	SHEET INDEX
SHEET NO.	DESCRIPTION
1	TITLE SHEET
2-4	PRELIMINARY EQUIVALENT SKETCH, REVISED PERCOLATION CERTIFICATION & LANDSCAPE PLAN
5-8	GRADING, SEDIMENT CONTROL & EROSION CONTROL PLAN
9-11	PRELIMINARY FOREST CONSERVATION PLAN
12-13	STORM DRAIN DRAINAGE AREA & SOILS MAP
14	STORMWATER MANAGEMENT NOTES & DETAILS

BUILDABLE PRESERVATION PARCEL 'A' & NON-BUILDABLE PRESERVATION PARCELS 'B' THRU 'D' **ZONED: RC-DEO** GENERAL NOTES:

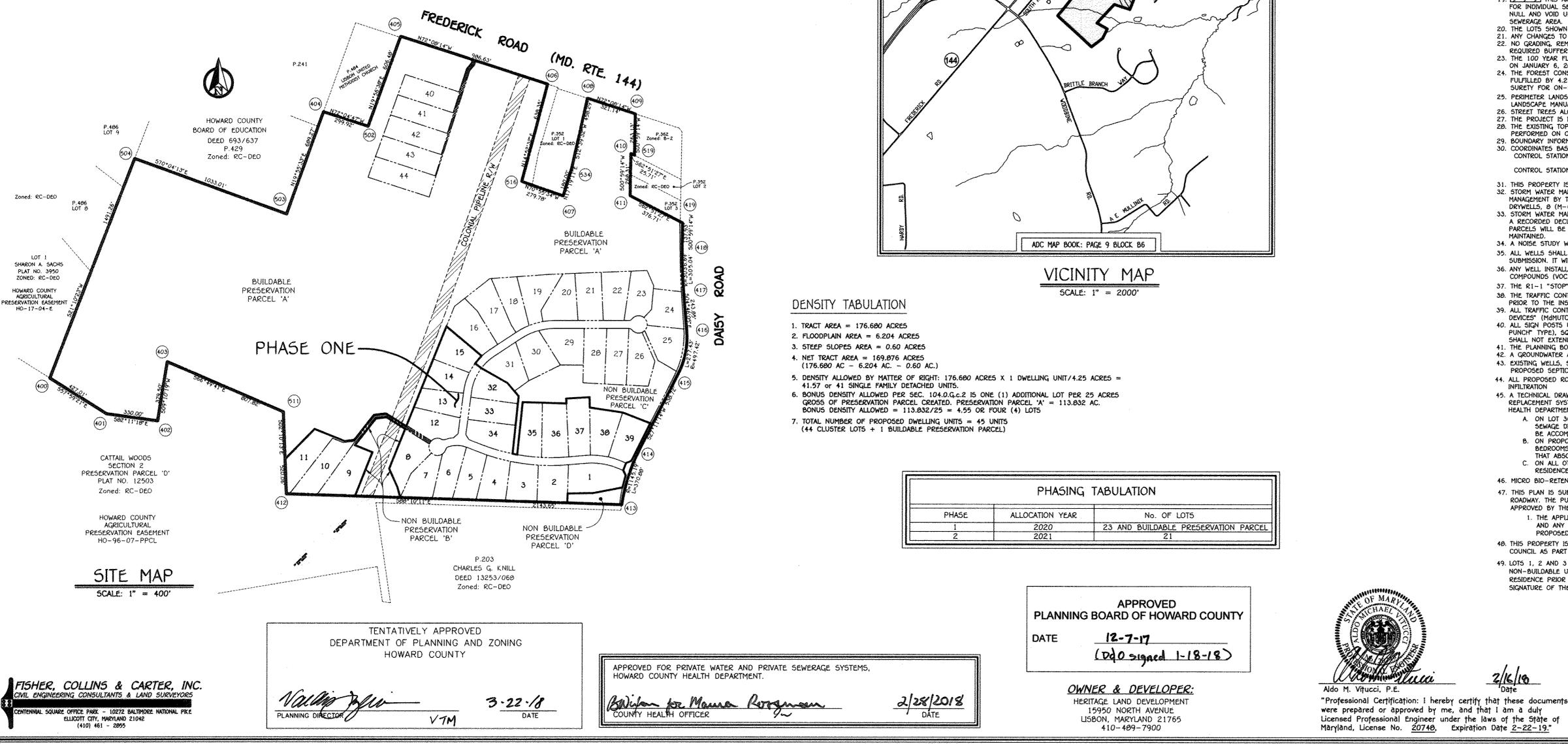
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		art
GROSS AREA	PIPESTEM AREA	MINIMUM LOT SIZE
63,809 Sq.Ft.	4,313 Sq.Ft.	59,496 5q.Ft.
61,671 5q.Ft.	5.761 Sq.Ft.	55.910 Sq.Ft.
60,715 Sq.Ft.	5,681 Sq.Ft.	55,034 5q.Ft.
51,551 Sq.Ft.	1,050 Sq.Ft.	50,501 Sq.Ft.
52,706 Sq.Ft.	1,707 Sq.Ft.	51,079 Sq.Ft.
56,698 Sq.Ft.	2,356 Sq.Ft.	54,342 5q.Ft.
58,754 Sq.Ft.	3,028 Sq.Ft.	55,726 Sq.Ft.
60,810 5q.Ft.	3,700 5q.Ft.	57,110 Sq.Ft.
	63,009 5q.Ft. 61,671 5q.Ft. 60,715 5q.Ft. 51,551 5q.Ft. 52,706 5q.Ft. 56,690 5q.Ft. 58,754 5q.Ft.	GROSS AREA AREA 63,009 Sq.Ft. 4,313 Sq.Ft. 61,671 Sq.Ft. 5,761 Sq.Ft. 60,715 Sq.Ft. 5,601 Sq.Ft. 51,551 Sq.Ft. 1,050 Sq.Ft. 52,706 Sq.Ft. 1,707 Sq.Ft. 56,690 Sq.Ft. 2,356 Sq.Ft. 50,754 Sq.Ft. 3,028 Sq.Ft.

POADWAY INFORMATION CHART

	KUAUWAT	INFORTATION CHAR		
ROAD NAME	CLASSIFICATION	DESIGN SPEED	POSTED SPEED LIMIT	R/W WIDTH
LINDEN GROVE	PUBLIC ACCESS STREET	30 M.P.H.	25 M.P.H.	50'
HERITAGE RIDGE	PUBLIC ACCESS STREET	30 M.P.H.	25 M.P.H.	50'
KIMBERLYS WAY	PRIVATE ORIVEWAY	15 M.P.H.		24' EASE.

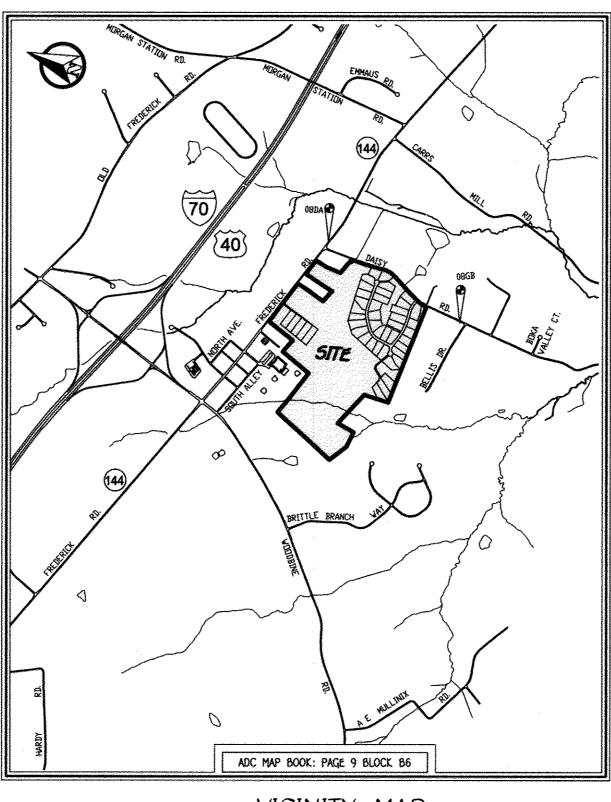
	TRAFFIC C	ONTROL	SIGNS	
ROAD NAME	CENTERLINE STA	OFFSET	POSTED SIGN	SIGN COD
LINDEN GROVE	0+43	21'L	STOP W/ROAD NAME SIGN	R1-1
LINDEN GROVE	2+00	14'R	SPEED LIMIT 25	R2-1
HERITAGE RIDGE	0+32	10'L	STOP	R1-1
HERITAGE RIDGE	1+52	14'R	SPEED LIMIT 25	R2-1
FREDERICK ROAD	14+02	20'L	STOP	R1-1



PRELIMINARY EQUIVALENT SKETCH & REVISED PERCOLATION CERTIFICATION PLAN

LINDEN GROVE LOTS 1 THRU 44,

TAX MAP No. 7 GRID No. 18 & AX MAP No. 8 GRID No. 13 PARCEL No. 5 4th ELECTION DISTRICT HOWARD COUNTY, MARYLAND



	PHASING	TABULATION
PHASE	ALLOCATION YEAR	No. OF LOTS
1	2020	23 AND BUILDABLE PRESERVATION PAR
2	2021	21

2/16/18

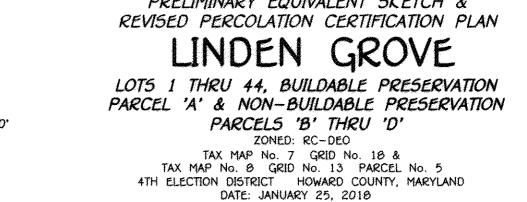
	U.5. [Equivalent	C	coordina:	ite Table	
Point #	Northing	Easting		Point #	Northing	Easting
413	604616.22	1294962.11		516	606663.51	1294319.80
414	604967.59	1295075.66		406	607200.46	1294403.60
415	605446.79	1295321.81		405	607583.10	1293544.61
416	605715.41	1295375.04		502	607012.99	1293337.74
417	605958.42	1295354.77		404	607105.27	1293052.37
419	606401.07	1295347.09		503	606457.27	1292817.47
411	606572.93	1295011.87		504	606809.39	1291846.32
410	606841.20	1295016.49		400	605410.79	1291307.70
519	606829.47	1295039.37		401	605192.44	1291669.78
409	607092.56	1295043.90		402	605147.59	1291996.72
408	607191.07	1294738.24		403	605522.24	1292057.21
534	606743.92	1294637.81		511	605204.37	1292799.86
407	606572.08	1294584.22		412	604684.68	1292019.55

PROPERTY ZONED RC-DEO WITH A TIER III DESIGNATION PER 10/6/13 COMPREHENSIVE ZONING PLAN. 2. AREA TABULATION:

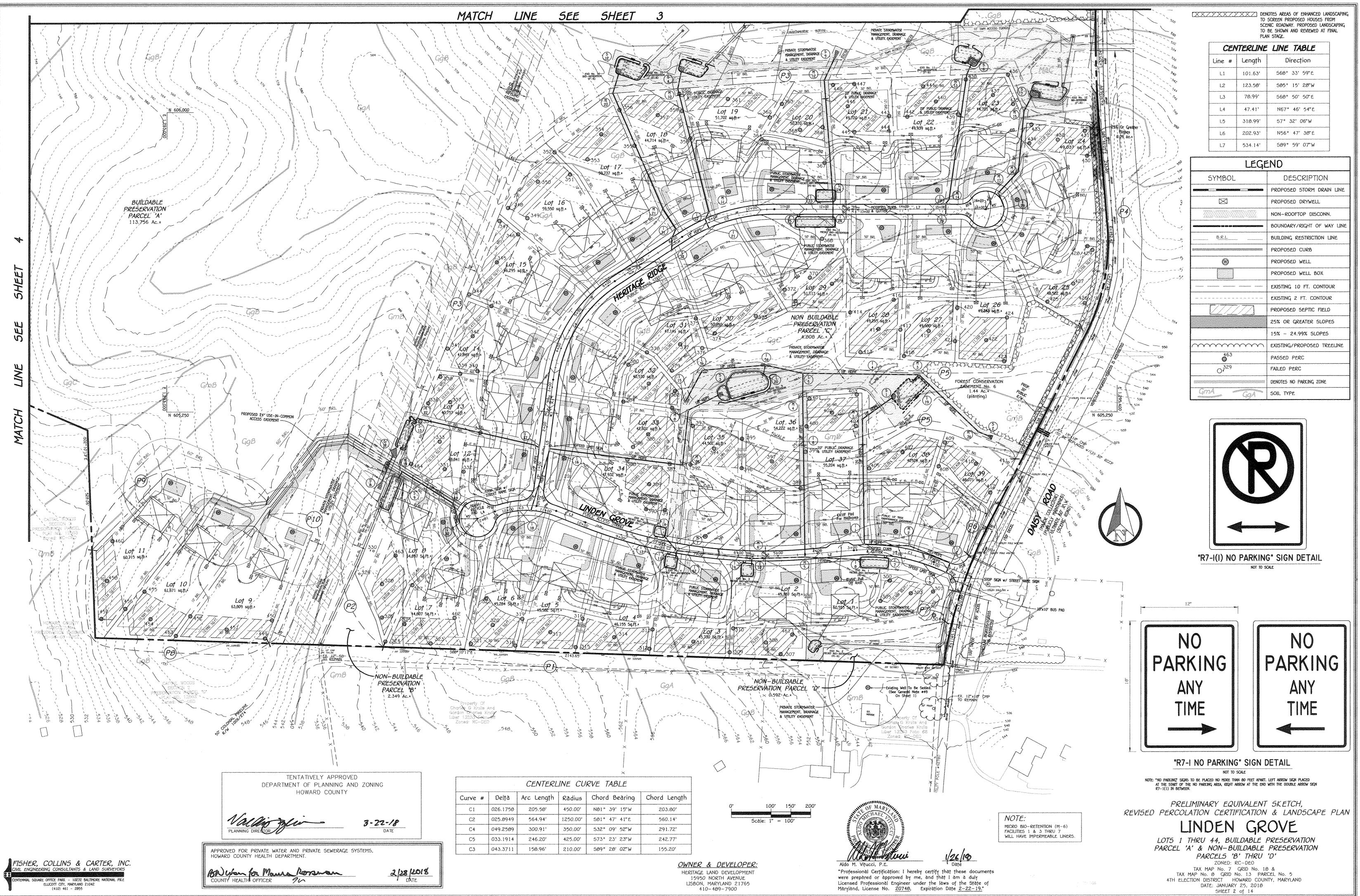
- A. TOTAL TRACT AREA = 176.680 Ac* B. AREA OF PROPOSED ROAD R/W = 4.410 Ac* C. AREA OF PROPOSED BUILDABLE LOTS = 50.765 Ac* D. AREA OF PROPOSED BUILDABLE PRESERVATION PARCELS 'A' = 113.756 Ac*
- E. AREA OF PROPOSED NON-BUILDABLE PRESERVATION PARCELS = 7.749 Ac* FLOODPLAIN AREA = 6.204 AC.
- STEEP SLOPE AREA = 0.60 AC.+ . AREA OF STREAMS (INCLUDING BUFFERS) = 7.84 AC.*
- 1. NET TRACT AREA = 169.876 AC.+ PREVIOUS HOWARD COUNTY FILE NUMBERS: ECP-17-019, WP-18-001, PB-
- K. DEED REFENCES: L. 445/F. 767, L. 954/F. 441, L. 993/F. 380, L. 15899/F. 246 L. TOTAL AREA OF WETLANDS (INCLUDING BUFFERS) = 1.57 AC.+
- NUMBER OF LOTS/PARCELS: A. BUILDABLE LOTS = 44
- BUILDABLE PRESERVATION PARCELS = . NON-BUILDABLE PRESERVATION PARCELS = 3
- D. MODERATE INCOME HOUSING UNITS REQUIRED = 5 MIHU (45 UNITS \times 10% = 5 MIHU); THE REQUIREMENT WILL BE MET BY A FEE-IN-LIEU PAYMENT. SOILS INFORMATION TAKEN FROM NRCS WEB SOIL SURVEY.
- THE FOREST STAND & WETLANDS DELINEATION REPORT DATED DECEMBER, 2016 WAS PREPARED BY ECO-SCIENCE PROFESSIONAL, INC AND WAS UPDATED ON AUGUST 4, 2017. THERE ARE STEEP SLOPES OF 25% OR GREATER ON SITE OF 0.60 ACRES. NO CEMETERIES EXIST ON SITE BY VISUAL OBSERVATION OR LISTED IN AVAILABLE HOWARD COUNTY CEMETERY INVENTORY MAP
-). THERE ARE NO HISTORIC HOUSE STRUCTURES ON-SITE. 9. SITE IS ADJACENT TO TWO SCENIC ROADS (DAISY ROAD & FREDERICK ROAD, A SCENIC ROADS REPORT HAS BEEN PROVIDED BY FISHER, COLLINS & CARTER, INC. DATED 10/24/16.
- 10. THE TRAFFIC STUDY FOR THIS PROJECT WAS PREPARED BY MARS GROUP DATED APRIL 19, 2016. 11. THERE ARE EXISTING STRUCTURES LOCATED WITHIN BUILDABLE PRESERVATION PARCEL 'A' TO REMAIN. PER THE ZONING DIVISION, A BARN IS A PERMITTED ACCESSORY USE TO A PRINCIPAL FARM USE. A DWELLING IS NOT REQUIRED IN ORDER TO RETAIN THE BARN. 12. BUILDABLE PRESERVATION PARCEL 'A' TO BE PRIVATELY OWNED AND ENCUMBERED BY AN EASEMENT AGREEMENT WITH THE LISBON GROVE HOMEOWNERS ASSOCIATION,
- INC. AND HOWARD COUNTY, MARYLAND. THE USE OF PARCEL 'A' WOULD BE FOR AN AGRICULTURAL USE AND A PROPOSED BUILDING SITE. 13. NON-BUILDABLE PRESERVATION PARCELS 'B' THRU 'D' WILL BE OWNED BY THE LINDEN GROVE PROPERTY HOMEOWNERS ASSOCIATION, INC. AND THE PRESERVATION EASEMENT WILL BE HELD BY HOWARD COUNTY, MARYLAND. THE USE FOR PARCEL 'B' IS FOR STORM WATER MANAGEMENT. THE USE FOR PARCEL 'C' IS STORM WATER MANAGEMENT. THE USE FOR PARCEL 'D' IS FOR STORM WATER MANAGEMENT.
- 14. ALL LOTS AREAS ARE MORE OR LESS. 15. DRIVEWAYS SHALL BE PROVIDED PRIOR TO ISSUANCE OF A USE AND OCCUPANCY PERMIT FOR ANY NEW DWELLINGS TO ENSURE SAFE ACCESS FOR FIRE AND EMERGENCY
- VEHICLES PER THE FOLLOWING MINIMUM REQUIREMENTS: A) WIDTH - 12 FEET (16 FEET) SERVING MORE THAN ONE RESIDENCE);
- B) SURFACE SIX (6") INCHES OF COMPACTED CRUSHER RUN BASE WITH TAR AND CHIP COATING. $(1 - 1/2^{\circ} MINIMUM);$) GEOMETRY - MAXIMUM 15% GRADE, MAXIMUM 10% GRADE CHANGE AND 45-FOOT TURNING RADIUS;
-) STRUCTURES (CULVERTS/BRIDGES) CAPABLE OF SUPPORTING 25 GROSS TONS (H25-LOADING); E) DRAINAGE ELEMENTS - CAPABLE OF SAFELY PASSING 100 YEAR FLOOD WITH NO MORE THAN 1 FOOT DEPTH
- OVER SURFACE: F) STRUCTURE CLEARANCES - MINIMUM 12 FEET G) MAINTENANCE - SUFFICIENT TO ENSURE ALL WEATHER USE
- 16. FOR FLAG OR PIPESTEM LOTS, REFUSE COLLECTION, SNOW REMOVAL AND ROAD MAINTENANCE ARE PROVIDED TO THE JUNCTION OF THE FLAG OR PIPESTEM AND ROAD RIGHT-OF-WAY LINE AND NOT TO THE PIPESTEM LOT DRIVEWAY. 17. ARTICLES OF INCORPORATION FOR THE LINDEN GROVE PROPERTY HOMEOWNERS ASSOCIATION, INC. WILL BE FILED WITH THE STATE DEPARTMENT OF ASSESSMENTS AND TAXATION PRIOR TO RECORDATION OF THE FINAL PLAT. 18. A PRE-SUBMISSION COMMUNITY MEETING WAS HELD FOR THIS PROJECT ON 2/23/17 AT THE GLENWOOD LIBRARY AT 6:00 P.M
- 19. THIS AREA DESIGNATES A PRIVATE SEWERAGE AREA OF AT LEAST 10,000 SQUARE FEET AS REQUIRED BY THE MARYLAND STATE DEPARTMENT OF THE ENVIRONMENT FOR INDIVIDUAL SEWAGE DISPOSAL IMPROVEMENTS OF ANY NATURE IN THESE AREAS ARE RESTRICTED UNTIL PUBLIC SEWERAGE IS AVAILABLE. THESE AREAS SHALL BECOME NULL AND VOID UPON CONNECTION TO A PUBLIC SEWERAGE SYSTEM. THE COUNTY HEALTH OFFICER SHALL HAVE THE AUTHORITY TO GRANT ADJUSTMENTS TO THE PRIVATI SEWERAGE AREA. RECORDATION OF A MODIFIED AREA SHALL NOT BE NECESSARY. THE LOTS SHOWN HEREON COMPLY WITH THE MINIMUM OWNERSHIP WIDTH AND LOT AREA AS REQUIRED BY THE MARYLAND STATE DEPARTMENT OF THE ENVIRONME 21. ANY CHANGES TO THE PRIVATE SEWERAGE AREA SHALL REQUIRE A REVISED PERC CERTIFICATION PLAN. 22. NO GRADING, REMOVAL OF VEGETATIVE COVER OR TREES, PAVING AND NEW STRUCTURES SHALL BE PERMITTED WITHIN THE LIMITS OF WETLANDS, STREAM(S), OR THEIR REQUIRED BUFFERS, FLOODPLAIN AND FOREST CONSERVATION EASEMENT AREAS. 23. THE 100 YEAR FLOODPLAIN DELINEATED ON THIS PLAN HAS BEEN DETERMINED TO BE "NOT CRITICAL" BASED ON A REPORT PREPARED BY FISHER. ON JANUARY 6. 2017. 24. THE FOREST CONSERVATION REQUIREMENTS PER SECTION 16.1200 OF THE HOWARD COUNTY CODE AND FOREST CONSERVATION MANUAL FOR THIS SUBDIVISION WILL BE FULFILLED BY 4.24 AC.* OF ON-SITE CREDITED RETENTION AND 12.27 AC.* OF ON-SITE AFFORESTATION. THERE IS NO SURETY FOR FOREST RETENTION.
- SURETY FOR ON-SITE PLANTING IS \$267,241.00, (12.27 ac. x 43,560 sq.ft. x \$0.50). 25. PERIMETER LANDSCAPING FOR THIS DEVELOPMENT SHALL BE IN ACCORDANCE WITH SECTION 16.124 OF THE SUBDIVISION AND LAND DEVELOPMENT REGULATIONS AND LANDSCAPE MANUAL. FINAL LANDSCAPING REVIEW AND SURETY IS DEFERRED UNTIL THE FINAL SUBDIVISION PLAN STAGE. 26. STREET TREES ALONG PUBLIC ROADS WILL BE PROVIDED AT THE FINAL PLAN STAGE AND WILL BE INCLUDED IN DED'S COST ESTIMATE
- HE PROJECT IS IN CONFORMANCE WITH THE LATEST HOWARD COUNTY STANDARDS UNLESS ALTERNATIVE COMPLIANCES HAVE BEEN APPROVED. 28. THE EXISTING TOPOGRAPHY INFORMATION SHOWN IS BASED ON HOWARD COUNTY AERIAL CONTOURS (2' interval) AND SUPPLEMENTED WITH A FIELD RUN TOPOGRAPHIC SURVEY PERFORMED ON OR ABOUT 7/21/16 BY FISHER, COLLINS & CARTER, INC. 29. BOUNDARY INFORMATION IS BASED ON A SURVEY PERFORMED ON OR ABOUT 11/11/14 BY FISHER, COLLINS & CARTER, INC. 30. COORDINATES BASED ON NAD '83, MARYLAND COORDINATE SYSTEM AS PROJECTED BY HOWARD COUNTY GEODETIC CONTROL STATIONS NOS:
- CONTROL STATION NO. OB DA N 606,934.18 ELEV. 554.836

Scale: 1" = 2000'

