81 216.80	216,21 216,20	216.25 216.24	- 3.9 - 3.8903	F/S	24 +69.70 217.07 24 +70.00 217.06	3.9	217.89 217.88	217.85 217.84	218.45 218.44	218 <i>5</i> 8 218 <i>5</i> 7	2469 <u>.69</u> 2470	21 21	
216.84	216.71	216.11	216.15	- 3,5783	1	24 + 80 00   216 90	3 5723	217.65	217.61	218 <i>-</i> 21	218.34	2480	21	
216.73 216.60	216.60 216.47	216.00 215.87	216.04 215.91	- 3,2663 - 2,9543		24 +90.00 216.73 25 +00.00 216.53 25 +10.00 216.31 25 +11.36 216.21 25 +20.00 216.07 25 +24.84 215.94	3.2663 2.9543	217.42 217.15	217.37 217.11	217.97 217.71	218.10 217.84	2490 2500	21 21	
216,44	216.47 216.31	215.71	215.76	- 2,6423		25 +1000 21631	2,6423	216.86	216 <b>.</b> 32	217 <b>.4</b> 2	217.55	2510	21	
216.35 216.27	216,22 216,14	215.62 215.54	215.66 215.58	- 2,5999 - 2,3303	PT	25 +71 36  21621 25 +2000  21607	2.5999 2.3303	216.76 216.56	216.71 216.52	217.31 217.12	217.44 217.25	2511.36 2520	21 21	
216.17	216.041	215.44	215.48	- 2 <b>.</b> 1793	PVRC	25 +24.84 215.94 25 +30.00 215.81	2.1793	216.40	216.36	216.96	217.09	2524.84	21	
216.07 216.06	215.94 215.93	215.34 215.33	215 <i>3</i> 9 215 <i>3</i> 7	- 2,0183 - 2,0000	R/C	25 +30.00  215.81 25 +30.59  215.79	2,0183	216.23 216.21	216 <b>.</b> 19 216 <b>.</b> 17	216.79 216.77	216.92 216.90	2530 2530.59	21 21	
216.06 215.83	215.70	215.10	215.14	- 2		25 +40.00L 215.56	1.7064	215.92	215,38	216 <b>.4</b> 8	216.61	2540	21	
215.58 215.34 215.10 214.90	215.45 215.21	214.85 214.61	214.89 214.65	2 2		25 +50.00 <u>215.31</u> 25 +60.00 <u>215.07</u>	1.0824	215.60 215.30	215.56 215.26	216 <b>.</b> 16 215 <b>.8</b> 6	216.29 215.99	2550 2560	21 21	
215.10	214.971	214.37	214.41	- 2 - 2		25 +70.00 214.83	0.7704	214.99	214.95	215.55	215.68	2570	21	
214.69	214.77 214.56	214.17 213.96	214.21 214.00	<u>- 2</u>		25 +90.001 214.42	0.1464	214.73 214.45	214.68 214.41	215,28 215,01	215.41 215.14	2580 2590	21 21	
214.69 214.59 214.49	214.46 214.36	213.86 213.76	213.90	- 2 - 2	H/L	25 +94 <b>.</b> 70  214 <b>.3</b> 2	0.0000	214.32	214,28	214.88	215.01	2594,69	21	
21430	214.17	213.57	213.80 213.61	- 2		26 +00 00 <u>214 22</u> 26 +10 00 <u>214 03</u>	-0.4777	214 <b>.</b> 19 213 <b>.</b> 93	214.14 213.89	214.74 214.49	214.87 214.62	2600 2610	21 21	
214.12	213.99 213.81	213.39 213.21	213.43 213.25	- 2 - 2		26 +20.00  213.85	- 0.7897 - 1.1017	213.68	213.64	214.24	214.37	2620	21 21	
213.94 213.77	213,64	213.04	213.08	<u>- 2</u>		26 +30.00 <u>213.67</u> 26 +40.00 <u>213.50</u>	-1.4137	213.44 213.20	213.40 213.16	214.00 213.76	214.13 213.89	2630 2640	21	
213.62 213.47	213.49 213.34	212.89	212.93 212.78	- 2 - 2		26 +50.00 <u>213.35</u> 26 +60.00 <u>213.2</u> 0	-1.7257	212.99 212.77	212.95 212.73	213.55 213.33	213.68 213.46	2650 2660	21 21	
213.44	213.31	212.71	212.75	<u> </u>		26 +58 80 213 17	-2.000	212.75	212.71	213.31	213.46	2658.8	21	

#### LEGEND:

E/T- END TRANSITION PC- POINT OF CURVATURE H/L- RUNOFF HP- HIGH POINT LT/CR- LEFT CURB RADIUS

F/S- FULL SUPERELEVATION PVC- POINT OF VERTICAL CURVATURE PVI- POINT OF VERTICAL INTERSECTION PVRC- POINT OF VERTICAL REVERSE CURVATURE PVT- POINT OF VERTICAL TANGENCY RT/CR- RIGHT CURB RADIUS PT- POINT OF TANGENCY R/C- REVERSE CURVATURE

DEPARTMENT OF PUBLIC WORKS
HOWARD COUNTY, MARYLAND

N/C- NORMAL CROWN

LP- LOW POINT

Phoenix - Nolan Joint Venture

Fax: (410) 247-9397

	E OF MARY
X	

	DES: J.R.H.	S,E.W.	$\triangle$	ADD NEW SHEET	10.9.02	
	DRN: D.R.B.					DAVENAENT ELEVATIONE
						PAVEMENT ELEVATIONS
	CHK:					
	DATE:					
•	DATE	BY	NO.	REVISION	DATE	600' SCALE MAP NO. BLOCK N

DORSEY RUN ROAD SOUTH LINK PHASE 1

CAPITAL PROJECT NO. J-4110

BLOCK NO.

SCALE AS SHOWN

SHEET 30A0F<u>30</u>