- E 1,295,730.52 CONTROL STATION NO. 00 GB N 603,764.82 E 1,294,891.90 ELEV. 570,387
- 31. THIS PROPERTY IS NOT LOCATED WITHIN THE METROPOLITAN DISTRICT. PRIVATE WELL AND PRIVATE SEPTIC WILL BE UTILIZED FOR THIS PROJECT 32. STORM WATER MANAGEMENT IS IN ACCORDANCE WITH THE M.D.E. STORM WATER DESIGN MANUAL, VOLUMES 1 & 11, REVISED 2009. WE ARE PROVIDING STORM WATER MANAGEMENT BY THE USE OF 3 AREAS OF (N-1) ROOFTOP DISCONNECTION CREDIT, 3 AREAS OF (N-2) NON-ROOFTOP DISCONNECTION CREDIT, 83 AREAS OF (M-5) DRYWELLS, & (M-6) MICRO-BIORETENTION FACILITIES AND 6 (F-6) BIO-RETENTION FACILITIES TO MEET AND EXCEED THE REQUIRED ESD VOLUME. 33. STORM WATER MANAGEMENT DEVICES LOCATED ON INDIMIDUAL LOTS WILL BE OWNED AND MAINTAINED BY THAT PARTICULAR LOT OWNER AND SUBJECT TO THE REQUIREMENTS OF A RECORDED DECLARATION OF COVENANT, SWM DEVICES LOCATED WITHIN THE PUBLIC R/W WILL BE PRIVATELY OWNED AND JOINTLY MAINTAINED, AND SWM DEVICES LOCATED ON
- PARCELS WILL BE OWNED AND MAINTAINED BY THE H.O.A., SWM FACILITIES SERVING PUBLIC ROADS, BUT LOCATED ON PRIVATE LOTS WILL BE PRIVATELY OWNED AND JOINTLY 34. A NOISE STUDY WAS PREPARED BY MARS GROUP DATED MAY, 2017 AND APPROVED ON OCTOBER 24, 2017. 35. ALL WELLS SHALL BE DRILLED PRIOR TO FINAL PLAT RECORDATION. IT IS THE DEVELOPER'S RESPONSIBILITY TO SCHEDULE THE WELL DRILLING PRIOR TO FINAL PLAT SUBMISSION. IT WILL NOT BE CONSIDERED "GOVERNMENT DELAY" IF THE WELL DRILLING HOLDS UP HEALTH DEPARTMENT SIGNATURE OF THE RECORD PLAT.
- 36. ANY WELL INSTALLED FOR POTABLE WATER CONSUMPTION ON LOTS 40 THRU 44 IN THE LINDEN GROVE SUBDIVISION SHALL BE SAMPLED AND ANALYZED FOR VOLATILE ORGANIC COMPOUNDS (VOC). 37. THE R1-1 "STOP" SIGN AND THE STREET NAME SIGN (SNS) ASSEMBLY FOR THIS DEVELOPMENT MUST BE INSTALLED BEFORE THE BASE PAVING IS COMPLETED.
- 38. THE TRAFFIC CONTROL DEVICE LOCATIONS SHOWN ON THE PLANS ARE APPROXIMATE AND MUST BE FIELD APPROVED BY HOWARD COUNTY TRAFFIC DIVISION (410) 313-2430 PRIOR TO THE INSTALLATION OF ANT OF THE TRAFFIC CONTROL DEVICES. 39. ALL TRAFFIC CONTROL DEVICES AND THEIR LOCATIONS SHALL BE IN ACCORDANCE WITH THE LATEST EDITION OF THE "MARYLAND MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES" (MdMUTCD). 40. ALL SIGN POSTS USED FOR TRAFFIC CONTROL SIGNS INSTALLED IN THE COUNTY RIGHT-OF-WAY SHALL BE MOUNTED ON A 2" GALVANIZED STEEL, PERFORATED ("QUICK
- PUNCH" TYPE), SQUARE TUBE POST (14 GAUGE) INSERTED INTO A 2-1/2" GALVANIZED STEEL, PERFORATED, SQUARE TUBE SLEEVE (12 GAUGE) 3' LONG. THE ANCHOR SHALL NOT EXTEND MORE THAN TWO "QUICK PUNCH" HOLES ABOVE GROUND LEVEL A GALVANIZED STEEL POLE CAP SHALL BE MOUNTED ON TOP OF EACH POST. 41. THE PLANNING BOARD APPROVED PB CASE No. 432 ON JANUARY 24, 2018. 42. A GROUNDWATER APPROPRIATIONS PERMIT NUMBER FOR THIS PROPOSED SUBDIMISION IS HO2017G002/01. 43. EXISTING WELLS, SEPTIC SYSTEMS AND SEWAGE DISPOSAL AREAS WITHIN 100 FEET OF THE PROPERTY AND THOSE WELLS WITHIN 200 FEET DOWN GRADIENT OF EXISTING AND
- PROPOSED SEPTIC SYSTEMS OR SEWAGE DISPOSAL AREAS HAVE BEEN SHOWN. 44. ALL PROPOSED ROADSIDE SWALES FOR THE SUBDIVISION MUST BE AT LEAST 50 FEET FROM ALL WELL AREAS OR AT LEAST 100 FEET IF THE SWALE IS DESIGNED FOR INFILTRATION
- 45. A TECHNICAL DRAWING, E.G. THE PLAN VIEW ON A SEPTIC SYSTEM INSTALLATION PLAN, ILLUSTRATING THE DRAINFIELD TRENCH LAYOUT FOR AN INITIAL SYSTEM AND FOR TWO REPLACEMENT SYSTEMS MUST BE SUBMITTED FOR THE PROPOSED RESIDENCE ON EACH RESPECTIVE LOT OF THIS SUBDIVISION PRIOR TO BUILDING PERMIT APPROVAL BY THE HEALTH DEPARTMENT
 - A. ON LOT 36, THE LIMITATIONS OF SOIL PROPERTIES ARE SUCH THAT A HOUSE WITH NO MORE THAN 4 BEDROOMS CAN BE SUPPORTED WITHIN THE DESCRIBED SEWAGE DISPOSAL AREA UNLESS AN EXHIBIT PREPARED BY A CERTIFIED PROFESSIONAL ILLUSTRATES THAT ABSOPTION TRENCH AREA FOR MORE BEDROOMS CAN BE ACCOMODATED WITHIN THE SDA.
 - B. ON PROPOSED LOTS 2, 3, 29, 32, 37, AND 30, THE LIMITATIONS OF SOIL PROPERTIES ARE SUCH THAT A RESIDENCE WITH NO MORE THAN FIVE (5) BEDROOMS CAN BE SUPPORTED WITHIN THE DESCRIBED SEWAGE DISPOSAL AREA UNLESS AN EXHIBIT PREPARED BY A CERTIFIED PROFESSIONAL ILLUSTRATES THAT ABSOPTION TRENCH AREA FOR MORE BEDROOMS CAN BE ACCOMODATED WITHIN THE SDA. C. ON ALL OTHER LOTS, 6 OR MORE BEDROOMS MAY BE PERMITTED IF AN EXHIBIT DEMONSTRATING THAT THE SDA WILL ACCOMMODATE 3 DRAINFIELDS FOR A RESIDENCE HAVING 6 BEDROOMS OR MORE IS PRESENTED BY A CERTIFIED PROFESSIONAL
- 46. MICRO BIO-RETENTION (M-6) FACILITIES 1 & 3 THRU 7 WILL HAVE IMPERMEABLE LINERS 47. THIS PLAN IS SUBJECT TO A WAIVER (WP-18-001) FROM SECTION 16.116.1.3. - ACCESS RESTRICTIONS, RESTRICTING TWO POINTS OF ACCESS FROM A MINOR ARTERIAL ROADWAY. THE PURPOSE OF THE TWO ACCESSES IS TO SEPARATE THE USE-IN-COMMON RESIDENTIAL DRIVEWAY FROM THE EXISTING FARM USE DRIVEWAY. THIS WAIVER WAS APPROVED BY THE HOWARD COUNTY PLANNING BOARD ON JANUARY 18, 2018 WITH THE FOLLOWING CONDITION:
 - 1. THE APPLICANT SHALL COORDINATE THE DESIGN OF THE DRIVEWAYS FOR FUTURE LOTS 40-44 WITH THE FIRE DEPARTMENT TO ENSURE ADEQUATE VEHICLE TURNAROUND AND ANY NECESSARY PULLOVER AREAS AND WITH THE DEVELOPMENT ENGINEERING DIVISION AND STATE HIGHWAY ADMINISTRATION TO ENSURE ADEQUATE SITE DISTANCE. THE PROPOSED ACCESS MUST MEET ALL SHA ACCESS AND SIGHT DISTANCE REQUIREMENTS.
- 40. THIS PROPERTY IS DESIGNATED AS A TIER III PROPERTY PER THE SUSTAINABLE GROWTH AND AGRICULTURAL ACT OF 2012, MAP 6-3, AS APPROVED BY THE HOWARD COUNTY COUNCIL AS PART OF PLAN HOWARD 2030. 49. LOTS 1, 2 AND 3 HAVE SEWAGE DISPOSAL AREAS THAT ARE UPGRADIENT FROM AN EXISTING WELL AT 1626 DAISY ROAD. LOTS 1, 2 AND 3 SHALL BE CONSIDERED NON-BUILDABLE UNTIL THE DOWNGRADIENT WELL AT 1626 DAISY ROAD IS SEALED. A NEW WELL MUST BE INSTALLED AT 1626 DAISY ROAD AND CONNECTED TO THE
- RESIDENCE PRIOR TO HEALTH DEPARTMENT SIGNATURE OF THE RECORD PLAT. IF THE EXISTING WELL IS TO BE SEALED, IT MUST BE SEALED PRIOR TO HEALTH DEPARTMENT SIGNATURE OF THE RECORD PLAT. PRELIMINARY EQUIVALENT SKETCH &



SHEET 1 of 14



5P-17-003



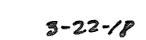
LS LEGEND		
NAME	CLAS5	Kw
to 25 percent slopes	B	.20
nt slopes	В	.20
nt slopes	В	.20
ent slopes	B	.20
percent slopes	С	.37
percent slopes	С	*** .37
to 8 percent slopes	С	*** .37
ent slopes	B	.24

LEGI	END
SYMBOL	DESCRIPTION
	PROPOSED STORM DRAIN LINE
\boxtimes	PROPOSED DRYWELL
777777777777777777777777777777777777	NON-ROOFTOP DISCONN.
	BOUNDARY/RIGHT OF WAY LINE
B.R.L.	BUILDING RESTRICTION LINE
	PROPOSED CURB
W	PROPOSED WELL
	PROPOSED WELL BOX
андалаан далганда улуу алуу алуу алуу алуу алуу алуу ал	EXISTING 10 FT. CONTOUR
anut of all all un all an	EXISTING 2 FT. CONTOUR
	PROPOSED SEPTIC FIELD
	25% OR GREATER SLOPES
	15% - 24.99% SLOPES
~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	EXISTING/PROPOSED TREELINE
463	PASSED PERC
O ³²⁹	FAILED PERC
an de an de la	
Gord Cox	SOIL TYPE

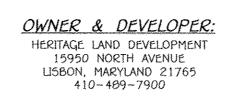


					PERIN	SCHEDU 1ETER LAN	JLE A DSCAPE ED	IGE						
ZONED: RC-DEO	PERIMETER CATEGORY LANDSCAPE TYPE	P-1 P-2 Adjacent to Perimeter Properties Preservation Parcel	P-3 Adjacent to Preservation Parce A	P-4* Adjacent to Roadway C	P-5 Adjacent to Preservation Parcel A	P-6 Front to Roadway N/A	P-7	P0	P-9 Adjacent to Preservation Parcel A	P-10 Adjacent to Preservation Parcel A	P-11 Adjàcent to Roàdway B	P-12 Adjacent to Preservation Parcel A	P-13 Adjacent to Preservation Parcel	P-14 Adjacent to Preservätion Parcel
	LINEAR FEET OR ROADWAY FRONTAGE/PERIMETER CREDIT FOR EXISTING VEGETATION (YES, NO LINEAR FEET) (DESCRIBE BELOW IF NEEDED)	1479.8' 468.9'	2406.2'	-	2350.4'	268.1'	79.6'	659.0°	537.4	419.2'	355.9'	702.3'	386.4'	702.5'
SHEE	CREDIT FOR WALL, FENCE OR BERM (YES, NO LINEAR FEET) (DESCRIBE BELOW IF NEEDED) NUMBER OF PLANTS REQUIRED SHADE TREES EVERGREEN TREES	25 Ø	- 40 -	- 27 54	- 39	-	22	- 11	9	7	7 9	12	6	
SEF	SHRUBS				1. Jan ( 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	EYOND THE LOTS		-BUILDABLE PRESERV	ATION PARCELS TO	SCREEN THE PROPOSI	ed houses from	THE SCENIC ROADV	- I	
CONSERVATION MENT. No. 4 1.56 (Act + planting)			х - х	REALING	SYMBOL	PROF	DESCRIPTION	DRAIN LINE		STREET	TREE SCHE			
PENSTING 100-TEAR					<u>B.R.L.</u>	NON- BOUN	-ROOFTOP DISC IDARY/RIGHT O DING RESTRICTIO	CONN. F WAY LINE	QTY. ROW LENGTH 2562'/40 = 64 TRE ROW LENGTH 3206'/40 =	= 1201' 2 64.05 E5 = 1603' 2	CAL.	COMMENTS D' APART ON PUE (Road 'A') D' APART ON PUE	BUC R/W	
25' WETLAND BUFFER WETLAND WETLAND ABOUT AND GMA					@ 	PROF	POSED CURB POSED WELL POSED WELL BO	x	80 TRE	£5	CAL.	(Road 'B')		
EXISTING FARMING IOPERATION CROSSING	Elevation Northing Easting Point # Elevation		rthing Easting			EXIST	ING 10 FT. CO ING 2 FT. CON OSED SEPTIC I OR GREATER S	TOUR TELD	LINEAR FEET NUMBER OF SH	RUBS PROVIDED:	LOTS 9-11 PA	D: 10 l.f. LOT5	40-44 PAD: 24 10	
FOREST CONSERVATION FOREST CONSERVATION EASEMENT NO. 3 (planting)	552.42         604827.30         1294826.03         349         579.83           550.25         604799.90         1294935.39         350         577.47           551.01         604795.67         1294937.94         351         574.20           548.59         604776.54         1294937.96         352         0.00           551.24         604776.54         1294937.96         353         571.36           548.00         604643.22         1294550.76         354         567.73	7         605826.46         1293937.05         378         565.04         609           0         605844.39         1294018.13         379         559.04         609           605897.93         1293968.49         380         565.54         609           8         605882.67         1294062.19         381         561.32         609	5419.30         1294296.70           5399.05         1294212.60           5355.34         1294275.62           5360.13         1294166.05           5320.60         1294217.59           5302.16         1294283.60	<u> </u>	463	15%	- 24.99% SLO ING/PROPOSED ED PERC	PES	OF THE 2. THE L EXCLU 3. THE P	E PRIVATE USE-IN ANDSCAPING SHALL DING THE SIDE AD ERIMETER LANDSCA	-COMMON MAIN . BE INSTALLED JACENT TO THE APING OBLIGATIO	TENANCE AGREEM AROUND THE PE PUBLIC ROAD R INS WILL BE FULI	ERIMETER OF THE I IGHT-OF-WAY.	PAD
N 606,000 129 309 309 310 461 311	549.66         604672.29         1294513.60         355         568.23           555.05         604647.70         1294422.06         356         563.52           554.28         604707.53         1294431.04         357         562.53           547.82         604692.09         1294579.86         358         564.03           559.96         604674.39         1294330.52         359         560.04	3         605916.70         1294180.94         383         556.56         609           2         606006.60         1294142.84         304         561.61         609           3         605993.70         1294239.54         305         561.55         609           3         605935.43         1294321.95         386         564.67         609           4         606003.83         1294300.80         387         561.71         609	5260.25         1294276.62           5275.71         1294153.43           5193.92         1294216.15           5162.04         1294177.99           5119.79         1294270.50	<u> </u>	0 ³²⁹ mA G		D PERC							
WETLAND A1'	563.94         604685.39         1294130.66         362         559.86           561.29         604660.32         1294033.32         363         558.14	5         606033.96         1294416.55         389         568.09         609           6         605987.57         1294522.65         390         571.56         609           4         606021.82         1294552.75         391         568.30         609           7         605932.88         1294501.83         392         559.01         609	5130.38         1294163.66           5066.77         1294218.61           5006.21         1294210.72           5004.20         1294258.10           5117.96         1294322.94           5215.16         1294328.17							(P1)	7			
319 320 321	561.61         604716.04         1293023.92         444         555.51           557.95         604669.12         1293760.60         445         0.00           563.45         604782.57         1293807.06         446         556.15	3         605963.46         1294655.53         394         554.13         605           605991.57         1294623.56         395         550.98         605           1         605954.19         1294623.15         396         552.00         605           605951.90         1294735.79         397         548.62         605           5         606016.39         1294718.72         398         549.73         605	5158.03         1294382.72           5182.93         1294452.89           5109.02         1294452.00           5126.00         1294528.38           5058.82         1294500.60			(		[				7	$\bigcap$	
324 325 462 325	543.10         604674.72         1293552.73         440         555.10           545.39         604718.55         1293600.74         438         440.00           557.04         604734.02         1293727.38         439         554.25           542.95         604734.02         1293544.10         440         552.00	0         606072.27         1294735.09         399         545.05         605           0         606069.49         1294681.61         400         546.26         605           0         606083.13         1295017.09         401         548.77         605           5         605995.82         1294997.06         402         546.04         605           0         606028.13         1294941.40         403         545.08         605           2         606055.86         1294909.27         404         542.93         605	5214.00         1294615.89           5285.51         1294623.00           5248.40         1294680.13           5293.65         1294742.65		$\bigwedge$						P12			
463 449 450 451	554.56         604682.56         1293248.34         437         551.95           554.78         604728.03         1293266.19         430         552.01           558.13         604705.04         1293152.10         431         550.96	2         606021.79         1295136.31         407         542.24         609           5         606044.30         1295085.50         408         543.24         609           1         605892.11         1295323.45         409         538.91         609           6         605954.63         1295317.61         410         538.64         609	5149.06         1294858.24           5113.99         1294949.60           5173.48         1294964.89           5120.04         1295043.37							P13>			•	
452 453 454 455 456	556.65         604609.40         1293023.54         433         549.95           0.00         604731.47         1292959.36         434         552.35           0.00         604799.74         1292942.89         428         557.31           548.23         604757.10         1292895.63         429         556.37	6         605932.34         1295249.10         412         540.20         605           5         605970.31         1295182.70         470         561.12         607           5         605923.34         1295177.39         471         558.89         607           1         605665.62         1295324.62         472         561.13         607           7         505656.15         1295336.97         473/474         561.25         607           5         605571.93         1295280.64         475         566.45         607	7417.56         1293764.50           7447.20         1293559.63           7392.71         1293660.26           7360.64         1293611.10		,					/		P3-		
450 566 19 1 1 1 5 331 332 333	544.38         604826.99         1292849.61         425         553.02           542.54         604926.84         1292863.03         424         549.80           558.50         605106.45         1293702.29         423         542.95           561.77         605100.03         1293749.83         421         545.86           558.44         605175.39         1293689.56         420         549.86	2         605526.45         1295223.32         476         565.79         607           0         605486.63         1295121.52         477         564.02         607           5         605377.01         1295114.68         478         568.45         607           6         605427.37         1294990.34         479         574.00         607           6         605510.86         1294995.98         480         572.13         607	129362528           129362528           1293573.10           1210.44           1293559.48           1149.46           1293673.29           1142.90           1293549.22			~								(A)
464 335 336 337	551.69         605119.62         1293617.76         418         545.89           563.62         605197.92         1293792.35         417         549.89           558.33         605271.40         1293660.38         416         554.01           560.68         605274.41         1293716.07         415         550.25	5         605452.83         1294923.88         482         575.12         607           9         605390.27         1294861.68         483         569.87         607           9         605456.14         1294852.28         484         569.74         606           1         605531.28         1294835.47         485/486         570.23         606           5         605457.99         1294797.28         487         576.26         606           0         605399.90         1294751.70         489         573.76         606	7048.44         1293615.70           7999.94         1293509.67           79954.67         1293461.22           7892.02         1293558.25										2	
339 340 341 342 343	563.63         605345.41         1293741.32         414         556.00           565.29         605351.77         1293785.07         369         563.86           564.04         605408.25         1293709.19         371         566.51           568.11         605439.49         1293772.85         372         569.70           572.00         605511.04         1293821.72         370         568.12	0         605499.64         1294725.65         488         571.81         606           9         605571.17         1294679.50         490         574.01         606           1         605527.91         1294587.62         491         572.21         606           0         605556.18         1294560.21         492         572.13         606           2         605586.64         1294623.93         493         573.96         606	1293427.65           1293427.65           1293447.11           1293447.11           1293403.09           1293403.09           1293414.07           1669.61           1293465.93			d C C		P9	P10 (P2	A			(P)	6
24	570.60         605543.93         1293763.85         368         569.01           575.77         605624.62         1293833.50         373         567.01           579.20         605694.59         1293807.17         374         563.04           570.80         605728.10         12938039.82         375         565.42           579.40         605760.63         1293804.60         376         559.69	1         605490.41         1294487.58           4         605446.84         1294383.98           2         605484.12         12943836.11	1293377.66				PE	RIMETER LA		BUFFER SCH				
		and the second s	OF MARY	<u>.</u>					No Scale	PRI 15ED PERCO	ELIMINARY DLATION C			CAPE PLAN

TENTATIVELY APPROVED DEPARTMENT OF PLANNING AND ZONING HOWARD COUNTY

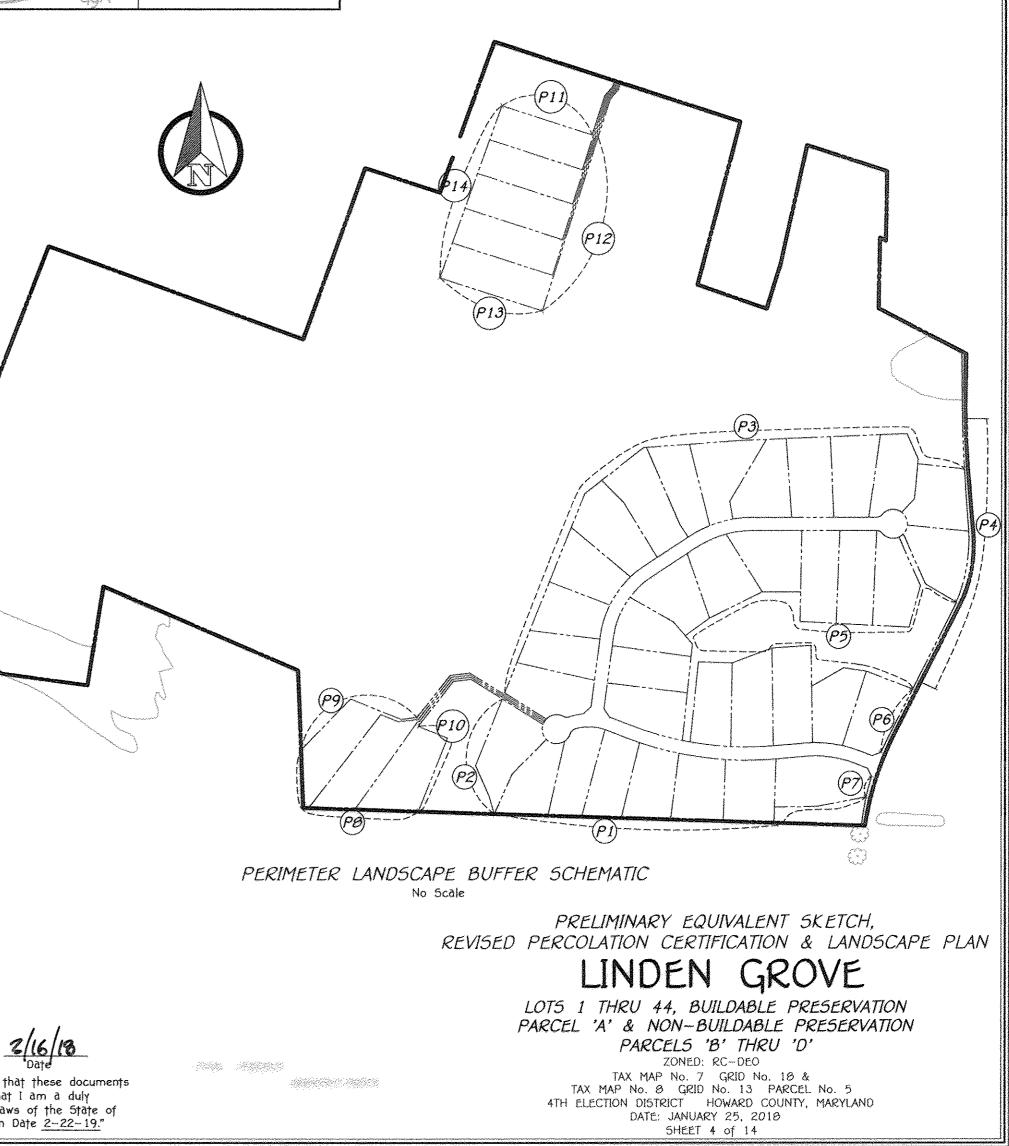


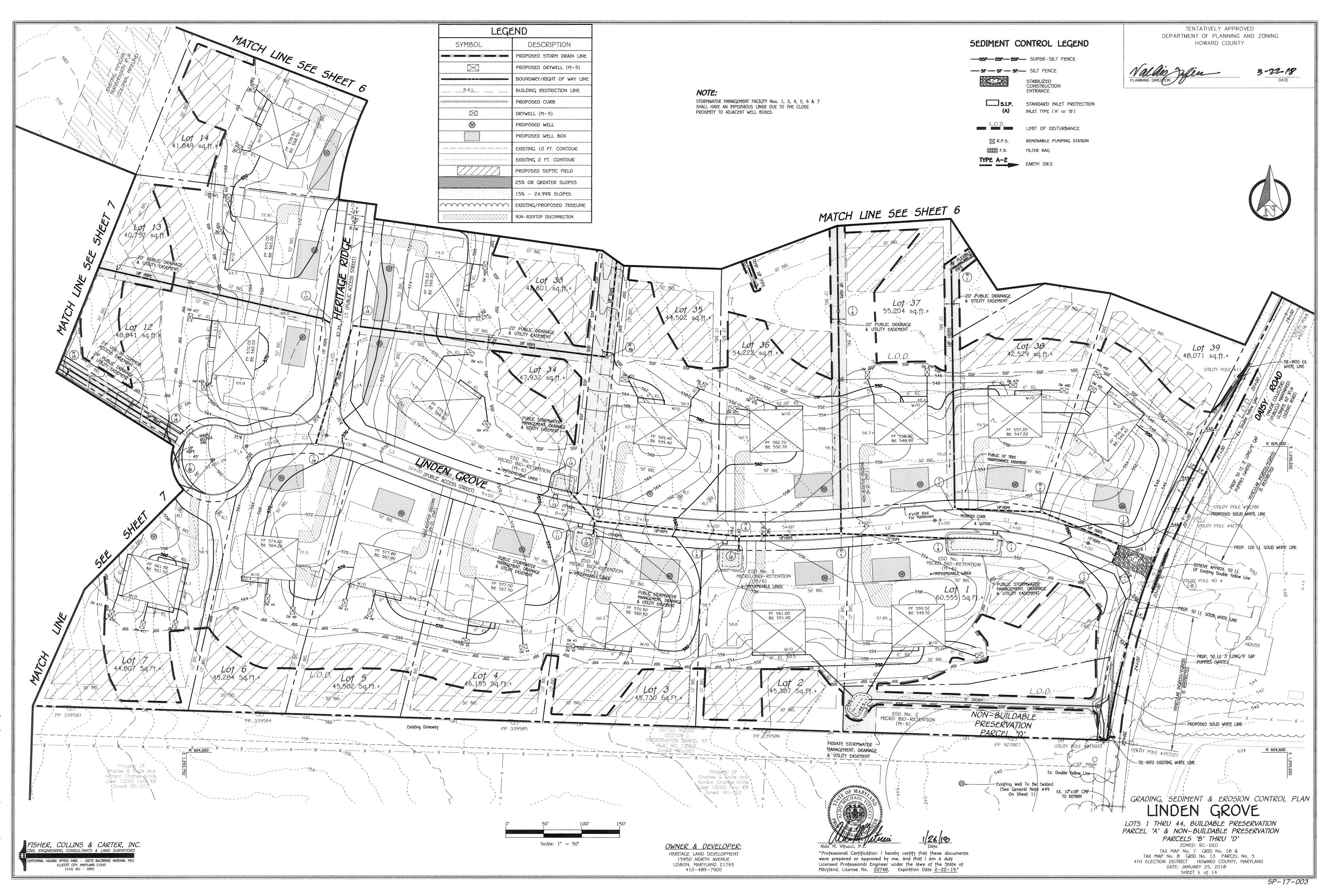
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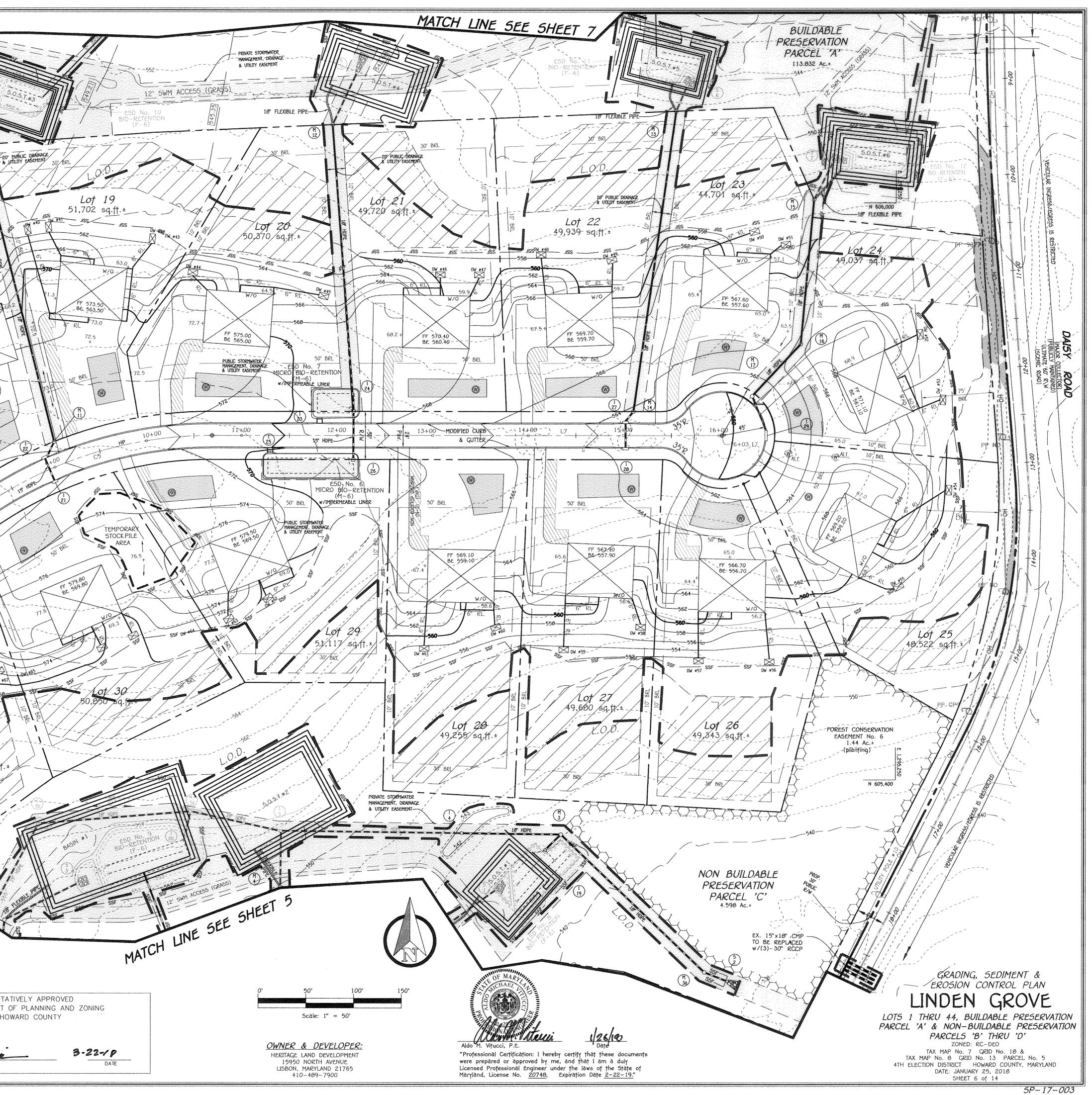
"Professional Certification: I hereby certify that these documents were prepared or approved by me, and that I am a duly Licensed Professional Engineer under the laws of the State of Maryland, License No. <u>20740</u>. Expiration Date <u>2-22-19.</u>"

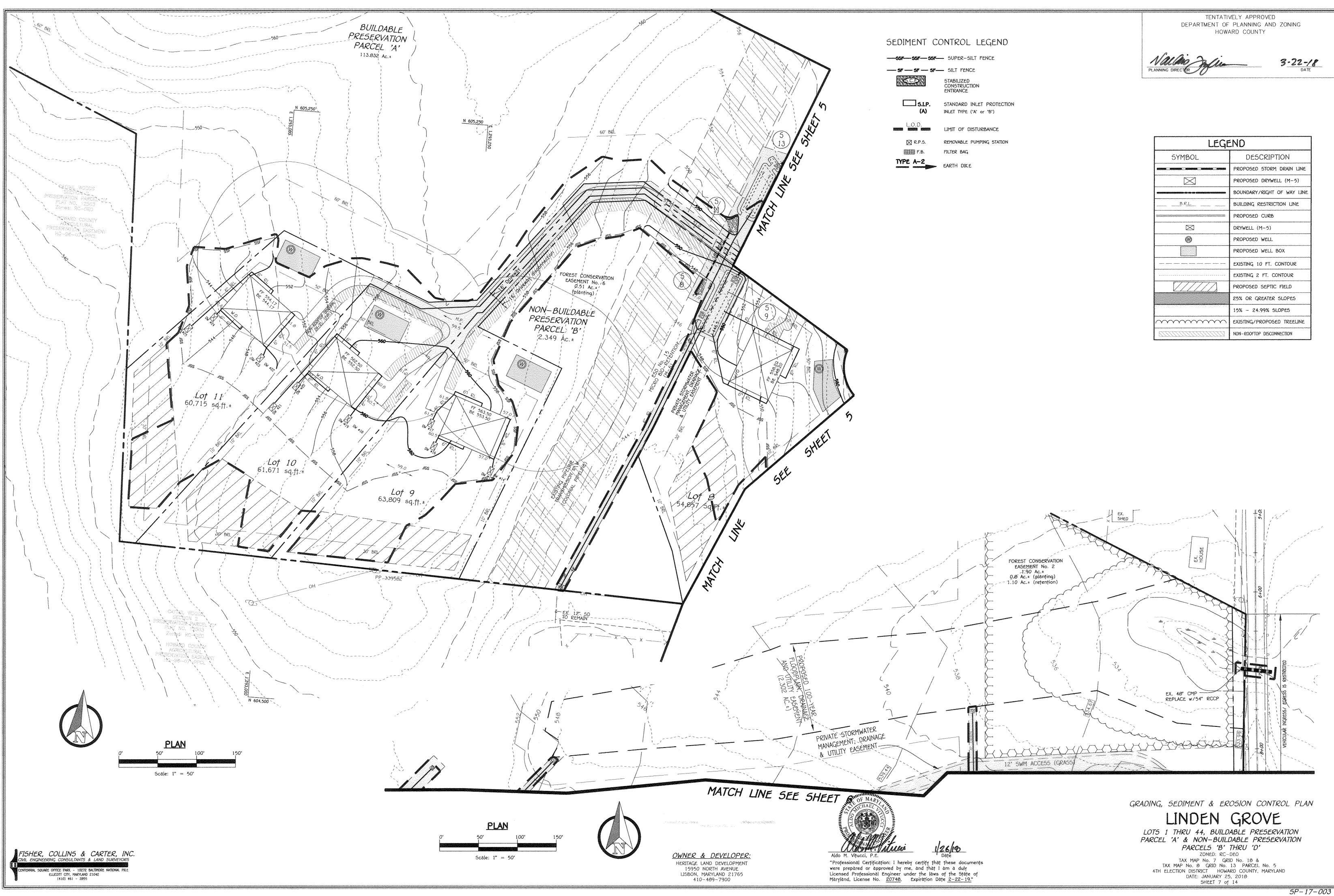




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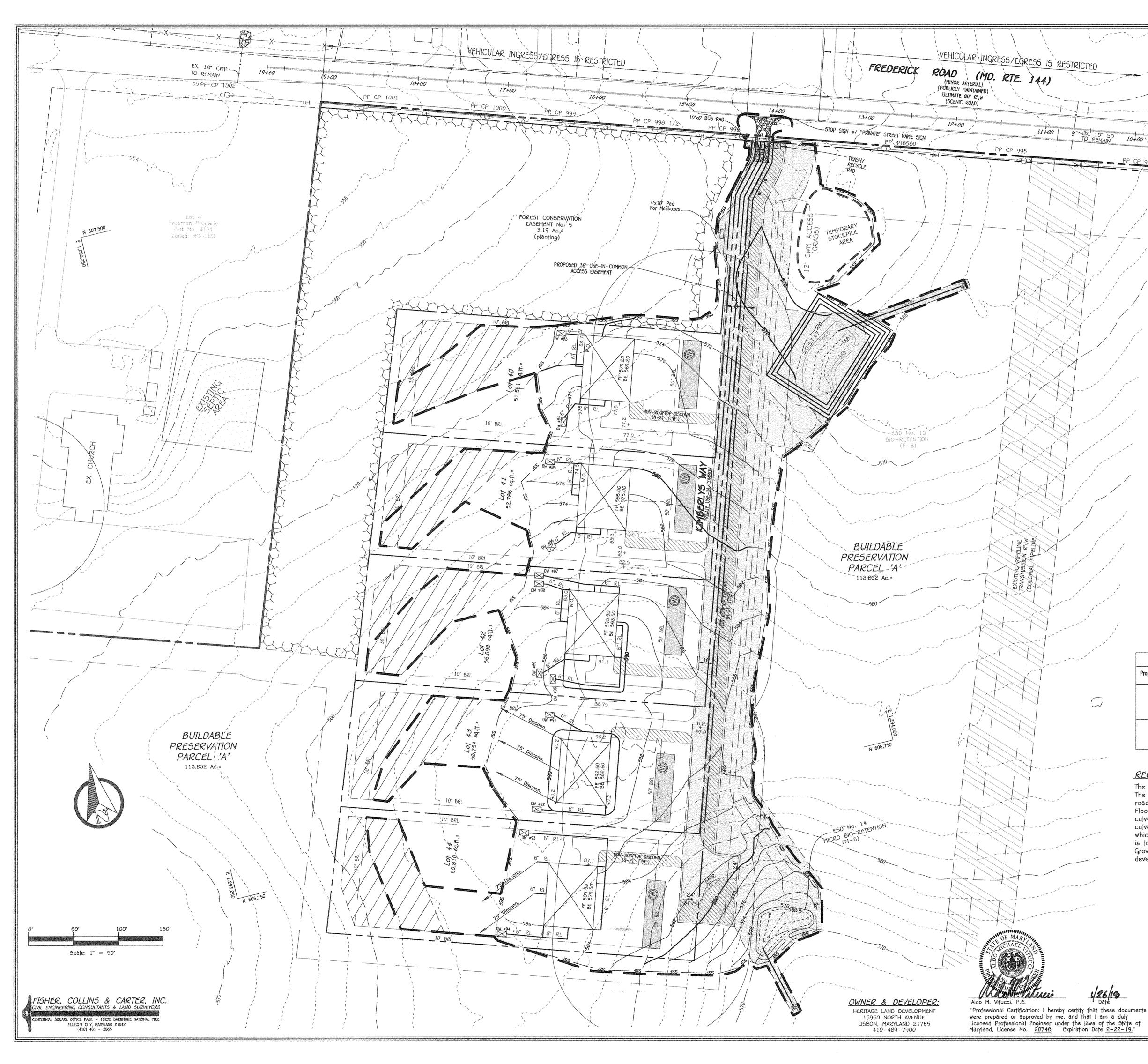
		14		ESD No. 16 BIO-RETENTION			· 570	×, ³ >?
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					PRESERVÀTION PARCEL 'À'			
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	4				1 N 606,000		Reversion of the second s	
		LIC DRAINAGE Y EASEMENT					Wishing Pile	
	- at	and the second		of 17 87_sq.tt_t	59	XXX	4 2 8	
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	FF 579.00 BE 569.00	76.0 FF				1. (/ /Lof	Jrn !	
			1. 20 73.6	. \ \			the list	
	(A) (21a)					V'		
Lot     15     15       Hard     Hard     Hard       Hard     Hard     <	100 C	$\langle / / \rangle$						
49/295 sq.ft       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100	1.5 HOPE	nGF "			00.3×			
49/295 sq.ft       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100       100	H	ALTESS STREE	HERITA					
LEGEND       SYMBOL       DESCRIPTION       PROPOSED STORM DRAIN LINE       PROPOSED DRIVELL (M-5)       BUILDING RESTRICTION LINE       PROPOSED CLUEB       DRYMELL (M-5)       BOILDING RESTRICTION LINE       PROPOSED WELL						A Se		48,295
Image: Stress of the stress	745	50			1. 	Contraction of the second	B STA	
LEGEND         SYMBOL       DESCRIPTION         PROPOSED       STORM DRAIN LINE         BOUNDARY/RIGHT OF WAY LINE         PROPOSED       DRIVELL (M-5)         BOUNDARY/RIGHT OF WAY LINE         PROPOSED       CURB         DRYWELL (M-5)         BORYWELL (M-5)         PROPOSED       DRYWELL	A - A		$\times$ $// \lambda$					
LEGEND         SYMBOL       DESCRIPTION         PROPOSED STORM DRAIN LINE         PROPOSED STORM DRAIN LINE         BOUNDARY/RIGHT OF WAY LINE         BOUNDARY/RIGHT OF WAY LINE         PROPOSED CURB         DRYWELL (M-5)         DRYWELL (M-5)         PROPOSED WELL         PROPOSED WELL	570 W *	We the state	560		St A	516	ORI	
LEGEND         SYMBOL       DESCRIPTION         PROPOSED STORM DRAIN LINE         PROPOSED DRYWELL (M-5)         BOUNDARY/RIGHT OF WAY LINE         BUILDING RESTRICTION LINE         PROPOSED CURB         PROPOSED WELL         PROPOSED WELL         PROPOSED WELL         PROPOSED WELL		- SSF	BRI	$1 \setminus \wedge 1$	- KAR			
SYMBOL       DESCRIPTION         PROPOSED STORM DRAIN LINE         PROPOSED DRYWELL (M-5)         BOUNDARY/RIGHT OF WAY LINE         BUILDING RESTRICTION LINE         PROPOSED CURB         DRYWELL (M-5)         DRYWELL (M-5)         PROPOSED CURB         DRYWELL (M-5)         PROPOSED WELL         PROPOSED WELL	07 31 41 59.55	Lot 47,141						
PROPOSED DRYWELL (M-5)         BOUNDARY/RIGHT OF WAY LINE         B.R.L         BUILDING RESTRICTION LINE         PROPOSED CURB         DRYWELL (M-5)         PROPOSED WELL         PROPOSED WELL	AND			al And		<b>I</b> ///	DESCR	
B.R.L BUILDING RESTRICTION LINE PROPOSED CURB DRYWELL (M-5) PROPOSED WELL PROPOSED WELL					MIN	RYWELL (M-5)	PROPOSED DR	
PROPOSED WELL	$\sum i$	107 32 12 .570/ sq.ft.*; B	8 9 9 40. 10.			IRB	= PROPOSED CL	
		X/X	5			ELL	PROPOSED WE	
EXISTING 10 FT. CONTOUR           EXISTING 2 FT. CONTOUR           NOTE:           STORMWATER MANAGEMENT FACILITY Nos. 1, 3, 4, 5, 6 & 7			1. 3. 4. 5. 6 & 7		l l	FT. CONTOUR	- EXISTING 10 I	
PROPOSED SEPTIC FIELD 25% OR GREATER SLOPES SHALL HAVE AN IMPERVIOUS LINER DUE TO THE CLOSE PROXIMITY TO ADJACENT WELL BOXES.			TO THE CLOSE	E AN IMPERVIOUS LINER DUE	SHALL H	TER SLOPES	25% OR GREA	
15% - 24.99% SLOPES       EXISTING/PROPOSED TREELINE       DEPAR	TENT PARTMENT H	DEPAI				POSED TREELINE	existing/pro	
FISHER, COLLINS & CARTER, INC.	2110	Nalan						FISHER, COLLINS CIVIL ENGINEERING CONSUL
CENTENNAL SQUARE OFFICE PARK - 10272 BALTIMORE NATIONAL PIKE ELLICOTT CITY, MARYLAND 21042 (410) 461 - 2055	<i>Tf</i> 118 	PLANNING DIRECTOR					- 10272 BALTIMORE NATIONAL I VARYLAND 21042	CENTENNIAL SQUARE OFFICE PARK - ELLICOTT CIPY, 1





Nallio Solio
 PLANNING DIRECTOR

LEGEND							
SYMBOL	DESCRIPTION						
	PROPOSED STORM DRAIN LINE						
$\square$	PROPOSED DRYWELL (M-5)						
	BOUNDARY/RIGHT OF WAY LINE						
<u>8.R.L.</u>	BUILDING RESTRICTION LINE						
	PROPOSED CURB						
$\square$	DRYWELL (M-5)						
W	PROPOSED WELL						
	PROPOSED WELL BOX						
	EXISTING 10 FT. CONTOUR						
	EXISTING 2 FT. CONTOUR						
	PROPOSED SEPTIC FIELD						
	25% OR GREATER SLOPES						
	15% - 24.99% SLOPES						
~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	EXISTING/PROPOSED TREELINE						
	NON-ROOFTOP DISCONNECTION						



TENTATIVELY APPROVED DEPARTMENT OF PLANNING AND ZONING HOWARD COUNTY

3-22-18 DATE

SEDIMENT CONTROL LEGEND

<u> </u>	- SUPER-SILT FENCE
5F 5F	- SILT FENCE
	STABILIZED CONSTRUCTION ENTRANCE
(A)	STANDARD INLET PROTECTION INLET TYPE ('A' or 'B')
L.O.D.	LIMIT OF DISTURBANCE
🛛 R.P.5.	REMOVABLE PUMPING STATION
F.B.	FILTER BAG
TYPE A-2	EARTH DIKE

LEGEND							
SYMBOL	DESCRIPTION						
	PROPOSED STORM DRAIN LINE						
\square	PROPOSED DRYWELL (M-5)						
	BOUNDARY/RIGHT OF WAY LINE						
B.R.L.	BUILDING RESTRICTION LINE						
	PROPOSED CURB						
	DRYWELL (M-5)						
0	PROPOSED WELL						
	PROPOSED WELL BOX						
مارستان والمعرفين والمعرفين والمعرفين المرامعين المرامعين والمعرفين والمعرفين والمعرفين والمعرفين والمعرفين	EXISTING 10 FT. CONTOUR						
	EXISTING 2 FT. CONTOUR						
	PROPOSED SEPTIC FIELD						
	25% OR GREATER SLOPES						
	15% – 24.99% SLOPES						
~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	EXISTING/PROPOSED TREELINE						
Electron and the second se	NON-ROOFTOP DISCONNECTION						

	CULVERT DESIGN SUMMARY								
Proposed Culvert	Roadway	lov. lo.	Inv. Out	Ex. Pipe Size	Design Storm	Ex. Q	Design Q	Roadway Elev.	Headwater Elev.
(3) 30° RCCP CULVERTS	Daisy Rd. 5ta. 19+31*	534.80	533.78	15"x10" CMP	50-YR	70.51	66.29	538.29	537.29
54" RCCP CULVERTS	Daisy Rd. Sta. 7+00*	526.80	526.60	46° CMP	100-yr	113.92	152.66	535.00	533.95

### RECOMMENDATIONS:

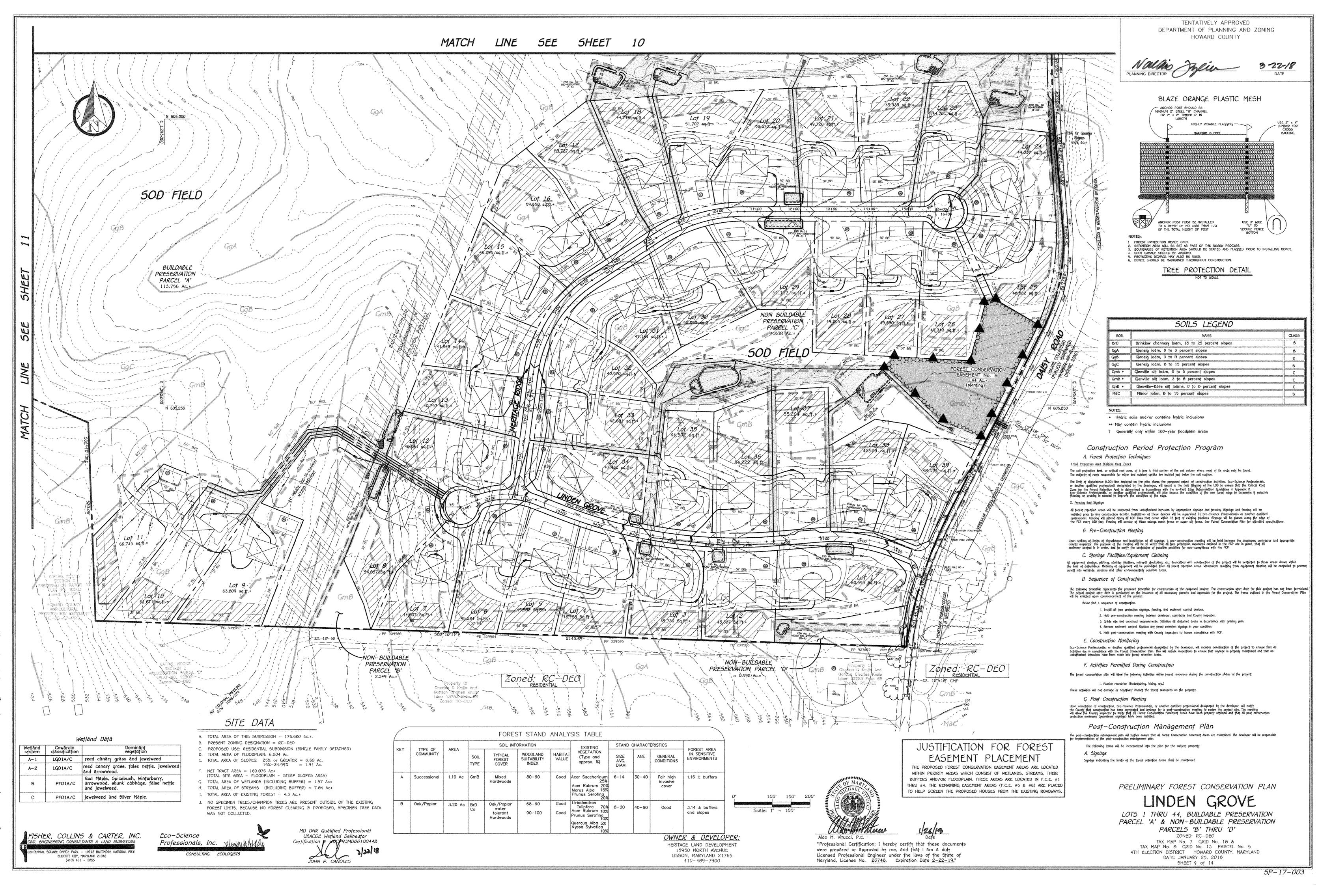
10+00

The culverts are being design on the 10 and 50-year storms pending the classification of the roadways. The requirement of providing 1-foot of freeboard from the design storm headwater elevation to the edge of roadway is a design manual requirement in the Howard County Design Manual Volume I – Storm Drainage and Floodplains. The majority of the culverts will need to be replaced with either multiple culverts or a single pipe culvert that is larger is diameter to obtain the required 1-foot of freeboard. As shown in the chart above in the culvert # column, the proposed pipe information is located there. These culverts vary in size and material type which depends on how much vertical room we have to place the culvert in. Drainage Area 'C''s existing culvert is located well offsite along Daisy Road. This culvert is located 306 feet south of the intersection of Lisbon Grove and Daisy Road intersection. This culvert is located 87'-90' south of the property line. With the development of this site there is not a significant increase in the Q heading to this design point.

GRADING, SEDIMENT & EROSION CONTROL PLAN

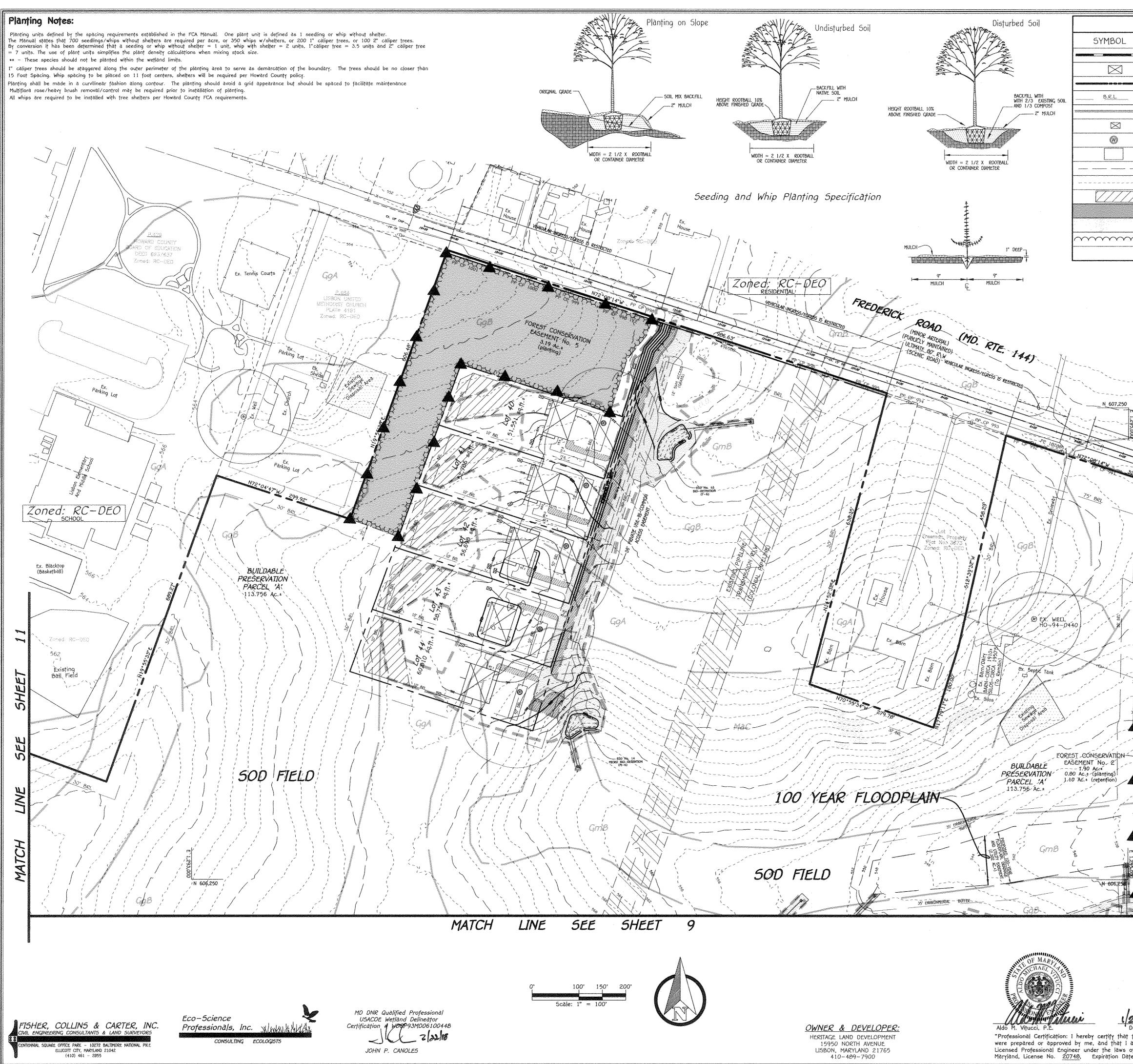
# LINDEN GROVE

LOTS 1 THRU 44, BUILDABLE PRESERVATION PARCEL 'A' & NON-BUILDABLE PRESERVATION PARCELS 'B' THRU 'D' TAX MAP No. 7 GRID No. 18 & TAX MAP No. 7 GRID No. 18 & TAX MAP No. 8 GRID No. 13 PARCEL No. 5 4TH ELECTION DISTRICT HOWARD COUNTY, MARYLAND DATE: JANUARY 25, 2018 SHEET 8 of 14

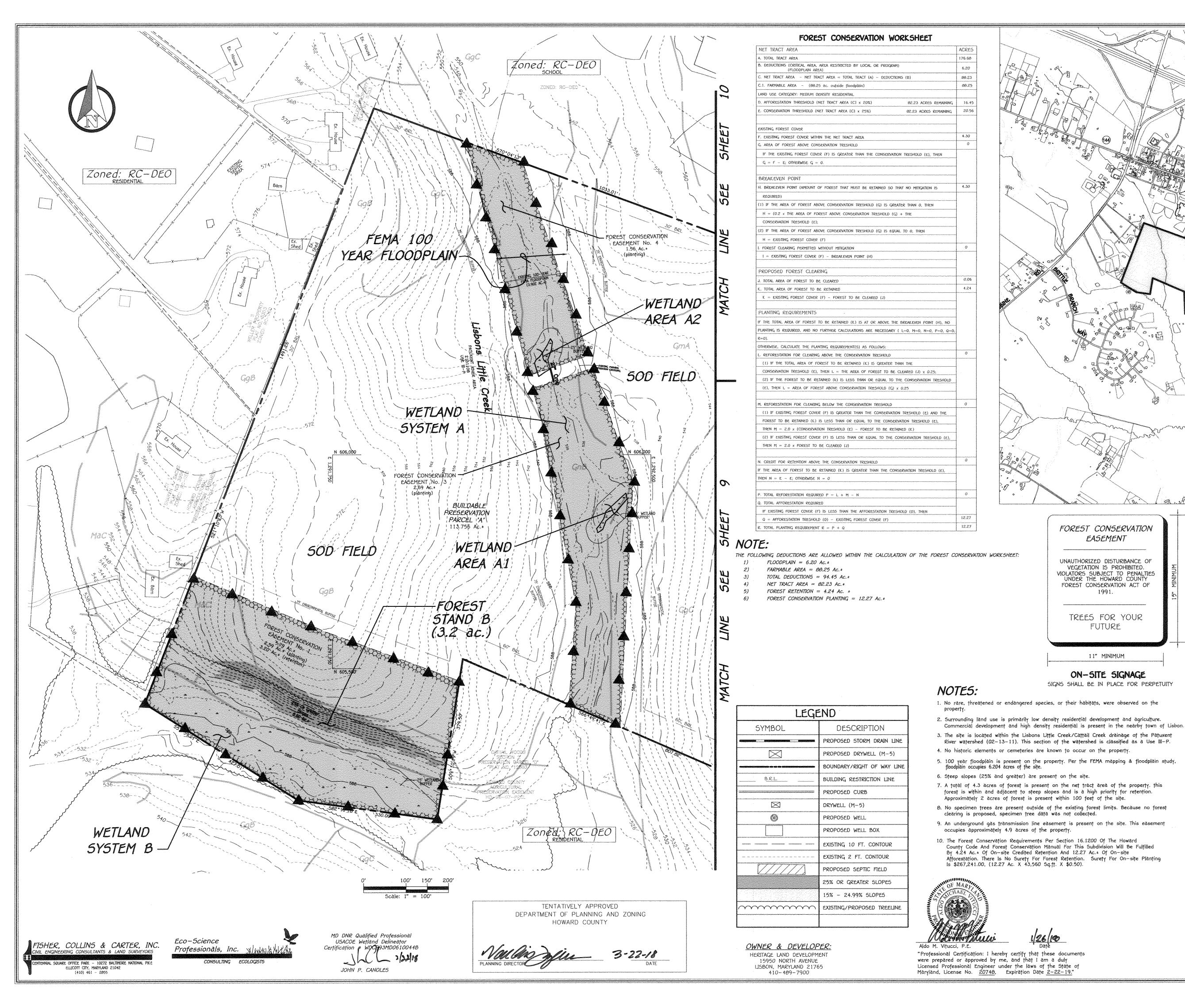


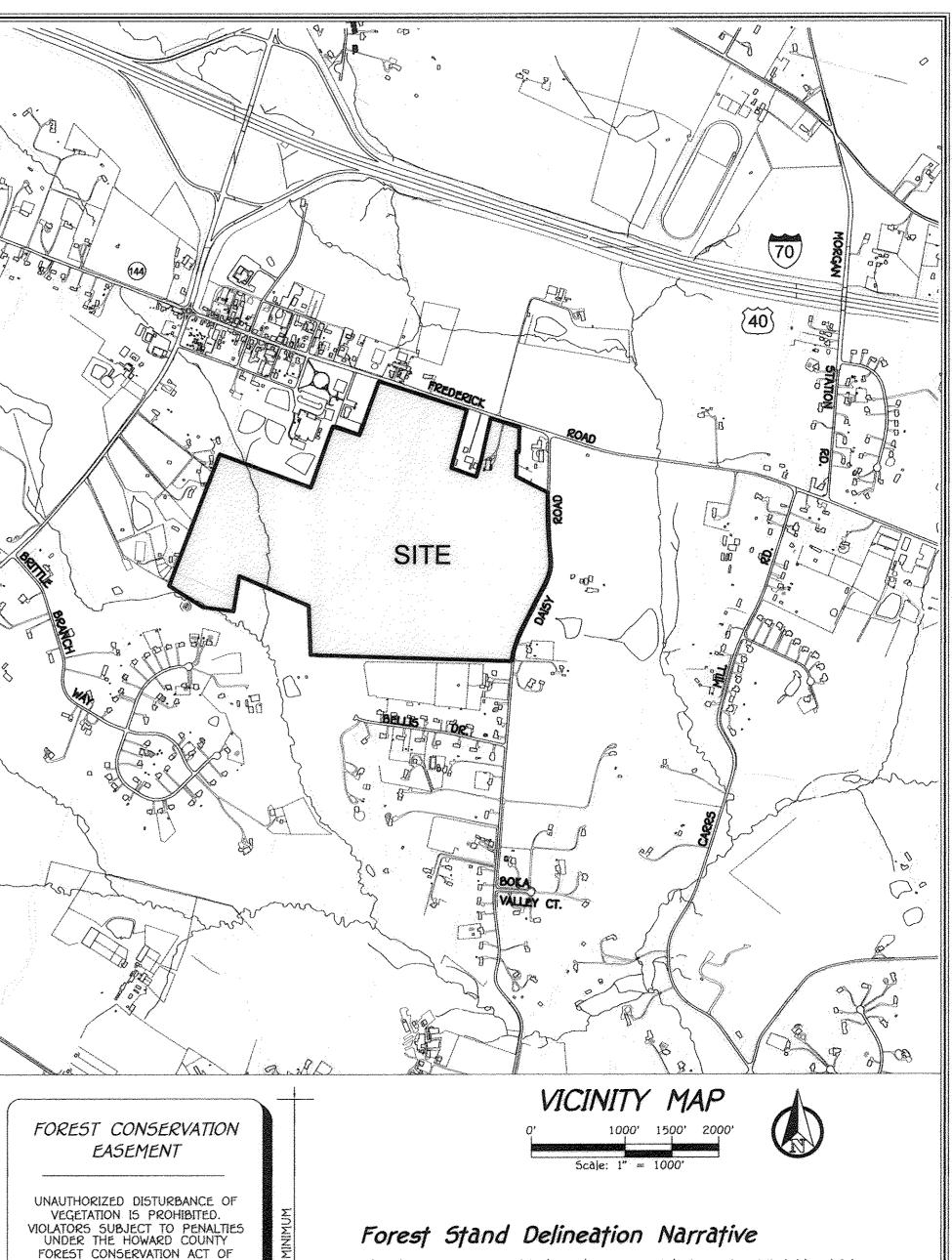
** - These species should not be planted within the wetland limits.

15 Foot Spacing. Whip spacing to be placed on 11 foot centers, shelters will be required per Howard County policy.



LEGEND		TENTATIVELY APPROVED DEPARTMENT OF PLANNING AND ZONING
DESCRIPTION PROPOSED STORM DRAIN LINE		HOWARD COUNTY
PROPOSED DRYWELL (M-5)		Nallin 3-22-18
BOUNDARY/RIGHT OF WAY LINE		PLANNING DIRECTOR DATE
BUILDING RESTRICTION LINE	t	FCE Planțing Area # 1 - 2.59 acres
PROPOSED CURB		Planting units required: 1814 (907 whips) Planting units provided: 1814 (907 whips)
DRYWELL (M-5) PROPOSED WELL		Qty Species Size Spacing Total FC/ Units
PROPOSED WELL BOX		120Acer rubrum - Red maple2-3' whip11' o.c.120Cercis canadensis - Red bud2-3' whip11' o.c.
EXISTING 10 FT. CONTOUR		117Cornus florida - Flowering dogwood2-3' whip11' o.c.110Liriodendron tulipifera - Tulip poplar2~3' whip11' o.c.110Prunus serotina - Black cherry2-3' whip11' o.c.
EXISTING 2 FT. CONTOUR		110     Franks seroinid - black cherning     1.0 whip     11 o.c.       110     Robinia pseudo-acacia - Black locust     2-3' whip     11' o.c.       110     Quercus alba - White oak     2-3' whip     11' o.c.
PROPOSED SEPTIC FIELD		110Viburnum prunifolium - Bläckhäw2-3' whip11' o.c.907 Total whip plantings (2 planting units per tree) =1014 Total FCA unit credit
25% OR GREATER SLOPES 15% - 24.99% SLOPES		WHIPS w/shelters = $350/ACRE$ = $350 \times 2.59 AC$ . = $906.5$ WHIPS 2 Planting units = 1 Whip
EXISTING/PROPOSED TREELINE		FCE Planting Area # 2 - 0.80 acres Planting units required: 560 (280 whips)
		Planting units provided: 560 (280 whips)       Qty     Species       Size     Spacing
		35     Acer rubrum - Red maple     2-3' whip     11' o.c.
PATTERN SPA	CING DIAGRAM	35     Cercis cànàdensis - Red bud     2-3' whip     11' o.c.       35     Cornus floridà - Flowering dogwood     2-3' whip     11' o.c.       35     Liriodendron tulipiferà - Tulip poplar     2-3' whip     11' o.c.
* * * * *	* * * * * *	35     Liriodendron tulipiferà - Tulip poplàr     2-3' whip     11' o.c.       35     Prunus seroțină - Black cherry     2-3' whip     11' o.c.       35     Robinià pseudo-acâciă - Blâck locust     2-3' whip     11' o.c.
* * * * * * * * * * * * * * * * * * * *	* * * * * *	35Quercus alba - White oak2-3' whip11' o.c.35Viburnum prunifolium - Blackhaw2-3' whip11' o.c.
	# # # #	280 Total whip plantings (2 planting units per tree) = $560$ Total FCA unit credit WHIPS w/shetters = $350/ACRE$ = $350 \times 0.80$ AC. = $280$ WHIPS
# # # #	# # # #	2 Planting units = 1 Whip $FCF Planting Area = 3 - 269 acree$
,	tter 11' on center spacing ree 15' on center spacing	FCE Planting Area # 3 - 2.69 acres Planting units required: 1884 (942 whips) Planting units provided: 1884 (942 whips)
TT Species shall	be randomly interspersed, e planting along contours	Qty Species Size Spacing Total FCA Units
		125Acer rubrum - Red maple2-3' whip11' o.c.126Cercis canadensis - Red bud2-3' whip11' o.c.
1.22 29 55		126     Cornus florida - Flowering dogwood     2-3' whip     11' o.c.       125     Liriodendron tulipiferà - Tulip poplar     2-3' whip     11' o.c.
VEHICULAR INGRESS/EGRESS IS RESTRICTED		110     Prunus seroțină - Black cherry     2-3' whip     11' o.c.       110     Robiniă pseudo-acaciă - Black locust     2-3' whip     11' o.c.       110     Quercus albă - White oăk     2-3' whip     11' o.c.
IS RESTRICTED	)	110     Viburnum prunifolium – Błackhaw     2-3' whip     11' o.c.       942 Total whip plantings (2 planting units per tree) =     1884 Total FCA unit credit
321.14		WHIPS w/shelters = $350/ACRE$ = $350 \times 2.69 AC.$ = $941.5$ WHIPS 2 Planting units = 1 Whip
PR CP Store		FCE Planting Area # 4 - 1.56 acres
E C C C C C C C C C C C C C C C C C C C	8	Planting units required: 1092 (546 whips) Planting units provided: 1092 (546 whips) Qty Species Size Spacing Total FCA
1 32 GGA	and the second	Qty         Species         Size         Spacing         Total         FCA           70         Acer rubrum - Red maple         2-3' whip         11' o.c.         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         11'         1'         1'         1'         1'         1'         1'         1'         1'         1' <t< td=""></t<>
Zoned: B-2	A los	70         Cercis cànadensis - Red bud         2-3' whip         11' o.c.           70         Cornus floridà - Flowering dogwood         2-3' whip         11' o.c.
Deros A	e / e /	70     Liriodendron tulipiferà - Tulip poplàr     2-3' whip     11' o.c.       70     Prunus seroțină - Black cherry     2-3' whip     11' o.c.       70     Robiniă pseudo-acăciă - Black locust     2-3' whip     11' o.c.
<pre>/ ' Presempt Traperty / ' Pret No! 4223 * *</pre>		70     Robinia pseudo-acacia - Black locust     2-3' whip     11' o.c.       66     Quercus alba - White oak     2-3' whip     11' o.c.       60     Viburnum prunifolium - Blackhaw     2-3' whip     11' o.c.
Xoned: B-2		546 Total whip plantings (2 planting units per tree) = 1092 Total FCA unit credit WHIPS w/shelters = 350/ACRE = 350 x 1.56 AC. = 546 WHIPS
	0	2 Planting units = 1 Whip
-562651'27'E	AD)	FCE Planting Area # 5 - 3.19 acres Planting units required: 2234 (1117 whips)
Latv2	COLLE AMAIN NIC RO	Planting units provided: 2234 (767 whips and 200 trees) Qty Species Size Spacing Total FCA
Soned: RC4DEC		Units       100     Acer rubrum - Red maple     1" cal.     15' o.c.       100     Quercus alba - White oak     1" cal.     15' o.c.
Ý XÌN	à/ª	200Total 1° caliper trees (3.5 planting units per tree) =700Total FCA unit credit75Acer rubrum - Red maple $2-3^\circ$ whip11' o.c.
Zoned: RC-DEO RESIDENTIAL		75Cercis cànàdensis - Red bud2-3' whip11' o.c.117Cornus floridà - Flowering dogwood2-3' whip11' o.c.
of the state of th	a A A A A A A A A A A A A A A A A A A A	100Uriodendron tulipifera - Tulip poplar2-3' whip11' o.c.100Prunus seroțina - Black cherry2-3' whip11' o.c.
Bit Ne. 3673		100     Robinia pseudo-acacia - Black locust     2-3' whip     11' o.c.       100     Quercus alba - White oak     2-3' whip     11' o.c.
Ex.		100     Viburnum prunifolium - Blackhaw     2-3' whip     11' o.c.       767     Total whip plantings (2 planting units per tree) =     1534     Total FCA unit credit       5%     Total Unit Credit     (1534 + 700)     2234
37		1000000000000000000000000000000000000
A Print Barrier Ba	P Len Aund	3.5 Planting units = $1 - 1^{\circ}$ Cal. Tree 2 Planting units = 1 Whip
E Cit	DUFFER	FCE Planting Area # 6 - 1.44 acres
EX. WEILAND 'C'		Planting units required: 1008 (504 whips) Planting units provided: 1008 (329 whips and 100 trees) Qty Species Size Spacing Total FCA
	EX AS CMP REPLACE W/ 5M RCCP	50         Acer rubrum - Red maple         1" cal.         15' o.c.
		50     Quercus alba - White oak     1" cal.     15' o.c.       - 524     100 Total 1" caliper trees (3.5 planting units per tree) = 350 Total FCA unit credit
- The state		$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
A THE ALL AND		50 Liriodendron tulipifera – Tulip poplar 2–3' whip 11' o.c.
12 SWH ACCESS (2045)		328     40     Robinia pseudo-acacia - Black locust     2-3' whip     11' o.c.       32     40     Quercus alba - White oak     2-3' whip     11' o.c.
		40     Viburnum prunifolium – Blackhaw     2-3' whip     11' o.c.       53-     329 Total whip plantings (2 planting units per tree) =     658 Total FCA unit credit
- FOREST	WETLAND	Total Unit Credit         (658 + 350)         1009           1" CAL. TREES = 200/ACRE (100 TREES/200 = 0.50 AC.)         WHIPS w/shelters = $350/ACRE = 350 \times 0.94$ AC. = $329$ WHIPS
STAND A	SYSTEM C	while's w/shefters = 350/ACKE = 350 x 0.94 AC. = 329 while's 3.5 Planting units = $1 - 1^{\circ}$ Cal. Tree 2 Planting units = 1 Whip
(1.1 AC.)		RELIMINARY FOREST CONSERVATION PLAN
		LINDEN GROVE
		LOTS 1 THRU 44, BUILDABLE PRESERVATION
26/100	F	PARCEL 'A' & NON-BUILDABLE PRESERVATION PARCELS 'B' THRU 'D'
Date t these documents		ZONED: RC-DEO TAX MAP No. 7 GRID No. 18 & TAX MAP No. 8 GRID No. 13 PARCEL No. 5
am a duly		4TH ELECTION DISTRICT HOWARD COUNTY, MARYLAND DATE: JANUARY 25, 2018
of the State of the <u>2-22-19.</u> "		SHEET 10 of 14





The subject property is located in the southwest corner of the intersection of Frederick and Daisy Roads in the Lisbon section of Howard County, Maryland. The property is shown on tax map 8 as parcel 5. The property encompass 176.60 acres of land

The majority of the site is maintained as crop field. At the time of our visit the site the fields were being used to grow soybeans and sod. An underground gas transmission line bisects the property. Forest resources on the property are limited. A small successional forest community, Stand A. is present in a swale located in the northern eastern corner of the site and a larger mature community, Stand B. is present along steep slopes and stream valley in the southwest corner of the property. Stand A is dominated by silver maple, red maple. mulberry and black cherry. The canopy trees are mixed age. The shrub layer includes a high percentage of invasive species including Japanese barberry and multiflora rose. Poison ivy, Japanese honeysuckle and Virginia creeper are also present in the area. This isolated patch of forest occupies approximately 1.1 acres of the site. This forest is associated with a wetland/stream system and associated buffers.

Stand B is a tulip poplar dominated community that includes black cherry, red maple as common canopy associates. Black gum is present in the understory. The shrub layer is heavily influenced by invasive species including barberry, multiflora rose, but also contains spicebush, arrowwood and blackhaw. The canopy trees are generally 10-20 inch diameter with scattered larger individuals. This community occurs along steep slopes and into a stream valley along the property boundary. In wetland and stream areas in the valley bottom red maple is the most common canopy species. This stand occupies approximately 3.2 acres onsite. This community does extend offsite but is the overall forest patch is isolated within the agricultural and

As indicated, the site also contains wetland and stream resources. Three distinct resource areas were identified during our field review. All of these areas are within the Lisbons Little Creek watershed which is part of the Use III-P watershed of Cattall Creek. This system is part of the Brighton Dam/Patuxent

System A is the mainstem of Lisbons Little Creek. This stream cuts across the western end of the property. The perennial stream is deeply incised but does have some adjacent wetland development along seeps that have not been disturbed by past agricultural practices. Wetland Area A1 is dominated by reed canary grass. Though native, this species overwhelms riparian areas and wetlands, particularly areas disturbed by agriculture and other land uses. Jewelweed was also noted in the wetland. A stone foundation was present at the head of the system, this may suggest that a springhouse was once present in this area. Wetland Area A2 has developed within a depression behind a farm crossing of the stream. It appears that floodflows back up into this area causing extended innundation. Reed canary grass, false nettle, jewelweed and arrowwood are present in this portion of the system.

System B includes a stream and wetland complex in the southwestern corner of the site, associated with forest stand B. A broad wetland terrace is present along the base of the steep slopes The wetlands occupy most of the streamside terrace. Red maple, spicebush, winterberry and arrowwood are common woody plants in the wetland. Skunk cabbage, false nettle, and jewelweed are common herbaceous species. This system was field flag with flag line 1-37.

System C is a small headwater wetland seep located within forest stand A in the northeast corner of the site. A deeply incised stream channel has developed as the result of bed and headcut erosion caused by concentrated surface water flows through the area. The stream channel was flowing at the time of our field review. Though the weak flow would suggest that it could be intermittent in nature, we have defined it as a perennial stream for the purpose of this report. Additional monitoring may prove it to be intermittent, Adjacent wetland development is present around the stream head and on terraces above the stream channel. In these areas lewelweed is common. Silver maple is also present along the streambanks. An upland drainageway extends upslope from the groundwater fed stream channel. this drainageway received substantial flows from the adjacent farm fields. A culvert passes the flows under Daisy Road.

> LINDEN GROVE LOTS 1 THRU 44. BUILDABLE PRESERVATION PARCEL 'A' & NON-BUILDABLE PRESERVATION PARCELS 'B' THRU 'D' ZONED: RC-DEO TAX MAP No. 7 GRID No. 18 & TAX MAP No. 8 GRID No. 13 PARCEL No. 5

PRELIMINARY FOREST CONSERVATION PLAN

1/26/100

1991.

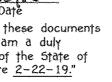
TREES FOR YOUR

FUTURE

11" MINIMUM

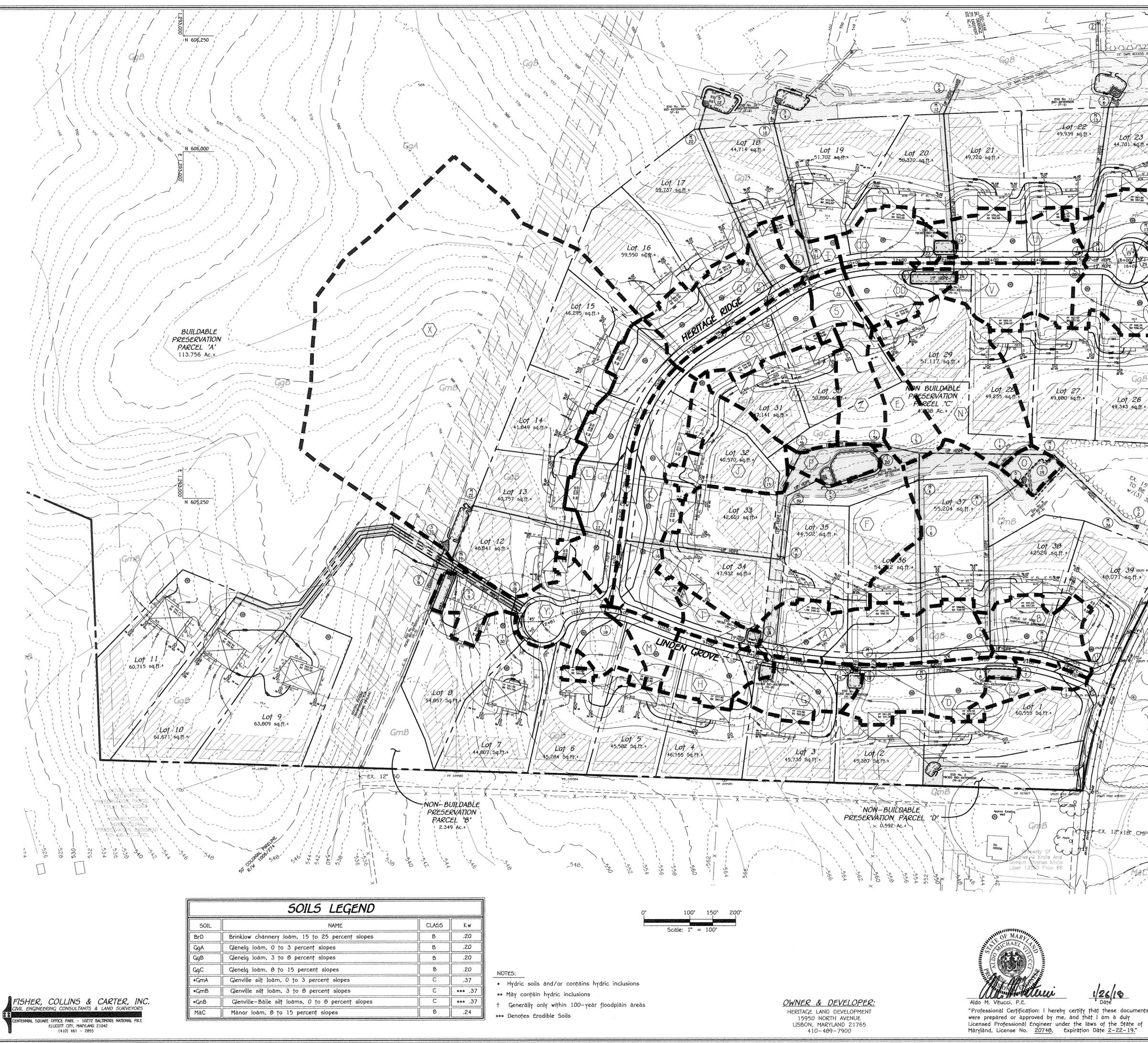
ON-SITE SIGNAGE

SIGNS SHALL BE IN PLACE FOR PERPETUITY



4TH ELECTION DISTRICT HOWARD COUNTY, MARYLAND DATE: JANUARY 25, 2018 SHEET 11 of 14

5P-17-003

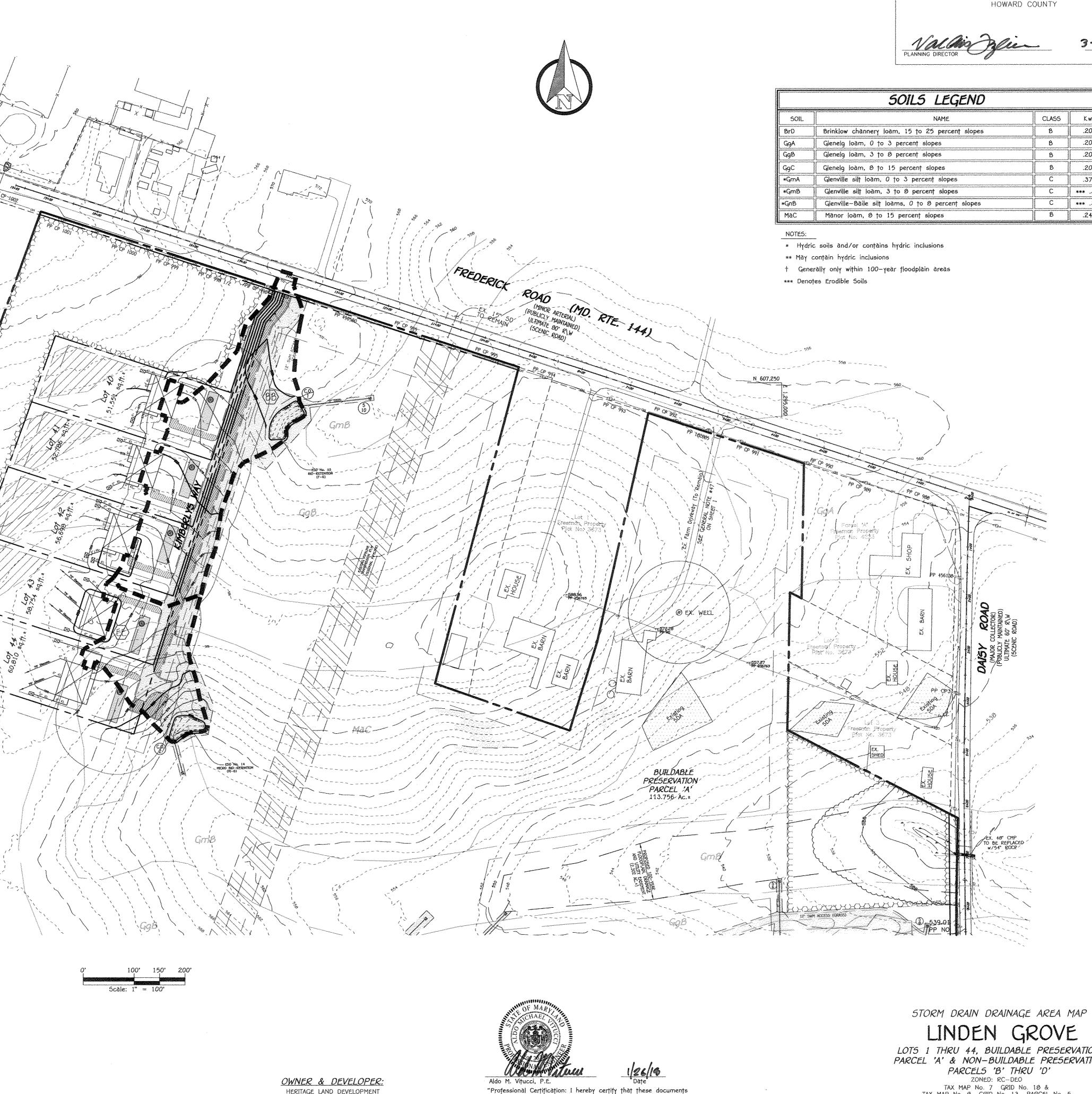


$\frac{1-5}{8} = 0.47 \text{ AC. } \text{RC} - \text{DEO} = 0.25 = 5.00  \text{D} - 4.10  \text{D} - 4.12  \text{M}  0.59 \text{ AC. } \text{RC} - \text{DEO}  0.42  5.00  \text{D} - 4.22  \text{M} \text{D} - 374.62  \text{D} - 4.13  \text{D} - 4.13  \text{AC}  \text{RC} - \text{DEO}  0.43  5.00  \text{D} - 4.22  \text{M} \text{D} - 374.62  \text{D} - 4.14  \text{D} - 16  \text{K}  1.34 \text{ AC. } \text{RC} - \text{DEO}  0.43  5.00  \text{D} - 4.03  \text{D} - 4.10  \text{D} - 4.10 $		-			TENTATIVELY APPROVED DEPARTMENT OF PLANNING AND ZONING HOWARD COUNTY						
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39 van met + 1         DRAINAGE         AREA         ZONED         TC         TME         REMARKES           39 van met + 1	Bit was and the set of the set o	W BE XIE IN ACED	N 605,250 - 532								
39 mm vac       Image: Structure       DRAINAGE       AREA       ZONED       TME       MMARKS         1-1       A       1.35 AC.       RC-DEO       0.46       5.00       D-4.03         1-2       B       0.67 AC.       RC-DEO       0.46       5.00       D-4.03         1-3       C       0.30 AC.       RC-DEO       0.46       5.00       D-4.03         1-7       & 1-8       D       0.84 AC.       RC-DEO       0.41       5.00       D-4.03         1-7       & 1-8       D       0.84 AC.       RC-DEO       0.45       5.00       D-4.03         1-7       & 1-8       D       0.84 AC.       RC-DEO       0.45       5.00       D-4.10         1-6       F       3.13 AC.       RC-DEO       0.42       5.00       D-4.10         1-9       & 1-10       G       0.59 AC.       RC-DEO       0.42       5.00       D-4.10         1-9       & 1-10       G       0.59 AC.       RC-DEO       0.42       MD-374.62         1-13       I-114       I       0.26 AC.       RC-DEO       0.42       MD-374.62         1-13       I-17       H       0.59 AC.       RC-DEO       0.41	39         31         DRAVIACE         AREA         ZONED         TM         REMARKS           1-1         A         1.35 AC         RC-DED         0.45         5.00         D-4.03           1-2         B         0.637 AC         RC-DED         0.49         5.00         D-4.03           1-3         C         0.30 AC         RC-DED         0.49         5.00         D-4.03           1-7         B         D         0.44 AC         RC-DED         0.41         5.00         D-4.03           1-7         B         D         D.44 AC         RC-DED         0.45         5.00         D-4.10           1-5         E         0.47 AC         RC-DED         0.45         5.00         D-4.12         410-374.69           1-9         M         1-10         G         0.59 AC         RC-DED         0.42         410-374.69           1-13         M         1-14         D.25 AC         RC-DED         0.42         410-374.69           1-14         D.26 AC         RC-DED         0.42         410-374.69         1.11         1.13         1.12         1.13         1.14         1.28         RC-DED         0.27         5.00         D-4.22										
STRUCTURE NO.         DRAINAGE AREA         AREA         ZONED         TC         TIME FACTOR         REMARKS           I-1         A         1.35 AC.         RC-DEO         0.46         5.00         D-4.03           I-2         B         0.67 AC.         RC-DEO         0.44         5.00         D-4.03           I-2         B         0.67 AC.         RC-DEO         0.49         5.00         D-4.03           I-3         C         0.30 AC.         RC-DEO         0.41         5.00         D-4.03           I-7         & I-8         D         0.84 AC.         RC-DEO         0.45         5.00         D-4.22 & MD-374.66           I-7         & I-9         D         0.94 AC.         RC-DEO         0.42         5.00         D-4.22 & MD-374.66           I-7         & I-10         G         0.59 AC.         RC-DEO         0.42         5.00         D-4.22 & MD-374.66           I-11         & I-10         G         0.59 AC.         RC-DEO         0.42         3.00         D-4.22 & MD-374.66           I-13         & I-10         G         0.59 AC.         RC-DEO         0.43         5.00         D-4.10           I-18         M-14         I <td< th=""><th>STRUCTURE         DRAMACE         AREA         ZONED         FCCOR         (Mb)         REMARKS           1-1         A         1.35 AC         RC-DEO         0.46         5.00         D-4.03           1-2         B         0.67 AC         RC-DEO         0.46         5.00         D-4.03           1-3         C         0.30 AC         RC-DEO         0.41         5.00         D-4.03           1-7         &amp; 1-8         D         0.30 AC         RC-DEO         0.41         5.00         D-4.03           1-7         &amp; 1-8         D         0.34 AC         RC-DEO         0.45         5.00         D-4.03           1-7         &amp; 1-8         D         0.24 AC         RC-DEO         0.42         8.MD-374.68           1-5         E         0.47 AC         RC-DEO         0.42         8.MD-374.68           1-13         1-12         H         0.25 AC         RC-DEO         0.42         8.MD-374.68           1-13         J         0.33 AC         RC-DEO         0.42         8.MD-374.68           1-14         D-26 AC         RC-DEO         0.47         5.00         D-4.03           1-14         D-26 AC         RC-DEO         <td< th=""><th>all all all all all all all all all all</th><th>WESS !!</th><th></th><th></th><th></th><th></th><th></th></td<></th></td<>	STRUCTURE         DRAMACE         AREA         ZONED         FCCOR         (Mb)         REMARKS           1-1         A         1.35 AC         RC-DEO         0.46         5.00         D-4.03           1-2         B         0.67 AC         RC-DEO         0.46         5.00         D-4.03           1-3         C         0.30 AC         RC-DEO         0.41         5.00         D-4.03           1-7         & 1-8         D         0.30 AC         RC-DEO         0.41         5.00         D-4.03           1-7         & 1-8         D         0.34 AC         RC-DEO         0.45         5.00         D-4.03           1-7         & 1-8         D         0.24 AC         RC-DEO         0.42         8.MD-374.68           1-5         E         0.47 AC         RC-DEO         0.42         8.MD-374.68           1-13         1-12         H         0.25 AC         RC-DEO         0.42         8.MD-374.68           1-13         J         0.33 AC         RC-DEO         0.42         8.MD-374.68           1-14         D-26 AC         RC-DEO         0.47         5.00         D-4.03           1-14         D-26 AC         RC-DEO <td< th=""><th>all all all all all all all all all all</th><th>WESS !!</th><th></th><th></th><th></th><th></th><th></th></td<>	all	WESS !!								
NO.         AREA         ACA         ENLD         FACTOR         (Min.)         ENHAD           I-1         A         1.35 AC.         RC-DEO         0.46         5.00         0-4.03           I-2         B         0.67 AC.         RC-DEO         0.49         5.00         0-4.03           I-2         B         0.67 AC.         RC-DEO         0.41         5.00         0-4.03           I-3         C         0.30 AC.         RC-DEO         0.45         5.00         0-4.03           I-7         I-8         D         0.84 AC.         RC-DEO         0.45         5.00         0-4.03           I-7         I-8         D         0.84 AC.         RC-DEO         0.42         \$MO-374.66           I-7         I-10         G         0.59 AC.         RC-DEO         0.42         \$MD-374.66           I-11 & I-12         H         0.59 AC.         RC-DEO         0.42         \$MD-374.66           I-13 & I-14         I         0.26 AC.         RC-DEO         0.42         \$MD-374.66           I-13         I-14         I         0.26 AC.         RC-DEO         0.43         5.00         D-4.14           I-15         J         0.93	NO.         ARCA         LOND         FACTOR         (Min.)         LOND           I-1         A         1.35 AC.         SC-DED         0.40         0.00         0-4.03           I-2         S         0.67 AC.         RC-DED         0.49         5.00         0-4.03           I-2         S         0.67 AC.         RC-DED         0.49         5.00         0-4.03           I-3         C         0.30 AC.         RC-DED         0.41         5.00         0-4.03           I-7         K         I-6         0         0.44 AC.         RC-DED         0.25         5.00         0-4.10           I-5         E         0.47 AC.         RC-DED         0.25         5.00         0-4.12         MD-374.68           I-19         AI-10         Q.59 AC.         RC-DED         0.43         5.00         0-4.22         MD-374.68           I-11 & I-12         H         0.59 AC.         RC-DED         0.43         5.00         0-4.22         MD-374.68           I-13         I-17         L         1.43 AC.         RC-DED         0.43         5.00         0-4.03           I-11         N         D.59 AC.         RC-DED         0.44         5.00 </th <th></th> <th>A LA LA</th> <th></th> <th></th> <th></th> <th></th> <th></th>		A LA								
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	I-3         C         0.30         AC         RC-DEO         0.41         5.00         D-4.03           I-7         A         I-8         0         0.84         C.         RC-DEO         0.45         5.00         D-4.22         M MO-374.66           I-5         €         0.47         AC.         RC-DEO         0.25         5.00         D-4.22         M MO-374.66           I-6         F         3.13         AC.         RC-DEO         0.22         5.00         D-4.22         M MO-374.66           I-9         A         I-10         G         0.59         AC.         RC-DEO         0.42         5.00         D-4.22         M MO-374.66           I-13         A         I-14         0.56         AC.         RC-DEO         0.42         5.00         D-4.22         M MO-374.66           I-13         A         I-14         0.76         AC.         RC-DEO         0.43         5.00         D-4.22         M MO-374.66           I-17         L         1.43         AC.         RC-DEO         0.43         5.00         D-4.03           I-17         L         1.43         AC.         RC-DEO         0.43         5.00         D-4.03 <td></td> <td>Contraction of the second seco</td> <td>DRAINAGE T</td> <td></td> <td>'C'</td> <td>TIME</td> <td>DEMADY 6</td>		Contraction of the second seco	DRAINAGE T		'C'	TIME	DEMADY 6			
$\frac{1-5}{3} = \frac{1}{6} - \frac{5}{6} = \frac{1}{6} - \frac{4}{7} - \frac{4}{7} - \frac{1}{6} - \frac{5}{6} - \frac{5}{6} - \frac{1}{6} - \frac{5}{6} - $	Instrume		STRUCTURE NO. 1-1	AREA	AREA ZONED 1.35 AC. RC-DEO	'C' FACTOR 0.46	TIME (Min.) 5.00	0-4.03			
$\begin{bmatrix} 1-9 & 1-10 & 4 & 1-10 & 4 & 0.59 & AC. & RC-DED & 0.42 & 5.00 & D-4.22 & MD-374.62 \\ \hline 1-11 & 1-12 & H & 0.59 & AC. & RC-DED & 0.52 & 5.00 & D-4.22 & MD-374.62 \\ \hline 1-13 & 1-14 & I & 0.26 & AC. & RC-DED & 0.43 & 5.00 & D-4.22 & MD-374.62 \\ \hline 1-15 & J & 0.93 & AC. & RC-DED & 0.43 & 5.00 & D-4.22 & MD-374.62 \\ \hline 1-16 & K & 1.34 & AC. & RC-DED & 0.48 & 5.00 & D-4.03 \\ \hline 1-17 & L & 1.43 & AC. & RC-DED & 0.48 & 5.00 & D-4.03 \\ \hline 1-18 & M & 0.28 & AC. & RC-DED & 0.45 & 5.00 & D-4.03 \\ \hline 1-19 & O & 0.18 & AC. & RC-DED & 0.45 & 5.00 & D-4.03 \\ \hline 1-19 & O & 0.18 & AC. & RC-DED & 0.45 & 5.00 & D-4.22 \\ \hline 1-20 & P & 0.30 & AC. & RC-DED & 0.44 & 5.00 & D-4.22 \\ \hline 1-31 & Q & 1.00 & AC. & RC-DED & 0.44 & 5.00 & D-4.03 \\ \hline 1-32 & R & 0.70 & AC. & RC-DED & 0.44 & 5.00 & D-4.03 \\ \hline 1-22 & 5 & 0.28 & AC. & RC-DED & 0.44 & 5.00 & D-4.22 & MD-374.62 \\ \hline 1-21 & T & 0.24 & AC. & RC-DED & 0.41 & 5.00 & D-4.22 & MD-374.62 \\ \hline 1-21 & T & 0.24 & AC. & RC-DED & 0.41 & 5.00 & D-4.22 & MD-374.62 \\ \hline 1-21 & T & 0.24 & AC. & RC-DED & 0.41 & 5.00 & D-4.22 & MD-374.62 \\ \hline 1-21 & T & 0.24 & AC. & RC-DED & 0.41 & 5.00 & D-4.22 & MD-374.62 \\ \hline 1-21 & T & 0.24 & AC. & RC-DED & 0.41 & 5.00 & D-4.22 & MD-374.62 \\ \hline 1-21 & T & 0.24 & AC. & RC-DED & 0.41 & 5.00 & D-4.22 & MD-374.62 \\ \hline 1-21 & T & 0.24 & AC. & RC-DED & 0.41 & 5.00 & D-4.22 & MD-374.62 \\ \hline 1-21 & T & 0.24 & AC. & RC-DED & 0.41 & 5.00 & D-4.22 & MD-374.62 \\ \hline 1-21 & T & 0.24 & AC. & RC-DED & 0.41 & 5.00 & D-4.22 & MD-374.62 \\ \hline 1-21 & T & 0.24 & AC. & RC-DED & 0.41 & 5.00 & D-4.22 & MD-374.62 \\ \hline 1-21 & T & 0.24 & AC. & RC-DED & 0.41 & 5.00 & D-4.22 & MD-374.62 \\ \hline 1-21 & T & 0.24 & AC. & RC-DED & 0.41 & 5.00 & D-4.22 & MD-374.62 \\ \hline 1-21 & T & 0.24 & AC. & RC-DED & 0.41 & 5.00 & D-4.22 & MD-374.62 \\ \hline 1-21 & T & 0.24 & AC. & RC-DED & 0.41 & 5.00 & D-4.22 & MD-374.62 \\ \hline 1-21 & T & 0.24 & AC. & RC-DED & 0.41 & 5.00 & D-4.22 & MD-374.62 \\ \hline 1-21 & T & 0.24 & AC. & RC-DED & 0.41 & 5.00 & D-4.22 & MD-374.62 \\ \hline 1-21 & T & 0.24 & AC. & RC-DED & 0.41 & 5.00 & D-4.22 & MD-374.62 \\ \hline 1-21 & $	I-9% & I-10       G       0.59 AC.       RC-DED       0.42       5.00       0-4.22       & MD-374.68         I-113       & I-14       I       0.59 AC.       RC-DED       0.42       \$.00       D-4.22       & MD-374.68         I-13       & I-14       I       0.26 AC.       RC-DED       0.43       \$.00       D-4.22       & MD-374.68         I-13       & I-17       L       1.43 AC.       RC-DED       0.27       \$.00       D-4.14         I-16       K       1.34 AC.       RC-DED       0.49       \$.00       D-4.03         I-17       L       1.43 AC.       RC-DED       0.49       \$.00       D-4.03         I-17       L       1.43 AC.       RC-DED       0.49       \$.00       D-4.03         I-18       M       0.28 AC.       RC-DED       0.45       \$.00       D-4.03         I-18       M       0.28 AC.       RC-DED       0.45       \$.00       D-4.03         I-19       O       0.18 AC.       RC-DED       0.45       \$.00       D-4.03         I-20       P       0.30 AC.       RC-DED       0.44       \$.00       D-4.03         I-22       S       0.28 AC.		STRUCTURE NO. 1-1 1-2 1-3	AREA A B C	AREA         ZONED           1.35         AC.         RC-DEO           0.67         AC.         RC-DEO           0.30         AC.         RC-DEO	,C' FACTOR 0.46 0.49 0.41	TIME (Min.) 5.00 5.00 5.00	0-4.03 0-4.03 0-4.03			
$\begin{bmatrix} 1-15 & J & 0.93 \text{ AC. } \text{RC}-\text{DEO} & 0.27 & 5.00 & D-4.14 \\ \hline I-16 & \text{K} & 1.34 \text{ AC. } \text{RC}-\text{DEO} & 0.48 & 5.00 & D-4.03 \\ \hline I-17 & L & 1.43 \text{ AC. } \text{RC}-\text{DEO} & 0.48 & 5.00 & D-4.03 \\ \hline I-17 & L & 1.43 \text{ AC. } \text{RC}-\text{DEO} & 0.47 & 5.00 & D-4.03 \\ \hline I-18 & \text{M} & 0.28 \text{ AC. } \text{RC}-\text{DEO} & 0.39 & 5.00 & D-4.03 \\ \hline I-4 & \text{N} & 1.59 \text{ AC. } \text{RC}-\text{DEO} & 0.45 & 5.00 & D-4.10 \\ \hline I-19 & O & 0.18 \text{ AC. } \text{RC}-\text{DEO} & 0.25 & 5.00 & D-4.22 \\ \hline I-20 & \text{P} & 0.30 \text{ AC. } \text{RC}-\text{DEO} & 0.30 & 5.00 & D-4.22 \\ \hline I-31 & Q & 1.00 \text{ AC. } \text{RC}-\text{DEO} & 0.44 & 5.00 & D-4.03 \\ \hline I-32 & \text{R} & 0.70 \text{ AC. } \text{RC}-\text{DEO} & 0.44 & 5.00 & D-4.03 \\ \hline I-22 & 5 & 0.28 \text{ AC. } \text{RC}-\text{DEO} & 0.44 & 5.00 & D-4.03 \\ \hline I-21 & \text{T} & 0.24 \text{ AC. } \text{RC}-\text{DEO} & 0.41 & 5.00 & D-4.22 \text{ MD}-374.68 \\ \hline I-21 & \text{T} & 0.24 \text{ AC. } \text{RC}-\text{DEO} & 0.41 & 5.00 & D-4.22 \text{ MD}-374.68 \\ \hline I-21 & \text{T} & 0.24 \text{ AC. } \text{RC}-\text{DEO} & 0.41 & 5.00 & D-4.22 \text{ MD}-374.68 \\ \hline I-21 & \text{T} & 0.24 \text{ AC. } \text{RC}-\text{DEO} & 0.41 & 5.00 & D-4.22 \text{ MD}-374.68 \\ \hline I-21 & \text{T} & 0.24 \text{ AC. } \text{RC}-\text{DEO} & 0.41 & 5.00 & D-4.22 \text{ MD}-374.68 \\ \hline I-21 & \text{T} & 0.24 \text{ AC. } \text{RC}-\text{DEO} & 0.41 & 5.00 & D-4.22 \text{ MD}-374.68 \\ \hline I-21 & \text{T} & 0.24 \text{ AC. } \text{RC}-\text{DEO} & 0.41 & 5.00 & D-4.22 \text{ MD}-374.68 \\ \hline I-21 & \text{T} & 0.24 \text{ AC. } \text{RC}-\text{DEO} & 0.41 & 5.00 & D-4.22 \text{ MD}-374.68 \\ \hline I-21 & \text{T} & 0.24 \text{ AC. } \text{RC}-\text{DEO} & 0.41 & 5.00 & D-4.22 \text{ MD}-374.68 \\ \hline I-21 & \text{T} & 0.24 \text{ AC. } \text{RC}-\text{DEO} & 0.41 & 5.00 & D-4.22 \text{ MD}-374.68 \\ \hline I-21 & \text{T} & 0.24 \text{ AC. } \text{RC}-\text{DEO} & 0.41 & 5.00 & D-4.22 \text{ MD}-374.68 \\ \hline I-21 & \text{T} & 0.24 \text{ AC. } \text{RC}-\text{DEO} & 0.41 & 5.00 & D-4.22 \text{ MD}-374.68 \\ \hline I-21 & \text{T} & 0.24 \text{ AC. } \text{RC}-\text{DEO} & 0.41 & 5.00 & D-4.22 \text{ MD}-374.68 \\ \hline I-21 & \text{T} & 0.24 \text{ AC. } \text{RC}-\text{DEO} & 0.41 & 5.00 & D-4.22 \text{ MD}-374.68 \\ \hline I-21 & \text{T} & 0.24 \text{ AC. } \text{RC}-\text{DEO} & 0.41 & 5.00 & D-4.22 \text{ MD}-374.68 \\ \hline I-21 & \text{T} & 0.24 \text{ AC. } \text{RC}-\text{DEO} & 0.41 & 5.00 & D-4.22 \text{ MD}-374.68 \\ \hline I$	i-15       J       0.93       AC.       RC-DEO       0.27       5.00       D-4.14         i-16       K       1.34       AC.       RC-DEO       0.40       5.00       D-4.03         i-17       L       1.43       AC.       RC-DEO       0.47       5.00       D-4.03         i-18       M       0.28       AC.       RC-DEO       0.49       5.00       D-4.03         i-19       0       0.18       AC.       RC-DEO       0.45       5.00       D-4.03         i-20       P       0.30       AC.       RC-DEO       0.45       5.00       D-4.22         i-31       Q       1.00       AC.       RC-DEO       0.45       5.00       D-4.22         i-32       R       0.70       AC.       RC-DEO       0.44       5.00       D-4.03         i-32       R       0.70       AC.       RC-DEO       0.44       5.00       D-4.03         i-32       R       0.70       AC.       RC-DEO       0.47       5.00       D-4.03         i-22       S       0.28       AC.       RC-DEO       0.47       5.00       D-4.03         i-24       V       0.80		STRUCTURE NO. 1-1 1-2 1-3 1-7 & 1-8 1-5	AREA A B C D E	AREA         ZONED           1.35         AC.         RC-DEO           0.67         AC.         RC-DEO           0.30         AC.         RC-DEO           0.84         AC.         RC-DEO           0.47         AC.         RC-DEO	'C' FACTOR 0.46 0.49 0.41 0.45 0.25	TIME. (Min.) 5.00 5.00 5.00 5.00 5.00	0-4.03 0-4.03 0-4.03 0-4.22 & MD-374.68 0-4.10 0-4.10			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	I-16       K       1.34 AC. RC-0E0       0.48       5.00       D-4.03         I-17       L       1.43 AC. RC-0E0       0.47       5.00       D-4.03         I-17       L       1.43 AC. RC-0E0       0.47       5.00       D-4.03         I-18       M       0.28 AC. RC-0E0       0.39       5.00       D-4.03         I-4       N       1.59 AC. RC-0E0       0.45       5.00       D-4.22         I-20       P       0.30 AC. RC-0E0       0.25       5.00       D-4.22         I-20       P       0.30 AC. RC-0E0       0.44       5.00       D-4.22         I-31       Q       1.00 AC. RC-0E0       0.44       5.00       D-4.22         I-32       R       0.70 AC. RC-0E0       0.44       5.00       D-4.03         I-32       R       0.70 AC. RC-0E0       0.44       5.00       D-4.03         I-22       S       0.28 AC. RC-0E0       0.41       5.00       D-4.03         I-21       T       0.24 AC. RC-0E0       0.47       5.00       D-4.03         I-27       U       0.70 AC. RC-0E0       0.47       5.00       D-4.03         I-28       V       0.80 AC. RC-0E0       0.47		STRUCTURE NO. 1-1 1-2 1-3 1-7 & 1-8 1-5 1-6 1-9 & 1-10	AREA A B C D E F G	AREA         ZONED           1.35         AC.         RC-DEO           0.67         AC.         RC-DEO           0.30         AC.         RC-DEO           0.84         AC.         RC-DEO           0.47         AC.         RC-DEO           3.13         AC.         RC-DEO           0.59         AC.         RC-DEO	'C' FACTOR 0.46 0.49 0.41 0.45 0.25 0.25 0.25 0.42	TIME. (Min.) 5.00 5.00 5.00 5.00 5.00 5.00 5.00	D-4.03           D-4.03           D-4.03           D-4.03           D-4.22 & MD-374.68           D-4.10           D-4.22 & MD-374.68           D-4.22 & MD-374.68           D-4.22 & MD-374.68			
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	I-18       M       0.28 AC.       RC-DEO       0.39       5.00       D-4.03         I-4       N       1.59 AC.       RC-DEO       0.45       5.00       D-4.10         I-19       O       0.18 AC.       RC-DEO       0.25       5.00       D-4.12         I-30       P       0.00 AC.       RC-DEO       0.25       5.00       D-4.22         I-31       Q       1.00 AC.       RC-DEO       0.30       5.00       D-4.03         I-32       R       0.70 AC.       RC-DEO       0.44       5.00       D-4.03         I-22       S       0.28 AC.       RC-DEO       0.44       5.00       D-4.03         I-22       S       0.28 AC.       RC-DEO       0.44       5.00       D-4.03         I-21       T       0.24 AC.       RC-DEO       0.44       5.00       D-4.03         I-21       T       0.24 AC.       RC-DEO       0.41       5.00       D-4.03         I-27       U       0.70 AC.       RC-DEO       0.47       5.00       D-4.03         I-29       W       1.53 AC.       RC-DEO       0.44       5.00       D-4.03         I-29       W       1.53 AC. <td>A PLANT POLE +92778</td> <td>STRUCTURE NO. 1-1 1-2 1-2 1-3 1-7 &amp; 1-8 1-5 1-6 1-9 &amp; 1-10 1-11 &amp; 1-12 1-13 &amp; 1-14</td> <td>AREA A B C D E F G H I</td> <td>AREA         ZONED           1.35         AC.         RC-DEO           0.67         AC.         RC-DEO           0.30         AC.         RC-DEO           0.84         AC.         RC-DEO           0.47         AC.         RC-DEO           3.13         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.26         AC.         RC-DEO           0.93         AC.         RC-DEO</td> <td>'C' FACTOR 0.46 0.49 0.41 0.45 0.25 0.25 0.25 0.42 0.52 0.43 0.27</td> <td>TIME. (Min.) 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.</td> <td>D-4.03           D-4.03           D-4.03           D-4.03           D-4.22 &amp; MD-374.68           D-4.10           D-4.22 &amp; MD-374.68           D-4.22 &amp; MD-374.68           D-4.22 &amp; MD-374.68           D-4.22 &amp; MD-374.68</td>	A PLANT POLE +92778	STRUCTURE NO. 1-1 1-2 1-2 1-3 1-7 & 1-8 1-5 1-6 1-9 & 1-10 1-11 & 1-12 1-13 & 1-14	AREA A B C D E F G H I	AREA         ZONED           1.35         AC.         RC-DEO           0.67         AC.         RC-DEO           0.30         AC.         RC-DEO           0.84         AC.         RC-DEO           0.47         AC.         RC-DEO           3.13         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.26         AC.         RC-DEO           0.93         AC.         RC-DEO	'C' FACTOR 0.46 0.49 0.41 0.45 0.25 0.25 0.25 0.42 0.52 0.43 0.27	TIME. (Min.) 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.	D-4.03           D-4.03           D-4.03           D-4.03           D-4.22 & MD-374.68           D-4.10           D-4.22 & MD-374.68           D-4.22 & MD-374.68           D-4.22 & MD-374.68           D-4.22 & MD-374.68			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	I-19       0       0.18 AC       RC-DE0       0.25       5.00       D-4.22         I-20       P       0.30 AC       RC-DE0       0.30       5.00       D-4.22         I-31       Q       1.00 AC       RC-DE0       0.44       5.00       D-4.03         I-32       R       0.70 AC       RC-DE0       0.50       5.00       D-4.22       MD-374.68         I-22       S       0.28 AC       RC-DE0       0.44       5.00       D-4.22       & MD-374.68         I-21       T       0.24 AC       RC-DE0       0.41       5.00       D-4.22       & MD-374.68         I-27       U       0.70 AC       RC-DE0       0.41       5.00       D-4.22       & MD-374.68         I-27       U       0.70 AC       RC-DE0       0.47       5.00       D-4.03         I-28       V       0.80 AC       RC-DE0       0.47       5.00       D-4.03         I-29       W       1.53 AC       RC-DE0       0.47       5.00       D-4.03         I-29       V       1.29 AC       RC-DE0       0.64       5.00       CULVERT         I-30       Y       1.29 AC       RC-DE0       0.64       5.00	A PLANT POLE +92778	STRUCTURE NO. 1-1 1-2 1-2 1-3 1-7 & 1-8 1-5 1-6 1-9 & 1-10 1-11 & 1-12 1-13 & 1-14 1-15 1-16	AREA A B C D E F G H I J K	AREA         ZONED           1.35         AC.         RC-DEO           0.67         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.47         AC.         RC-DEO           3.13         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.26         AC.         RC-DEO           0.93         AC.         RC-DEO           1.34         AC.         RC-DEO	'C' FACTOR 0.46 0.49 0.41 0.45 0.25 0.25 0.25 0.42 0.52 0.43 0.27 0.48	TIME. (Min.) 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.	D-4.03           D-4.03           D-4.03           D-4.03           D-4.22 & MD-374.68           D-4.10           D-4.10           D-4.22 & MD-374.68           D-4.23 & MD-374.68			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	I-31       Q       1.00 AC.       RC-DED       0.44       5.00       D-4.03         I-32       R       0.70 AC.       RC-DED       0.50       5.00       D-4.03         I-22       S       0.28 AC.       RC-DED       0.44       5.00       D-4.22 & MD-374.68         I-21       T       0.24 AC.       RC-DED       0.41       5.00       D-4.22 & MD-374.68         I-21       T       0.24 AC.       RC-DED       0.41       5.00       D-4.22 & MD-374.68         I-27       U       0.70 AC.       RC-DED       0.47       5.00       D-4.03         I-28       V       0.80 AC.       RC-DED       0.47       5.00       D-4.03         I-29       W       1.53 AC.       RC-DED       0.47       5.00       D-4.03         I-29       W       1.53 AC.       RC-DED       0.64       5.00       D-4.03         I-29       W       1.53 AC.       RC-DED       0.64       5.00       D-4.03         I-29       W       1.53 AC.       RC-DED       0.64       5.00       D-4.03         I-29       W       1.29 AC.       RC-DED       0.64       5.00       D-4.14         I-50	AND THE ADDRESS OF TH	STRUCTURE NO. 1-1 1-2 1-2 1-3 1-7 & 1-8 1-5 1-6 1-9 & 1-10 1-11 & 1-12 1-13 & 1-14 1-15 1-16 1-17 1-18	AREA A B C D E F G H I J K L M	AREA         ZONED           1.35         AC.         RC-DEO           0.67         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.47         AC.         RC-DEO           3.13         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.26         AC.         RC-DEO           1.34         AC.         RC-DEO           1.43         AC.         RC-DEO           0.28         AC.         RC-DEO	'C' FACTOR 0.46 0.49 0.41 0.45 0.25 0.25 0.25 0.42 0.52 0.43 0.27 0.48 0.27 0.48 0.47 0.39	TIME (Min.) 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			
I-22         5         0.28 AC.         RC-DEO         0.44         5.00         D-4.22 & MD-374.68           I-21         T         0.24 AC.         RC-DEO         0.41         5.00         D-4.22 & MD-374.68	$\frac{1-22}{5} = 5 = 0.28 \text{ AC}, \text{ RC-DEO} = 0.44 = 5.00 = 0.422 \text{ & MD-374.68} \\ 1-21 = T = 0.24 \text{ AC}, \text{ RC-DEO} = 0.41 = 5.00 = 0.4.22 \text{ & MD-374.68} \\ 1-21 = T = 0.24 \text{ AC}, \text{ RC-DEO} = 0.41 = 5.00 = 0.4.22 \text{ & MD-374.68} \\ 1-27 = U = 0.70 \text{ AC}, \text{ RC-DEO} = 0.47 = 5.00 = 0.4.03 \\ 1-28 = V = 0.80 \text{ AC}, \text{ RC-DEO} = 0.47 = 5.00 = 0.4.03 \\ 1-29 = W = 1.53 \text{ AC}, \text{ RC-DEO} = 0.47 = 5.00 = 0.4.03 \\ 1-29 = W = 1.53 \text{ AC}, \text{ RC-DEO} = 0.64 = 5.00 = 0.4.03 \\ 1-30 = Y = 1.29 \text{ AC}, \text{ RC-DEO} = 0.64 = 5.00 = 0.4.03 \\ 1-58 = Z = 0.52 \text{ AC}, \text{ RC-DEO} = 0.64 = 5.00 = 0.4.14 \\ 1-58 = A = 0.97 \text{ AC}, \text{ RC-DEO} = 0.94 = 5.00 = 0.4.14 \\ 1-23 \text{ & } 1-24 = CC = 0.54 \text{ AC}, \text{ RC-DEO} = 0.64 = 5.00 = 0.4.14 \\ 1-23 \text{ & } 1-24 = CC = 0.54 \text{ AC}, \text{ RC-DEO} = 0.64 = 5.00 = 0.4.22 \text{ & MD-374.68} \\ 1-25 \text{ & } 1-26 = DD = 0.51 \text{ AC}, \text{ RC-DEO} = 0.64 = 5.00 = 0.4.22 \text{ & MD-374.68} \\ 1-25 \text{ & } 1-26 = DD = 0.51 \text{ AC}, \text{ RC-DEO} = 0.64 = 5.00 = 0.4.22 \text{ & MD-374.68} \\ 1-25 \text{ & } 1-26 = DD = 0.51 \text{ AC}, \text{ RC-DEO} = 0.64 = 5.00 = 0.4.22 \text{ & MD-374.68} \\ 1-25 \text{ & } 1-26 = DD = 0.51 \text{ AC}, \text{ RC-DEO} = 0.64 = 5.00 = 0.4.22 \text{ & MD-374.68} \\ 1-25 \text{ & } 1-26 = DD = 0.51 \text{ AC}, \text{ RC-DEO} = 0.64 = 5.00 = 0.4.22 \text{ & MD-374.68} \\ 1-25 \text{ & } 1-26 = DD = 0.51 \text{ AC}, \text{ RC-DEO} = 0.64 = 5.00 = 0.4.22 \text{ & MD-374.68} \\ 1-25 \text{ & } 1-26 = DD = 0.51 \text{ AC}, \text{ RC-DEO} = 0.64 = 5.00 = 0.4.22 \text{ & MD-374.68} \\ 1-25 \text{ & } 1-26 = DD = 0.51 \text{ AC}, \text{ RC-DEO} = 0.64 = 5.00 = 0.4.22 \text{ & MD-374.68} \\ 1-25 \text{ & } 1-26 = DD = 0.51 \text{ AC}, \text{ RC-DEO} = 0.64 = 5.00 = 0.4.22 \text{ & MD-374.68} \\ 1-25 \text{ & } 1-26 = 0.99 \text{ & } 0.64 = 5.00 = 0.4.4 = 5.00 = 0.4.22 \text{ & } 0.4.22 \text{ & } 0.4.22 \text{ & } 0.4.22 \text{ & } 0.4.23 \text{ & } 0.4.$	AND THE ADDRESS OF TH	STRUCTURE NO. 1-1 1-2 1-3 1-7 & 1-8 1-5 1-6 1-9 & 1-10 1-11 & 1-12 1-13 & 1-14 1-15 1-16 1-17 1-18 1-4 1-19	AREA A B C D E F G H I J K L M N O	AREA         ZONED           1.35         AC.         RC-DEO           0.67         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.47         AC.         RC-DEO           0.47         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.47         AC.         RC-DEO           0.59         AC.         RC-DEO           0.47         AC.         RC-DEO           0.47         AC.         RC-DEO           0.47         AC.         RC-DEO           0.47         AC.         RC-DEO           0.48         AC.         RC-DEO           1.43         AC.         RC-DEO           1.43         AC.         RC-DEO           1.59         AC.         RC-DEO           0.18         AC.         RC-DEO	'C' FACTOR 0.46 0.49 0.41 0.45 0.25 0.25 0.42 0.52 0.42 0.52 0.43 0.27 0.48 0.47 0.39 0.45 0.25	TIME. (Min.) 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			
	I-27       U       0.70 AC.       RC-DE0       0.47       5.00       D-4.03         I-28       V       0.80 AC.       RC-DE0       0.47       5.00       D-4.03         I-29       W       1.53 AC.       RC-DE0       0.49       5.00       D-4.03         S-11       X       9.92 AC.       RC-DE0       0.64       5.00       CULVERT         I-30       Y       1.29 AC.       RC-DE0       0.64       5.00       D-4.03         1-58       Z       0.52 AC.       RC-DE0       0.64       5.00       D-4.03         1-58       Z       0.52 AC.       RC-DE0       0.64       5.00       D-4.14         1-58       A       0.97 AC.       RC-DE0       0.95       5.00       D-4.14         1-23 & 1-24       CC       0.54 AC.       RC-DE0       0.64       5.00       D-4.22 & MD-374.68         1-25 & 1-26       DD       0.51 AC.       RC-DE0       0.64       5.00       D-4.22 & MD-374.68         1-25 & 1-26       DD       0.51 AC.       RC-DE0       0.64       5.00       D-4.22 & MD-374.68         E5D #13       B8       2.34 AC.       RC-DE0       0.91       5.00       BIO-RETENTION	A CALL AND THE	STRUCTURE NO. 1-1 1-2 1-3 1-7 & 1-8 1-5 1-6 1-9 & 1-10 1-11 & 1-12 1-13 & 1-14 1-15 1-16 1-17 1-18 1-4 1-19 1-20 1-31	AREA A B C D E F G H I J K L M N O P Q	AREA         ZONED           1.35         AC.         RC-DEO           0.67         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.47         AC.         RC-DEO           0.47         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.47         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.46         AC.         RC-DEO           0.47         AC.         RC-DEO           0.48         AC.         RC-DEO           1.34         AC.         RC-DEO           1.43         AC.         RC-DEO           1.59         AC.         RC-DEO           0.18         AC.         RC-DEO           0.30         AC.         RC-DEO           1.00         AC.         RC-DEO	'C' FACTOR 0.46 0.49 0.41 0.45 0.25 0.25 0.42 0.52 0.42 0.52 0.43 0.27 0.48 0.47 0.39 0.45 0.25 0.25 0.30 0.44	TIME (Min.) 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			
	I-28       V       0.80 AC.       RC-DE0       0.47       5.00       D-4.03         I-29       W       1.53 AC.       RC-DE0       0.49       5.00       D-4.03         S-11       X       9.92 AC.       RC-DE0       0.64       5.00       CULVERT         I-30       Y       1.29 AC.       RC-DE0       0.64       5.00       D-4.03         1-58       Z       0.52 AC.       RC-DE0       0.64       5.00       D-4.13         1-58       Z       0.52 AC.       RC-DE0       0.94       5.00       D-4.14         1-58       AA       0.97 AC.       RC-DE0       0.95       5.00       D-4.14         1-58       AA       0.97 AC.       RC-DE0       0.95       5.00       D-4.14         1-23 & 1-24       CC       0.54 AC.       RC-DE0       0.64       5.00       D-4.22 & MD-374.68         1-25 & 1-26       DD       0.51 AC.       RC-DE0       0.64       5.00       D-4.22 & MD-374.68         1-25 & 1-26       DD       0.51 AC.       RC-DE0       0.89       5.00       BIO-RETENTION         E5D #13       BB       2.34 AC.       RC-DE0       0.91       5.00       BIO-RETENTION <td>A CALL STREE</td> <td>STRUCTURE NO. I-1 I-2 I-3 I-7 &amp; I-8 I-5 I-6 I-9 &amp; I-10 I-11 &amp; I-12 I-13 &amp; I-14 I-15 I-16 I-17 I-18 I-4 I-19 I-20 I-31 I-32</td> <td>AREA A B C D E F G H I J K L N N O P Q R</td> <td>AREA         ZONED           1.35         AC.         RC-DEO           0.67         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.47         AC.         RC-DEO           3.13         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.26         AC.         RC-DEO           0.93         AC.         RC-DEO           1.34         AC.         RC-DEO           1.43         AC.         RC-DEO           1.59         AC.         RC-DEO           0.16         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.70         AC.         RC-DEO</td> <td>'C' FACTOR 0.46 0.49 0.41 0.45 0.25 0.25 0.42 0.52 0.42 0.52 0.43 0.27 0.48 0.47 0.39 0.45 0.25 0.25 0.30 0.44 0.50</td> <td>TIME. (Min.) 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.</td> <td>$\begin{array}{c ccccccccccccccccccccccccccccccccccc$</td>	A CALL STREE	STRUCTURE NO. I-1 I-2 I-3 I-7 & I-8 I-5 I-6 I-9 & I-10 I-11 & I-12 I-13 & I-14 I-15 I-16 I-17 I-18 I-4 I-19 I-20 I-31 I-32	AREA A B C D E F G H I J K L N N O P Q R	AREA         ZONED           1.35         AC.         RC-DEO           0.67         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.47         AC.         RC-DEO           3.13         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.26         AC.         RC-DEO           0.93         AC.         RC-DEO           1.34         AC.         RC-DEO           1.43         AC.         RC-DEO           1.59         AC.         RC-DEO           0.16         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.70         AC.         RC-DEO	'C' FACTOR 0.46 0.49 0.41 0.45 0.25 0.25 0.42 0.52 0.42 0.52 0.43 0.27 0.48 0.47 0.39 0.45 0.25 0.25 0.30 0.44 0.50	TIME. (Min.) 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			
1-28 V 0.80 AC. RC-DEO 0.47 5.00 D-4.03	5-11       X       9.92 AC.       RC-DEO       0.64       5.00       CULVERT         1-30       Y       1.29 AC.       RC-DEO       0.64       5.00       D-4.03         1-58       Z       0.52 AC.       RC-DEO       0.94       5.00       D-4.14         -338       1-58       Z       0.52 AC.       RC-DEO       0.95       5.00       D-4.14         -338       1-58       Z       0.97 AC.       RC-DEO       0.95       5.00       D-4.14         -338       1-23 & 1-24       CC       0.54 AC.       RC-DEO       0.64       5.00       D-4.22 & MD-374.68         1-25 & 1-26       DD       0.51 AC.       RC-DEO       0.64       5.00       D-4.22 & MD-374.68         1-25 & 1-26       DD       0.51 AC.       RC-DEO       0.64       5.00       D-4.22 & MD-374.68         1-25 & 1-26       DD       0.51 AC.       RC-DEO       0.64       5.00       D-4.22 & MD-374.68         ESD #13       B8       2.34 AC.       RC-DEO       0.89       5.00       BIO-RETENTION         ESD #14       EE       0.99 AC.       RC-DEO       0.91       5.00       MICRO BIO-RETENTION	A Contraction of the second of	STRUCTURE         NO.         I-1         I-2         I-3         I-7 & I-8         I-5         I-6         I-9 & I-10         I-11 & I-12         I-13 & I-14         I-15         I-6         I-9 & I-10         I-18         I-17         I-18         I-19         I-20         I-31         I-32         I-22         I-21	AREA A B C D E F G H H I J K L N N O P Q Q R S T	AREA         ZONED           1.35         AC.         RC-DEO           0.67         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.47         AC.         RC-DEO           0.47         AC.         RC-DEO           0.47         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.26         AC.         RC-DEO           0.47         AC.         RC-DEO           0.26         AC.         RC-DEO           0.45         AC.         RC-DEO           1.34         AC.         RC-DEO           1.43         AC.         RC-DEO           0.16         AC.         RC-DEO           0.170         AC.         RC-DEO           0.30         AC.         RC-DEO           0.70         AC.         RC-DEO           0.28         AC.         RC-DEO           0.24         AC.         RC-DEO  <	'C' FACTOR 0.46 0.49 0.41 0.45 0.25 0.25 0.42 0.52 0.42 0.52 0.43 0.27 0.48 0.47 0.39 0.45 0.25 0.30 0.45 0.25 0.30 0.44 0.50 0.44 0.41	TIME. (Min.) 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			
5-11 X 992 AC RC-DEO 0.64 5.00 CUIVERT	1-50       1       1.2.9 AC.       RC-0L0       0.04       5.00       0-4.03         1-50       1-53       Z       0.52 AC.       RC-0E0       0.94       5.00       0-4.14         530       542       1-55       AA       0.97 AC.       RC-0E0       0.95       5.00       0-4.14         1-23 & 1-24       CC       0.54 AC.       RC-0E0       0.64       5.00       0-4.22 & MD-374.68         1-25 & 1-26       0D       0.51 AC.       RC-0E0       0.64       5.00       D-4.22 & MD-374.68         1-25 & 1-26       0D       0.51 AC.       RC-0E0       0.64       5.00       D-4.22 & MD-374.68         E50 #13       B8       2.34 AC.       RC-0E0       0.69       5.00       BIO-RETENTION         E50 #14       EE       0.99 AC.       RC-0E0       0.91       5.00       MICRO BIO-RETENTION	AND THE OPENING OF THE STREET	STRUCTURE         NO.         I-1         I-2         I-3         I-7 & I-8         I-5         I-6         I-9 & I-10         I-11 & I-12         I-3 & I-14         I-15         I-16         I-17         I-18         I-19         I-20         I-31         I-32         I-22         I-21         I-27         I-28	AREA       A       B       C       D       E       F       G       H       I       J       K       L       M       N       O       P       Q       R       S       T       U       V	AREA         ZONED           1.35         AC.         RC-DEO           0.67         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.47         AC.         RC-DEO           0.47         AC.         RC-DEO           0.47         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.26         AC.         RC-DEO           0.47         AC.         RC-DEO           0.47         AC.         RC-DEO           0.47         AC.         RC-DEO           0.47         AC.         RC-DEO           0.42         AC.         RC-DEO           0.43         AC.         RC-DEO           0.44         AC.         RC-DEO           0.16         AC.         RC-DEO           0.30         AC.         RC-DEO           0.40         AC.         RC-DEO           0.70         AC.         RC-DEO	'C' FACTOR 0.46 0.49 0.41 0.45 0.25 0.25 0.42 0.52 0.42 0.52 0.43 0.27 0.48 0.47 0.39 0.45 0.25 0.30 0.44 0.50 0.44 0.50 0.44 0.41 0.47 0.47	TIME. (Min.) 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			
1-00 1 1.27 AC. KO-010 0.07 0.00 0-4.00	1-5b         AA         0.97 AC.         RC-DEO         0.95         5.00         D-4.14           540         542         1-23 & 1-24         CC         0.54 AC.         RC-DEO         0.64         5.00         D-4.22 & MD-374.68           MAC         542         00         0.51 AC.         RC-DEO         0.64         5.00         D-4.22 & MD-374.68           MAC         544         0.97         AC.         RC-DEO         0.64         5.00         D-4.22 & MD-374.68           MAC         544         0.97         AC.         RC-DEO         0.64         5.00         D-4.22 & MD-374.68           MAC         544         0.97         AC.         RC-DEO         0.64         5.00         D-4.22 & MD-374.68           E50 #13         B8         2.34 AC.         RC-DEO         0.89         5.00         BIO-RETENTION           E50 #14         EE         0.99 AC.         RC-DEO         0.91         5.00         MICRO BIO-RETENTION	AND THE AREA OF THE AND THE AREA OF THE AR	STRUCTURE       NO.         I-1       I-2         I-3       I-7         I-7       I-8         I-5       I-6         I-9       I-10         I-11       I-12         I-3       I-7         I-6       I-9         I-10       I-10         I-11       I-12         I-13       I-14         I-15       I-16         I-17       I-18         I-19       I-20         I-31       I-32         I-22       I-21         I-22       I-21         I-27       I-28         I-29       S-11	AREA         A         B         C         D         E         F         G         H         I         J         K         L         M         N         O         P         Q         R         S         T         U         V         W	AREA         ZONED           1.35         AC.         RC-DEO           0.67         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.34         AC.         RC-DEO           0.47         AC.         RC-DEO           0.47         AC.         RC-DEO           0.47         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.47         AC.         RC-DEO           0.59         AC.         RC-DEO           0.47         AC.         RC-DEO           0.46         AC.         RC-DEO           1.34         AC.         RC-DEO           1.43         AC.         RC-DEO           0.18         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.70         AC.         RC-DEO           0.70         AC.         RC-DEO	'C' FACTOR 0.46 0.49 0.41 0.45 0.25 0.25 0.42 0.52 0.42 0.52 0.43 0.27 0.48 0.47 0.39 0.45 0.25 0.30 0.44 0.50 0.44 0.50 0.44 0.41 0.47 0.47 0.47 0.49 0.64	TIME (Min.) 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			
1-5b AA 0.97 AC. RC-DEO 0.95 5.00 D-4.14	I-25 & I-26       OD       0.51 AC.       RC-DEO       0.64       5.00       D-4.22 & MD-374.68         E5D #13       BB       2.34 AC.       RC-DEO       0.89       5.00       BIO-RETENTION         E5D #14       EE       0.99 AC.       RC-DEO       0.91       5.00       MICRO BIO-RETENTION	A CMP	STRUCTURE         NO.         I-1         I-2         I-3         I-7 & I-8         I-5         I-6         I-9 & I-10         I-11 & I-12         I-13 & I-14         I-15         I-16         I-17         I-18         I-19         I-20         I-31         I-22         I-21         I-22         I-21         I-22         I-21         I-22         I-22         I-20         I-31         I-32         I-20         I-31         I-32         I-29         S-11         I-30	AREA         A         B         C         D         E         F         G         H         I         J         K         L         M         N         O         P         Q         R         S         T         U         V         W         X         Y	AREA         ZONED           1.35         AC.         RC-DEO           0.67         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.34         AC.         RC-DEO           0.47         AC.         RC-DEO           0.47         AC.         RC-DEO           0.47         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.26         AC.         RC-DEO           0.30         AC.         RC-DEO           1.34         AC.         RC-DEO           0.28         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.28         AC.         RC-DEO           0.28         AC.         RC-DEO           0.29         AC.         RC-DEO	'C' FACTOR 0.46 0.49 0.41 0.45 0.25 0.25 0.42 0.52 0.42 0.52 0.43 0.27 0.48 0.47 0.39 0.45 0.25 0.30 0.45 0.25 0.30 0.44 0.50 0.44 0.50 0.44 0.41 0.47 0.47 0.47 0.49 0.64 0.64	TIME (Min.) 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			
	E5D #14 EE 0.99 AC. RC-DEO 0.91 5.00 MICRO BIO-RETENTION	A CMP	STRUCTURE         NO.         I-1         I-2         I-3         I-7 & I-8         I-5         I-6         I-9 & I-10         I-11 & I-12         I-13 & I-14         I-15         I-16         I-17         I-18         I-19         I-20         I-31         I-22         I-21         I-22         I-21         I-22         I-21         I-32         I-22         I-21         I-32         I-23         I-24         I-50         I-50	AREA         A         B         C         D         E         F         G         H         I         J         K         L         M         N         O         P         Q         R         S         T         U         V         W         X         Y         Z         AA	AREA         ZONED           1.35         AC.         RC-DEO           0.67         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.47         AC.         RC-DEO           0.47         AC.         RC-DEO           0.47         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.26         AC.         RC-DEO           0.93         AC.         RC-DEO           0.93         AC.         RC-DEO           0.28         AC.         RC-DEO           0.19         AC.         RC-DEO           0.19         AC.         RC-DEO           0.10         AC.         RC-DEO           0.10         AC.         RC-DEO           0.10         AC.         RC-DEO           0.20         AC.         RC-DEO           0.20         AC.         RC-DEO           0.20         AC.         RC-DEO           0.20         AC.         RC-DEO	'C' FACTOR 0.46 0.49 0.41 0.45 0.25 0.25 0.42 0.52 0.42 0.52 0.43 0.27 0.48 0.47 0.39 0.45 0.25 0.30 0.45 0.25 0.30 0.44 0.50 0.44 0.50 0.44 0.50 0.44 0.41 0.47 0.47 0.47 0.49 0.64 0.94 0.95	TIME (Min.) 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			
E5D #13 BB 2.34 AC. RC-DEO 0.89 5.00 BIO-RETENTION	E5D #14 EE 0.99 AC. RC-DEO 0.91 5.00 MICRO BIO-RETENTION	A CMP	STRUCTURE NO.         I-1         I-2         I-3         I-7 & I-8         I-5         I-6         I-9 & I-10         I-11 & I-12         I-3 & I-14         I-15         I-16         I-17         I-18         I-19         I-20         I-31         I-22         I-21         I-27         I-28         I-29         S-11         I-30         I-58         I-23 & I-24	AREA         A         B         C         D         E         F         G         H         I         J         K         L         M         N         O         P         Q         R         S         T         U         V         W         X         Y         Z         AA         CC	AREA         ZONED           1.35         AC.         RC-DEO           0.67         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.84         AC.         RC-DEO           0.84         AC.         RC-DEO           0.47         AC.         RC-DEO           0.13         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.26         AC.         RC-DEO           0.30         AC.         RC-DEO           0.28         AC.         RC-DEO           0.18         AC.         RC-DEO           0.10         AC.         RC-DEO           0.10         AC.         RC-DEO           0.10         AC.         RC-DEO           0.10         AC.         RC-DEO           0.28         AC.         RC-DEO           0.29         AC.         RC-DEO           0.20         AC.         RC-DEO	'C' FACTOR 0.46 0.49 0.41 0.45 0.25 0.25 0.42 0.52 0.42 0.52 0.43 0.27 0.48 0.47 0.39 0.45 0.25 0.30 0.45 0.25 0.30 0.44 0.50 0.44 0.50 0.44 0.50 0.44 0.47 0.47 0.47 0.47 0.47 0.47 0.4	TIME (Min.) 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			
		The serve of the s	STRUCTURE         NO.         I-1         I-2         I-3         I-7 & I-8         I-5         I-6         I-9 & I-10         I-11 & I-12         I-3 & I-14         I-15         I-6         I-9 & I-10         I-11 & I-12         I-13 & I-14         I-15         I-16         I-17         I-18         I-4         I-19         I-20         I-31         I-20         I-20         I-21         I-20         I-21         I-22         I-21         I-27         I-28         I-29         S-11         I-30         I-50         I-23 & I-24         I-25 & I-26	AREA         A         B         C         D         E         F         G         H         I         J         K         L         M         N         O         P         Q         R         S         T         U         V         W         X         Y         Z         AA         CC         DD	AREA         ZONED           1.35         AC.         RC-DEO           0.67         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.34         AC.         RC-DEO           0.47         AC.         RC-DEO           0.47         AC.         RC-DEO           0.59         AC.         RC-DEO           0.26         AC.         RC-DEO           0.30         AC.         RC-DEO           0.28         AC.         RC-DEO           0.18         AC.         RC-DEO           0.30         AC.         RC-DEO           0.10         AC.         RC-DEO           0.10         AC.         RC-DEO           0.28         AC.         RC-DEO           0.29         AC.         RC-DEO           0.20         AC.         RC-DEO           0.20         AC.         RC-DEO	'C' FACTOR 0.46 0.49 0.41 0.45 0.25 0.25 0.42 0.52 0.42 0.52 0.43 0.27 0.48 0.47 0.39 0.45 0.25 0.30 0.45 0.25 0.30 0.44 0.50 0.44 0.50 0.44 0.50 0.44 0.50 0.44 0.50 0.44 0.47 0.47 0.47 0.47 0.47 0.47 0.4	TIME (Min.) 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			
LINIDENI CONVE	a la targa prese a nameno esta la ser en la la seconda	The serve of the s	STRUCTURE         NO.         I-1         I-2         I-3         I-7 & I-8         I-5         I-6         I-9 & I-10         I-11 & I-12         I-13 & I-14         I-15         I-16         I-17         I-18         I-4         I-19         I-20         I-31         I-22         I-21         I-22         I-21         I-32         I-22         I-21         I-32         I-22         I-23         I-29         S-11         I-29         S-11         I-23 & I-24         I-25 & I-26         ESD #13	AREA         A         B         C         D         E         F         G         H         I         J         K         L         M         N         O         P         Q         R         S         T         U         V         W         X         Y         Z         AA         CC         DD         BB         EE	AREA         ZONED           1.35         AC.         RC-DEO           0.67         AC.         RC-DEO           0.30         AC.         RC-DEO           0.30         AC.         RC-DEO           0.34         AC.         RC-DEO           0.47         AC.         RC-DEO           0.47         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.59         AC.         RC-DEO           0.26         AC.         RC-DEO           0.34         AC.         RC-DEO           0.43         AC.         RC-DEO           0.45         AC.         RC-DEO           0.46         AC.         RC-DEO           0.47         AC.         RC-DEO           0.48         AC.         RC-DEO           0.40         AC.         RC-DEO           0.18         AC.         RC-DEO           0.10         AC.         RC-DEO           0.70         AC.         RC-DEO           0.70         AC.         RC-DEO           0.80         AC.         RC-DEO	'C' FACTOR 0.46 0.49 0.41 0.45 0.25 0.25 0.42 0.52 0.42 0.52 0.43 0.27 0.48 0.47 0.47 0.39 0.45 0.25 0.30 0.45 0.25 0.30 0.44 0.50 0.44 0.50 0.44 0.50 0.44 0.50 0.44 0.50 0.44 0.50 0.44 0.50 0.44 0.50 0.44 0.50 0.44 0.50 0.44 0.50 0.44 0.50 0.44 0.50 0.44 0.50 0.45 0.50 0.45 0.50 0.45 0.50 0.44 0.50 0.44 0.50 0.44 0.50 0.45 0.50 0.44 0.50 0.45 0.50 0.44 0.50 0.45 0.50 0.44 0.50 0.45 0.50 0.44 0.50 0.45 0.50 0.44 0.50 0.45 0.50 0.44 0.50 0.45 0.50 0.44 0.50 0.44 0.50 0.45 0.47 0.49 0.45 0.50 0.44 0.50 0.45 0.50 0.44 0.50 0.45 0.47 0.49 0.45 0.50 0.44 0.50 0.45 0.50 0.45 0.50 0.44 0.50 0.45 0.50 0.45 0.50 0.45 0.50 0.45 0.50 0.45 0.50 0.47 0.49 0.64 0.94 0.94 0.94 0.50 0.64 0.94 0.95 0.55 0.55 0.50 0.47 0.49 0.64 0.94 0.95 0.64 0.94 0.95 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55 0.55	TIME (Min.) 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.	0-4.03         0-4.03         0-4.03         0-4.03         0-4.22 & MD-374.68         0-4.10         0-4.22 & MD-374.68         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.22 & MD-374.68         0-4.03         0-4.03         0-4.03         0-4.22 & MD-374.68         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.14         0-4.22 & MD-374.68         BIO-RETENTION         MICRO BIO-RETENTION         MICRO BIO-RETENTION			
LINDEN GROVE		The serve of the s	STRUCTURE         NO.         I-1         I-2         I-3         I-7 & I-8         I-5         I-6         I-9 & I-10         I-11 & I-12         I-13 & I-14         I-15         I-16         I-17         I-18         I-4         I-19         I-20         I-31         I-22         I-21         I-22         I-21         I-32         I-22         I-21         I-32         I-22         I-23         I-29         S-11         I-29         S-11         I-23 & I-24         I-25 & I-26         ESD #13	AREA         A         B         C         D         E         F         G         H         I         J         K         L         M         N         O         P         Q         R         S         T         U         V         W         X         Y         Z         AA         CC         DD         BB         EE	AREA       ZONED         1.35       AC.       RC-DEO         0.67       AC.       RC-DEO         0.30       AC.       RC-DEO         0.30       AC.       RC-DEO         0.84       AC.       RC-DEO         0.47       AC.       RC-DEO         0.47       AC.       RC-DEO         0.59       AC.       RC-DEO         0.59       AC.       RC-DEO         0.59       AC.       RC-DEO         0.26       AC.       RC-DEO         0.34       AC.       RC-DEO         0.47       AC.       RC-DEO         0.59       AC.       RC-DEO         0.59       AC.       RC-DEO         0.47       AC.       RC-DEO         0.48       AC.       RC-DEO         0.40       AC.       RC-DEO         0.40       AC.       RC-DEO         0.10       AC.       RC-DEO         0.28       AC.       RC-DEO         0.70       AC.       RC-DEO         0.29       AC.       RC-DEO         0.20       AC.       RC-DEO         0.80       AC.	'C'         FACTOR         0.46         0.49         0.41         0.45         0.25         0.25         0.42         0.52         0.43         0.27         0.48         0.47         0.39         0.45         0.25         0.44         0.47         0.39         0.44         0.47         0.48         0.47         0.45         0.25         0.30         0.44         0.50         0.44         0.50         0.44         0.50         0.44         0.47         0.47         0.47         0.44         0.47         0.47         0.47         0.47         0.47         0.47         0.47         0.47         0.47         0.47         0.47         0.47         0.47         0.47      <	TIME (Min.) 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.	0-4.03 0-4.03 0-4.03 0-4.03 0-4.22 & MD-374.68 0-4.22 & MD-374.68 0-4.22 & MD-374.68 0-4.22 & MD-374.68 0-4.22 & MD-374.68 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.22 0-4.22 0-4.22 0-4.22 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-4.03 0-			
LOTS 1 THRU 44, BUILDABLE PRESERVATION PARCEL 'A' & NON-BUILDABLE PRESERVATION	LOTS 1 THRU 44, BUILDABLE PRESERVATION PARCEL 'A' & NON-BUILDABLE PRESERVATION	The serve of the s	STRUCTURE         NO.         I-1         I-2         I-3         I-7 & I-8         I-5         I-6         I-9 & I-10         I-11 & I-12         I-13 & I-14         I-15         I-16         I-17         I-18         I-4         I-19         I-20         I-31         I-22         I-21         I-22         I-21         I-32         I-22         I-21         I-32         I-22         I-23         I-29         S-11         I-29         S-11         I-23 & I-24         I-25 & I-26         ESD #13	AREA         A         B         C         D         E         F         G         H         I         J         K         L         M         N         O         P         Q         R         S         T         U         V         W         X         Y         Z         AA         CC         DD         BB         EE         577         LOT5	AREA       ZONED         1.35       AC.       RC-DEO         0.67       AC.       RC-DEO         0.30       AC.       RC-DEO         0.30       AC.       RC-DEO         0.47       AC.       RC-DEO         0.47       AC.       RC-DEO         0.47       AC.       RC-DEO         0.59       AC.       RC-DEO         0.59       AC.       RC-DEO         0.59       AC.       RC-DEO         0.26       AC.       RC-DEO         0.34       AC.       RC-DEO         0.359       AC.       RC-DEO         0.47       AC.       RC-DEO         0.30       AC.       RC-DEO         1.43       AC.       RC-DEO         0.28       AC.       RC-DEO         0.19       AC.       RC-DEO         0.30       AC.       RC-DEO         0.10       AC.       RC-DEO         0.28       AC.       RC-DEO         0.29       AC.       RC-DEO         0.20       AC.       RC-DEO         0.20       AC.       RC-DEO         0.24       AC.	<pre>'C' FACTOR 0.46 0.49 0.41 0.45 0.25 0.25 0.42 0.52 0.42 0.52 0.43 0.27 0.48 0.47 0.47 0.49 0.45 0.25 0.30 0.45 0.25 0.30 0.44 0.50 0.44 0.50 0.44 0.50 0.44 0.50 0.44 0.50 0.44 0.47 0.47 0.47 0.47 0.47 0.47 0.4</pre>	TIME (Min.) 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.	0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.10         0-4.10         0-4.10         0-4.10         0-4.22 & MD-374.68         0-4.22 & MD-374.68         0-4.22 & MD-374.68         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.22         0-4.03         0-4.22         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.14         0-4.22 & MD-374.68         BIO-RETENTION         MICRO BIO-RETENTION         MICRO BIO-RETENTION         PESERVATION			
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LOTS 1 THRU 44, BUILDABLE PRESERVATION PARCEL 'A' & NON-BUILDABLE PRESERVATION PARCELS 'B' THRU 'D'	LOTS 1 THRU 44, BUILDABLE PRESERVATION PARCEL 'A' & NON-BUILDABLE PRESERVATION PARCELS 'B' THRU 'D' ZONED: RC-DEO TAX MAP No. 7 GRID No. 18 & TAX MAP No. 8 GRID No. 13 PARCEL No. 5	Liments	STRUCTURE         NO.         I-1         I-2         I-3         I-7 & I-8         I-5         I-6         I-9 & I-10         I-11 & I-12         I-13 & I-14         I-15         I-16         I-17         I-18         I-4         I-19         I-20         I-31         I-22         I-21         I-22         I-21         I-32         I-22         I-21         I-32         I-22         I-23         I-29         S-11         I-29         S-11         I-23 & I-24         I-25 & I-26         ESD #13	AREA         A         B         C         D         E         F         G         H         I         J         K         L         M         N         O         P         Q         R         S         T         U         V         W         X         Y         Z         AA         CC         DD         BB         EE         577         LOTS         PARCE	AREA       ZONED         1.35       AC.       RC-DEO         0.67       AC.       RC-DEO         0.30       AC.       RC-DEO         0.34       AC.       RC-DEO         0.47       AC.       RC-DEO         0.47       AC.       RC-DEO         0.47       AC.       RC-DEO         0.59       AC.       RC-DEO         0.59       AC.       RC-DEO         0.59       AC.       RC-DEO         0.26       AC.       RC-DEO         0.34       AC.       RC-DEO         0.47       AC.       RC-DEO         0.59       AC.       RC-DEO         0.59       AC.       RC-DEO         0.47       AC.       RC-DEO         0.48       AC.       RC-DEO         0.40       AC.       RC-DEO         0.40       AC.       RC-DEO         0.70       AC.       RC-DEO         0.70       AC.       RC-DEO         0.70       AC.       RC-DEO         0.70       AC.       RC-DEO         0.80       AC.       RC-DEO         0.70       AC.	'C'         FACTOR         0.46         0.49         0.41         0.45         0.25         0.25         0.42         0.52         0.43         0.27         0.48         0.47         0.39         0.45         0.25         0.43         0.27         0.48         0.47         0.39         0.45         0.25         0.30         0.44         0.50         0.44         0.50         0.44         0.50         0.44         0.50         0.44         0.50         0.44         0.47         0.47         0.47         0.47         0.47         0.47         0.47         0.44         0.47         0.47         0.47         0.44         0.91         0.64         0.64         0.91      <	TIME (Min.) 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.	0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.22 & MD-374.68         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.22 & MD-374.68         0-4.22 & MD-374.68         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.03         0-4.14         0-4.22 & MD-374.68         BIO-RETENTION         MICRO BIO-RETENTION         MICRO BIO-RETENTION         PESERVATION			

4TH ELECTION DISTRICT HOWARD COUNTY, MARYLAND DATE: JANUARY 25, 2018 SHEET 12 of 14

 $\square$ Lot 4 Freeman Property Plat No. 4191 PRESERVATION PARCEL 'A' 113.756 Ac.+ 143 GmA /N 606,250 ~~~~~ The state of the s FISHER, COLLINS & CARTER, INC.

ENNIAL SQUARE OFFICE PARK - 10272 BALTIMORE NATIONAL PIKE ELLICOTT CITY, MARYLAND 21042 (410) 461 - 2055



OWNER & DEVELOPER: HERITAGE LAND DEVELOPMENT 15950 NORTH AVENUE LISBON, MARYLAND 21765 410-489-7900

"Professional Certification: I hereby certify that these documents were prepared or approved by me, and that I am a duly Licensed Professional Engineer under the laws of the State of Maryland, License No. <u>20748</u>, Expiration Date <u>2-22-19</u>."

TENTATIVELY APPROVED DEPARTMENT OF PLANNING AND ZONING HOWARD COUNTY

<u>3-22-/8</u> DATE

	SOILS LEGEND							
501L	NAME	CLASS	Kw					
BrD	Brinklow channery loam. 15 to 25 percent slopes	B	.20					
GgA	Gleneig loam, 0 to 3 percent slopes	ß	.20					
GgB	Glenelg loam, 3 to 8 percent slopes	8	,20					
GgC	Glenelg loam, 8 to 15 percent slopes	B	.20					
*GmA	Glenville silt loam, 0 to 3 percent slopes	C	.37					
*GmB	Glenville silt loam, 3 to 8 percent slopes	С	*** .37					
*GnB	Glenville-Baile silt loams. 0 to 8 percent slopes	С	*** .37					
MaC	Manor loam, 0 to 15 percent slopes	8	.24					

LINDEN GROVE LOTS 1 THRU 44, BUILDABLE PRESERVATION PARCEL 'A' & NON-BUILDABLE PRESERVATION ARCELL A & MON-BOILDABLL FRESERVATION PARCELS 'B' THRU 'D' ZONED: RC-DEO TAX MAP No. 7 GRID No. 18 & TAX MAP No. 8 GRID No. 13 PARCEL No. 5 4TH ELECTION DISTRICT HOWARD COUNTY, MARYLAND DATE: JANUARY 25, 2018 SHEET 13 of 14

### B.4.C Specifications for Micro-Bioretention, Rain Gardens, Landscape Infiltration & Infiltration Berms

### . Material Specifications

The allowable materials to be used in these practices are detailed in Table B.4.1. 2. Filtering Media or Planting Soil

The soil shall be a uniform mix, free of stones, stumps, roots or other similar objects larger than two inches. No other materials or substances shall be mixed or dumped within the micro-bioretention practice that may be harmful to plant growth, or prove a hindrance to the planting or maintenance operations. The planting soil shall be free of Bermuda grass. Quackgrass, Johnson grass, or other noxious weeds as specified under COMAR 15.08.01.05.

The planting soil shall be tested and shall meet the following criteria: Soil Component - Loamy Sand or Sandy Loam (USDA Soil Textural Classification)

Organic Content - Minimum 10% by dry weight (ASTM D 2974). In general, this can be met with a mixture of loamy sand (60%-65%) and compost (35% to 40%) or sandy loam (30%), coarse sand (30%), and compost (40%).

Clay Content - Media shall have a clay content of less than 5%.

pH Range Should be between 5.5 - 7.0. Amendments (e.g., lime, iron sulfate plus sulfur) may be mixed into the soil to increase or decrease pH. There shall be at least one soil test per project. Each test shall consist of both the standard soil test for pH, and additional tests of organic matter, and soluble salts. A textural analysis is required from the site stockpiled topsoil. If topsoil is imported, then a texture analysis shall be performed for each location where the topsoil was excavated. 3. Compaction

It is very important to minimize compaction of both the base of bioretention practices and the required backfill. When possible, use excavation hoes to remove original soil. If practices are excavated using a loader, the contractor should use wide track or marsh track equipment, or light equipment with turf type tires. Use of equipment with narrow tracks or narrow tires, rubber tires with large lugs, or high-pressure tires will cause excessive compaction resulting in reduced infiltration rates and is not acceptable. Compaction will significantly contribute to design failure.

Compaction can be alleviated at the base of the bioretention facility by using a primary tilling operation such as a chisel plow, ripper, or subsoiler. These tilling operations are to refracture the soil profile through the 12 inch compaction zone. Substitute methods must be approved by the engineer. Rototillers typically do not till deep enough to reduce the effects of compaction from heavy equipment.

Rototill 2 to 3 inches of sand into the base of the bioretention facility before backfilling the optional sand layer. Pump any ponded water before preparing (rototilling) base.

When backfilling the topsoil over the sand layer, first place 3 to 4 inches of topsoil over the sand, then rototill the sand/topsoil to create a gradation zone. Backfill the remainder of the topsoil to final grade.

When backfilling the bioretention facility, place soil in lifts 12" to 18". Do not use heavy equipment within the bioretention basin. Heavy equipment can be used around the perimeter of the basin to supply soils and sand. Grade bioretention materials with light equipment such as a compact loader or a dozer/loader with marsh tracks. 4. Plant Material

Recommended plant material for micro-bioretention practices can be found in Appendix A. Section A.2.3. 5. Plant Installation

Compost is a better organic material source, is less likely to float, and should be placed in the invert and other low areas. Mulch should be placed in surrounding to a uniform thickness of 2" to 3" Shredded or chipped hardwood mulch is the only accepted mulch. Pine mulch and wood chips will float and move to the perimeter of the bioretention area during a storm event and are not acceptable. Shredded mulch must be well aged (6 to 12 months) for acceptance.

Rootstock of the plant material shall be kept moist during transport and on-site storage. The plant root ball should be planted so 1/8 th of the ball is above final grade surface. The diameter of the planting pit shall be at least six inches larger than the diameter of the planting ball. Set and maintain the plant straight during the entire planting process. Thoroughly water ground bed cover after installation.

Trees shall be braced using 2" by 2"stakes only as necessary and for the first growing season only. Stakes are to be equally spaced on the outside of the tree ball.

Grasses and legume seed should be drilled into the soil to a depth of at least one inch. Grass and legume plugs shall be planted following the non-grass ground cover planting specifications.

The topsoil specifications provide enough organic material to adequately supply nutrients from natural cycling. The primary function of the bioretention structure is to improve water quality. Adding fertilizers defeats, or at a minimum, impedes this goal. Only add ferfilizer if wood chips or mulch are used to amend the soil. Rototill urea ferfilizer at a rate of 2 pounds per 1000 square feet.

### 6. Underdrains

Underdrains should meet the following criteria:

Pipe- Should be 4" to 6" diameter, slotted or perforated rigid plastic pipe (ASTMF 758, Type PS 28, or AASHTO-M-278) in a gravel layer. The preferred material is "slotted, 4 rigid pipe (e.g., PVC or HDPE).

Perforations - If perforated pipe is used, perforations should be 3/8" diameter located 6" on center with a minimum of four holes per row. Pipe shall be wrapped with a 1/4" (No. 4 or 4x4) galvanized hardware cloth.

Gravel -The gravel layer (No. 57 stone preferred) shall be at least 3" thick above and below the underdrain.

The main collector pipe shall be at a minimum 0.5% slope.

A rigid, non-perforated observation well must be provided (one per every 1,000 square feet) to provide a clean-out port and monitor performance of the filter.

A 4 layer of pea gravel (1/4" to 3/8" stone) shall be located between the filter media and inderdrain to prevent migration of fines into the underdrain. This layer may be considered part of the filter bed when bed thickness exceeds 24".

The main collector pipe for underdrain systems shall be constructed at a minimum slope of 0.5%. Observation wells and/or clean-out pipes must be provided (one minimum per every 1000 square feet of surface area).

. Miscellaneous These practices may not be constructed until all contributing drainage area has been stabilized

# Infiltration and Filter System Construction Specifications

Infiltration and filter systems either take advantage of existing permeable soils or create a permeable medium such as sand for WC), and Re y. In some instances where permeability is great, these facilities may be used for Qp as well. The most common systems include nfiltration trenches, infiltration basins, sand filters, and organic filters.

When property planted, vegetation will thrive and enhance the functioning of these systems. For example, pre-treatment buffers will trap sediments that often are bound with phosphorous and metals. Vegetation planted in the facility will aid in nutrient uptake and water storage. Additionally, plant roots will provide arteries for stormwater to permeate soil for groundwater recharge. Finally, successful plantings provide desthetic value and wildlife habitat making these facilities more desirable to the public. Design Constraints:

> Planting buffer strips of at least 20 feet will cause sediments to settle out before reaching the facility, thereby reducing the possibility of clogging. > Determine areas that will be saturated with water and water table depth so that appropriate plants may be selected (hydrology will be similar to bioretention facilities, see figure A.5 and Table A.4 for planting material guidance).

> Plants known to send down deep taproots should be avoided in systems where filter fabric is used as part of facility design. > Test soil conditions to determine if soil amendments are necessary.

> Plants shall be located so that access is possible for structure maintenance. > Stabilize heavy flow areas with erosion control mats or sod.

> Temporarily divert flows from seeded areas until vegetation is established. > See Table A.5 for additional design considerations.

Bio-retention

Soil Bed Characteristics the characteristics of the soil for the bioretention facility are perhaps as important as the facility location, size, and treatment volume. The soil must be permeable enough to allow runoff to filter through the media, while having characteristics suitable to promote and sustain a robust vegetative cover crop. In addition, much of the nutrient pollutant uptake (nitrogen and phosphorus) is accomplished through absorption and microbial activity within the soil profile. Therefore, soils must balance their chemical and physical properties to support biotic communities above and below ground.

The planting soil should be a sandy loam, loamy sand, loam (USDA), or a loam/sand mix (should contain a minimum 35 to 60% sand, by volume). The clay content for these soils should be less than 25% by volume [Environmental Quality Resources (EQR), 1996; Engineering Technology Inc. and Biohabitats, Inc. (ETAB), 1993]. Soils should fall within the SM, ML, SC classifications or the Unified Soil Classification System (USCS). A permeability of at least 1.0 feet per day (0.5"/hr) is required (a conservative value of 0.5 feet per day is used for design). The soil should be free of stones, stumps, roots, or other woody material over 1" in diameter. Brush or seeds from noxious weeds (e.g., Johnson Grass, Mugwort, Nutsedge, and Canada Thistle or other noxious weeds as specified under COMAR 15.08.01.05.) should not be present in the soils, Placement of the planting soil should be in 12 to 18 lifts that are loosely compacted (tamped lightly with a backhoe bucket or traversed by dozer tracks). The specific characteristics are presented in Table A.3.

Table A.3 Planting Soil Characteristic	
Pårameter	Value
pH range	5.2 to 7.00
Organic matter	1.5 to 4.0% (by weight)
Magnesium	35 lbs. per àcre, minimur
Phosphorus (phosphāte — P2O5)	75 lbs. per àcre, minimur
Potāssium (potāsh —1(K2O)	85 lbs. per àcre, minimur
Soluble salts	500 ppm
Ciay	0 to 5%
Silt	30 to 55%
Sànd	35 to 60%

Mulch Layer

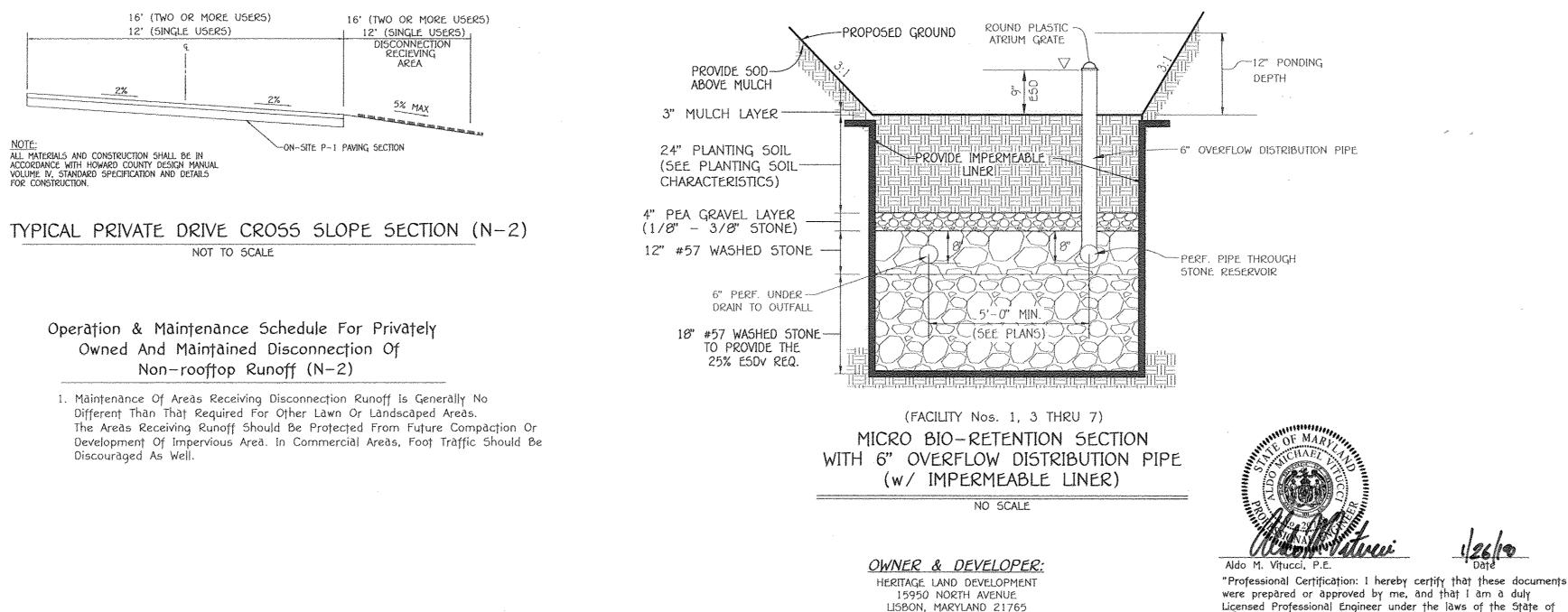
The mulch layer plays an important role in the performance of the bioretention system. The mulch layer helps maintain soil moisture and avoids surface sealing, which reduces permeability. Mulch helps prevent erosion, and provides a microenvironment suitable for soil biota at the mulch/soil interface. It also serves as a pretreatment layer, trapping the finer sediments. which remain suspended after the primary pretreatment.

The mulch layer should be standard landscape style, single or double shredded hardwood mulch or chips. The mulch layer should be well aged (stockpiled or stored for at least 12 months), uniform in color, and free of other materials, such as weed seeds, soil, roots, etc. The mulch should be applied to a maximum depth of three inches. Grass clippings should not be used as a mulch material.

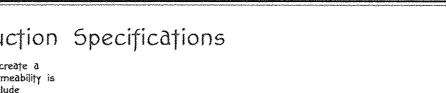
Planting Guidance Plant material selection should be based on the goal of simulating a terrestrial forested community of native species. Bioretention simulates an upland-species ecosystem. The community should be dominated by trees, but have a distinct community of understory trees, shrubs and herbaceous materials. By creating a diverse, dense plant cover, a bioretention facility will be able to treat stormwater runoff and withstand urban stresses from insects, disease, drought, temperature, wind, and exposure.

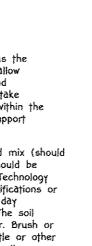
The proper selection and installation of plant materials is key to a successful system. There are essentially three zones within a bioretention facility (Figure A.5). The lowest elevation, supports plant species adapted to standing and fluctuating water levels. The middle elevation supports plants that like drier soil conditions, but can still tolerate occasional inundation by water. The outer edge

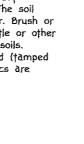
is the highest elevation and generally supports plants adapted to dryer conditions. For appropriate plant materials for bioretention facilities, Refer To MAA Approved Species List. The layout of plant material should be flexible, but should follow the general principals described in Table A.S. The objective is to have a system, which resembles a random, and natural plant layout, while maintaining optimal conditions for plant establishment and growth. For a more extensive bioretention plan, consult ETAB, 1993 or Claytor and Schueler, 1997.

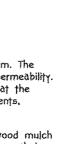


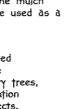
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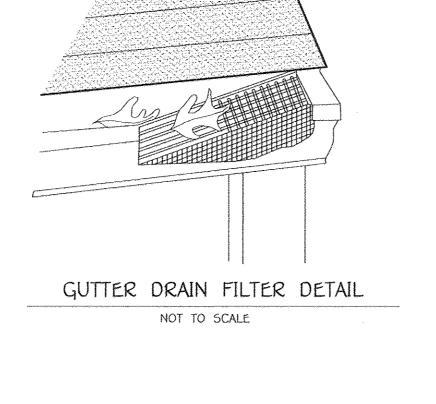


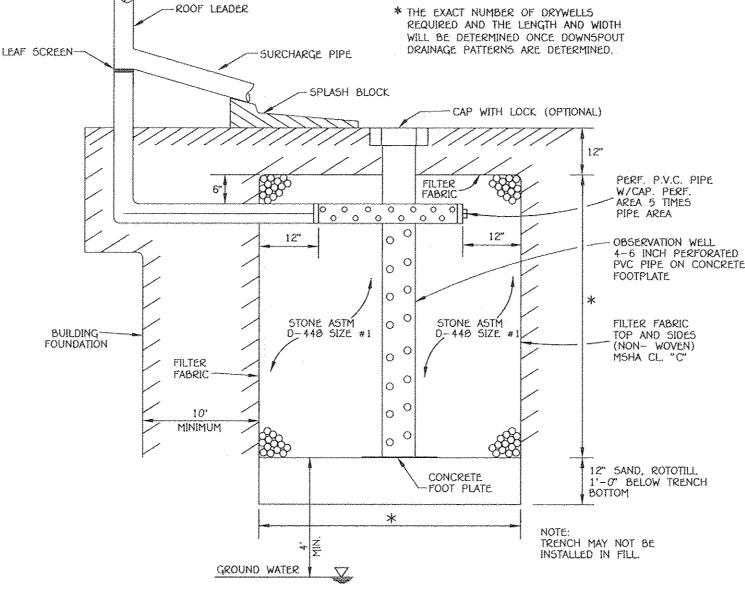












DRY WELL DETAIL (M-5) NOT TO SCALE

# Operation And Maintenance Schedule For Drywells (M-5)

1. The owner shall inspect the monitoring wells and structures on a guarterly basis and after every heavy storm event.

2. The owner shall record the water levels and sediment build up in the monitoring wells over a period of several days to insure trench drainage.

3. The owner shall maintain a log book to determine the rate at which the facility drains.

4. When the facility becomes clogged so that it does not drain down within a seventy two (72) hour time period, corrective action shall be taken.

5. The maintenance log book shall be available to Howard County for inspection to insure compliance with operation and maintenance criteria

6. Once the performance characteristics of the infiltration facility have been verified, the monitoring schedule can be reduced to an annual basis unless the performance data indicates that a more frequent schedule is required.

410-489-7900

were prepared or approved by me, and that I am a duly Licensed Professional Engineer under the laws of the State of Maryland, License No. 20748, Expiration Date 2-22-19."

INSTALLED.

